

COMMONWEALTH of VIRGINIA

DEPARTMENT OF TRANSPORTATION

1401 EAST BROAD STREET RICHMOND, VIRGINIA 23219-2000

PHILIP A. SHUCET COMMISSIONER

MOHAMMAD MIRSHAHI, P.E. STATE LOCATION AND DESIGN ENGINEER

March 17, 2003

MEMORANDUM

To: All Holders of the Virginia Department of Transportation's 2001 Road and Bridge Standards

The following is a list of standards contained in the 2001 <u>Road and Bridge Standards</u> that have been revised. Please add these pages to your copy of the standards. An insertable sheet will <u>not</u> be required in plan assemblies.

STANDARD	PAGE	REVISION
GS-10	702.00	Revised tables. Changed
GS-11	702.01	nomenclature of slopes from
GS-12	702.02	rational to percentage.
TC-5.01	802.13	Revised Relative Gradient
	802.14	Table and references to the
	802.22	table for application of the
	802.34 to 802.44	"two second rule" resulting in
		CR and LS Computations for
		9' and 10' roadway widths.

The following is a list of revised standards to the 2001 Road and Bridge Standards that do require an insertable sheet to be in included in your plan assembly until the next edition of the imperial standards is published. Please add these pages to your copy of the standards. The respective insertable sheet number has been placed with the revised standard in parenthesis. An insertable sheet is available for each of these revised standards. The insertable sheets are available on VDOT's web site on the FTP server and in Falcon DMS for VDOT personnel. These insertable sheets will be required in plan assemblies for projects utilizing the standard items listed below that have not been turned in for first submission.

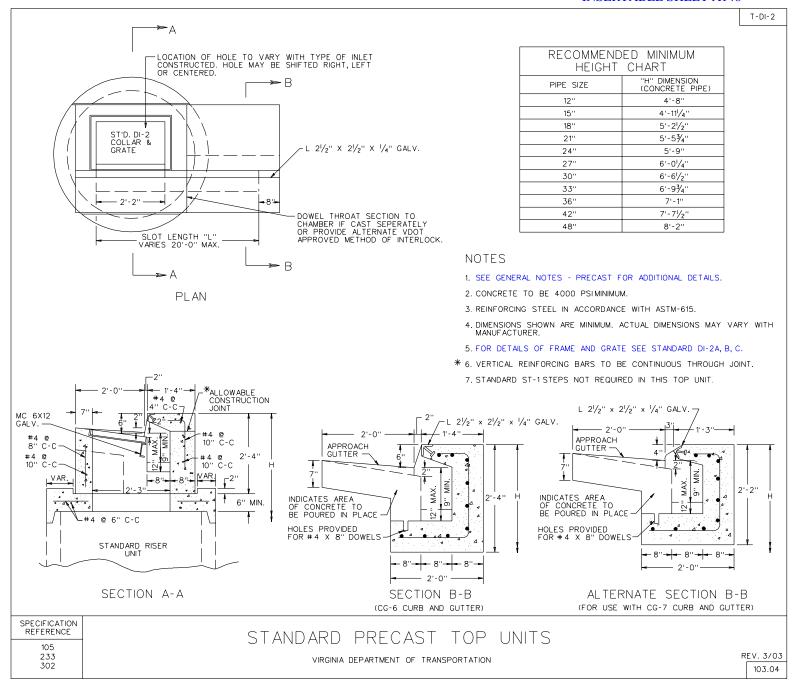
STANDARD	PAGE	REVISION
T-DI-2 (A148)	103.04	Modify min. height chart to
T-D-I-3, 4 (A148)	103.05	include additional pipe sizes.

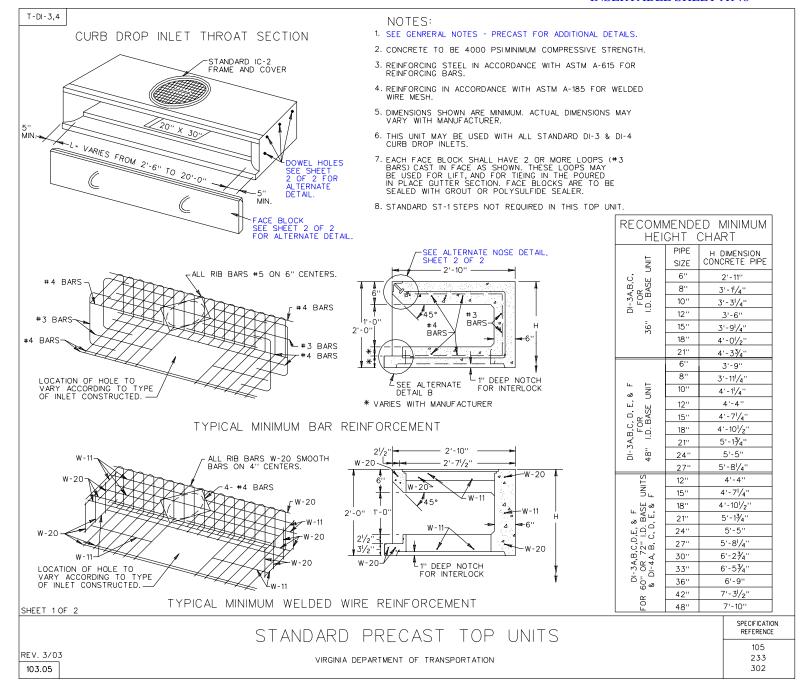
STANDARD SB-1 (A143) SB-1PC (A143)	PAGE 110.01 110.02	REVISION Revise dimension tables. Revise interior height of Circular structure.
EC-5 (ISD414-1) EC-6 (ISD414-2) EC-INS (ISD414-4)	114.06 114.07 115.01	Revised notes, dimensions, and references to Geotextile fabrics.
SWM-1 (ISD2209)	116.01 116.02	Replaced DI-7 cover with trash rack and riprap with Conc. Class A3 for invert fill.
	116.03	Void and removed From Standards
SWM-DR (ISD2216, ISD2216A)	116.04 116.05 116.06 116.07 116.08	Revise quantities for Concrete Cradle and added quantity table. Added HDPE Debris Rack. Added Trash Rack Details.
CG-12 (A59)	203.05 203.06 203.07	Revise typical application details and redefined as detectable warning surface.
CG-13 (A108)	203.08	Incorporates detectable warning surface.
RS-1 (ISD1722)	304.01	Removed notes referring to shoulder material.
RS-2	304.02	Void and removed from standards.
GR-6 (A132)	501.10	Added detail for occurrence of paved ditch.
GR-11 (A145)	501.21	Revised Pay Limits
GR-INS (A146)	501.33 501.34	Added detail for Terminal end occurrence beyond clear zone

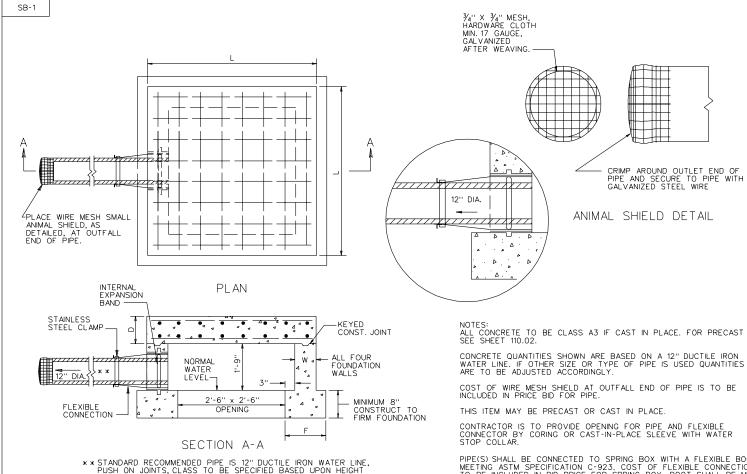
If you have any questions or comments regarding the listed revisions to this publication, please contact Mrs. N. E. Berry of the Engineering Services Section at (804) 786-2543.

Sincerely,

Mohammad Mirshahi, P.E. State Location and Design Engineer







					R	EINFORCI	NG S	reel)UANTIT	IES
HEIGHT OF FILL	SIZE (L)	TOP SLAB (D)	SIDEWALLS (W)			LENGTH	SIZE	SPACING C-C		REINF. STEEL LBS.	INCREMENT * CU. YDS.
BELOW 25'	4'	8''	6"	12''	32	3'-9''	#4	6"	1.189	80	0.043
25' - 50'	4'-4''	8''	8"	14''	32	4'-1''	#5	6"	1.512	136	0.053

OF COVER.

* QUANTITIES SHOWN ARE BASED ON A 8" DEPTH OF FOOTING, ADD INCREMENTAL QUANTITY FOR EACH ADDITIONAL 1" OF DEPTH.

ALL CONCRETE TO BE CLASS A3 IF CAST IN PLACE. FOR PRECAST SEE SHEET 110.02.

CONCRETE QUANTITIES SHOWN ARE BASED ON A 12" DUCTILE IRON WATER LINE. IF OTHER SIZE OR TYPE OF PIPE IS USED QUANTITIES ARE TO BE ADJUSTED ACCORDINGLY.

COST OF WIRE MESH SHIELD AT OUTFALL END OF PIPE IS TO BE

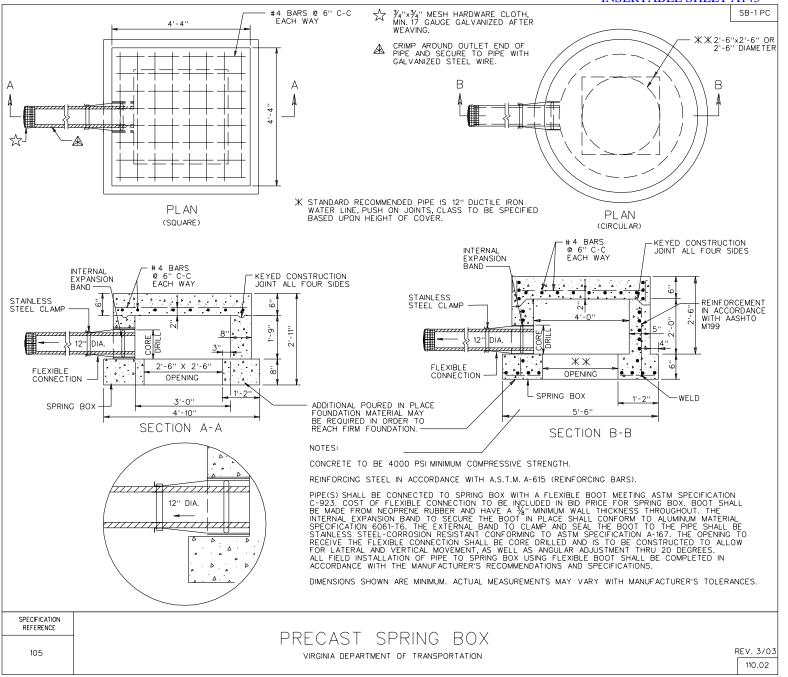
THIS ITEM MAY BE PRECAST OR CAST IN PLACE.

CONTRACTOR IS TO PROVIDE OPENING FOR PIPE AND FLEXIBLE CONNECTOR BY CORING OR CAST-IN-PLACE SLEEVE WITH WATER

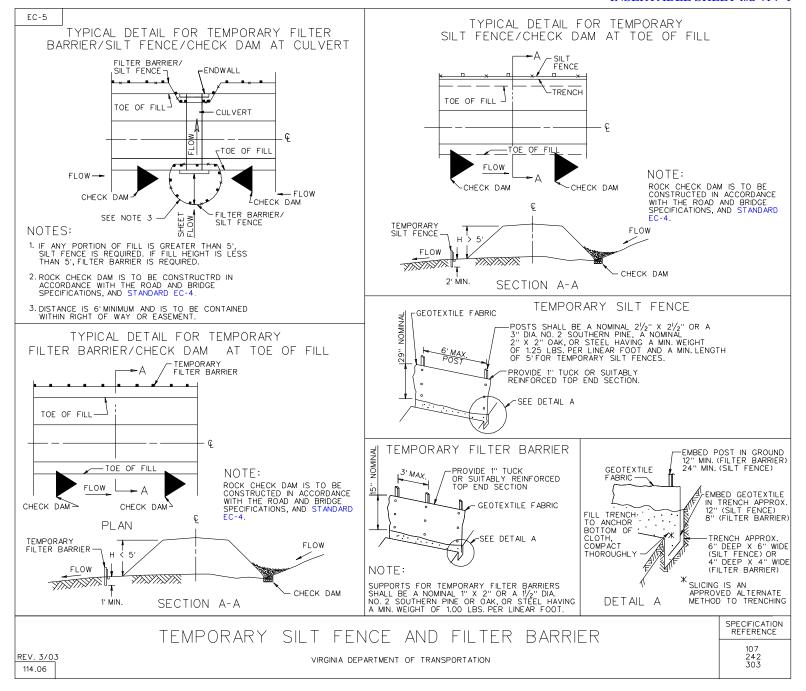
PIPE(S) SHALL BE CONNECTED TO SPRING BOX WITH A FLEXIBLE BOOT MEETING ASTM SPECIFICATION C-923. COST OF FLEXIBLE CONNECTION TO BE INCLUDED IN BID PRICE FOR SPRING BOX. BOOT SHALL BE MADE FROM NEOPRENE RUBBER AND HAVE A 3½" MINIMUM WALL THICKNESS THROUGHOUT. THE INTERNAL EXPANSION BAND TO SECURE THE BOOT IN PLACE SHALL CONFORM TO ALUMINUM MATERIAL SPECIFICATION 6061-16. THE EXTERNAL BAND TO CLAMP AND SEAL THE BOOT TO THE PIPE SHALL BE STAINLESS STEEL-CORROSION RESISTANT CONFORMING TO ASTM SPECIFICATION A-167. THE OPENING TO RECEIVE THE FLEXIBLE CONNECTION SHALL BE CORE DRILLED AND IS TO BE CONSTRUCTED TO ADJUSTMENT THRU 20 DEGREES. ALL FIELD INSTALLATION OF PIPE TO SPRING BOX USING FLEXIBLE BOOT SHALL BE COMPLETED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND SPECIFICATIONS ANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND SPECIFICATIONS.

STANDARD	SPRING	BOX

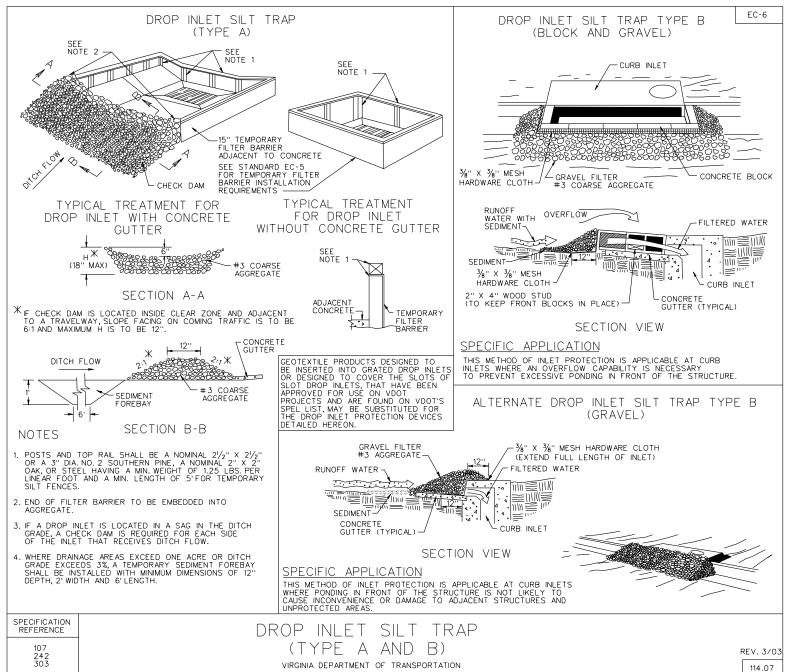
SPECIFICATION



INSERTABLE SHEET isd 414 1

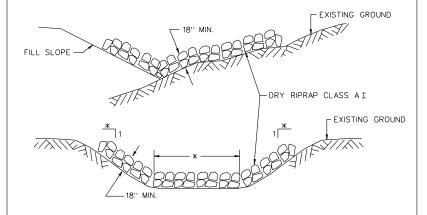


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ESC-INS

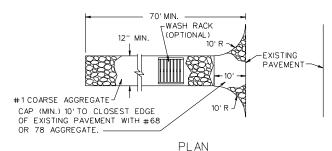
SUGGESTED METHOD OF TEMPORARILY PLACING RIPRAP FOR EROSION CONTROL IN CHANNELS, DITCHES, & AT TOE OF FILL SLOPES

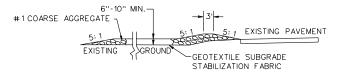


NOTES:

 THE DEPTH OF PROTECTION WILL DEPEND ON WHATEVER DEPTH IS ATTAINABLE, WITH THE RIPRAP BEING EVENLY SPREAD WITH THE QUANTITY SHOWN ON THESE PLANS. RIPRAP MAY BE ADDED OR DELETED AS FOUND NECESSARY BY THE ENGINEER.

MINIMUM REQUIREMENTS FOR STABILIZED CONSTRUCTION ENTRANCE





PROFILE

- 1. SURFACE WATER SHALL BE PIPED UNDER THE CONSTRUCTION ENTRANCE. IF PIPING IS IMPRACTICAL, A MOUNTABLE BERM WITH 5:1 SLOPES WILL BE PERMITTED.
- 2.THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHT OF WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR ADD/OR CLEANOUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHT OF WAY SHALL BE REMOVED IMMEDIATELY.
- 3. WHEELS SHALL BE CLEANED TO REMOVE SEDIMENT PRIOR TO ENTRANCE ONTO PUBLIC RIGHT OF WAY. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA STABILIZED WITH STONE AND WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE.
- 4.PERIODIC INSPECTION AND NEEDED MAINTENANCE SHALL BE PROVIDED AFTER HEAVY USE AND EACH RAIN.
- * SIDE SLOPES AND BOTTOM WIDTH (IF TRAPEZOIDAL) SHOWN IN TYPICAL SECTION OF PROPOSED DITCH OR CHANNEL.

SHEET 1 OF 3

SPECIFICATION REFERENCE

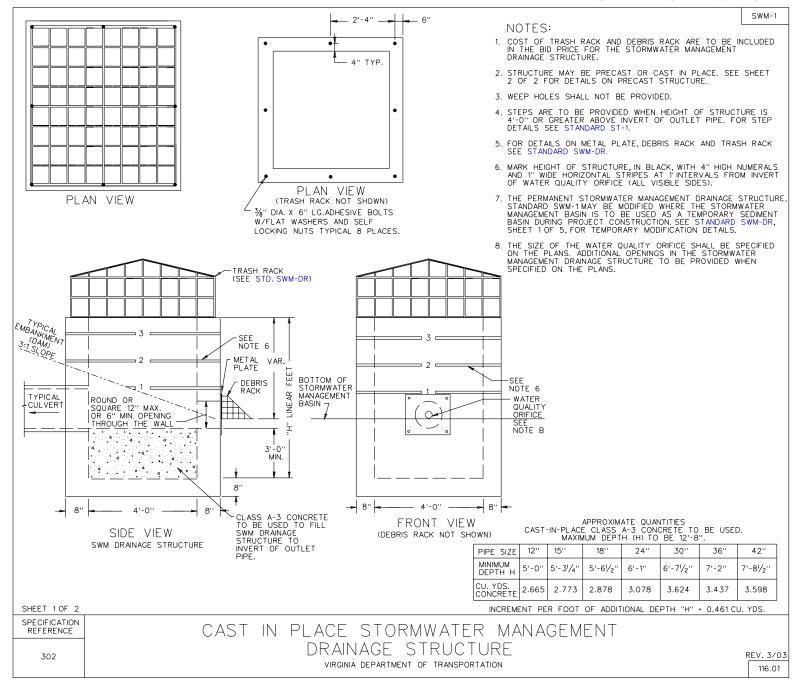
TEMPORARY FROSION & SILTATION CONTROL

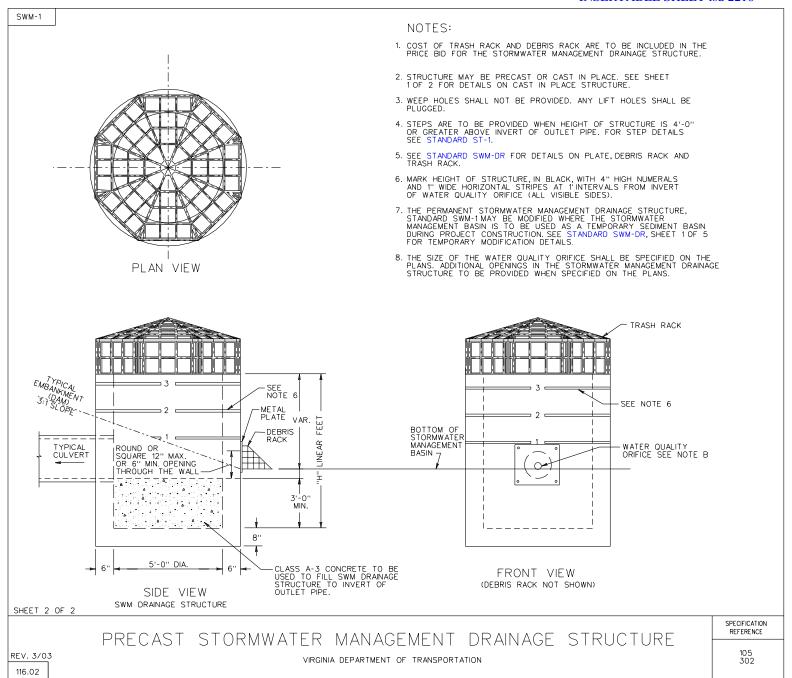
107 303

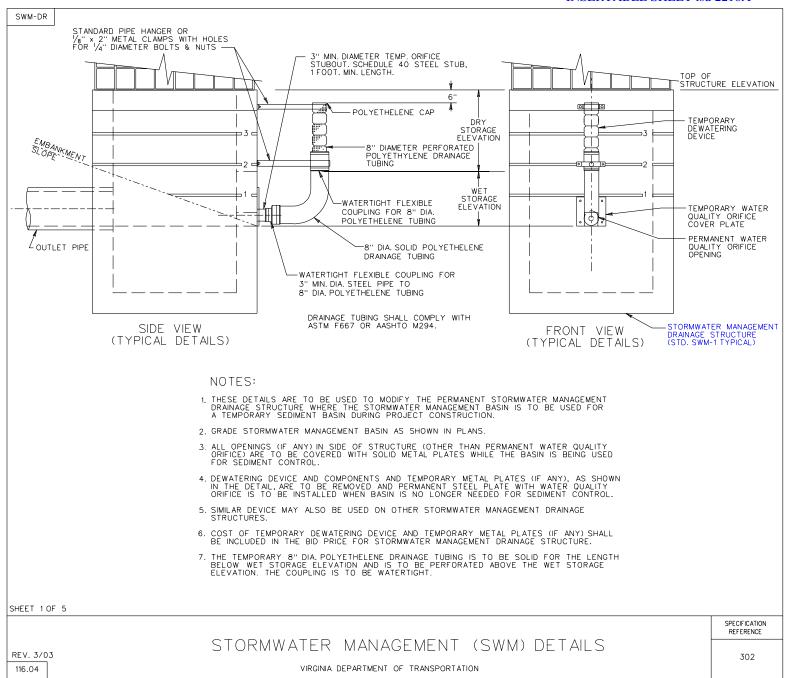
VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03

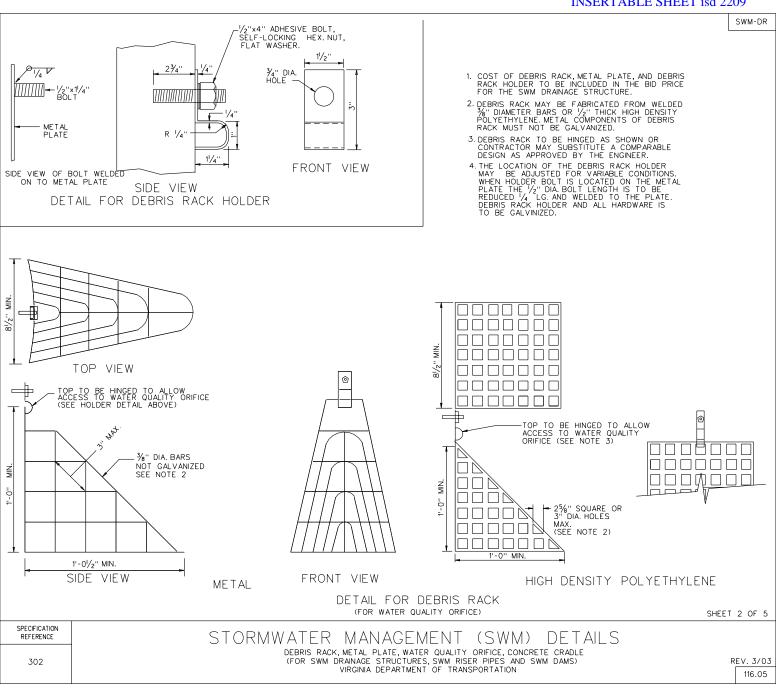
INSERTABLE SHEET isd 2216



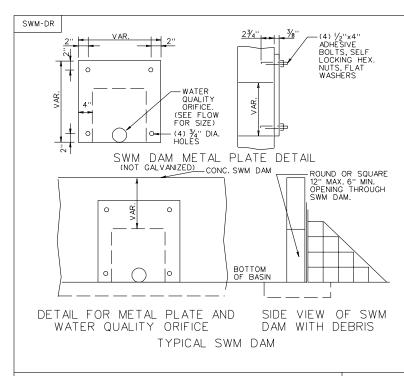


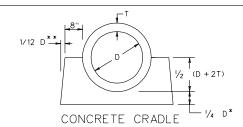


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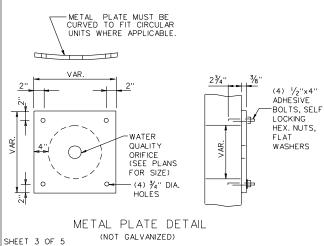


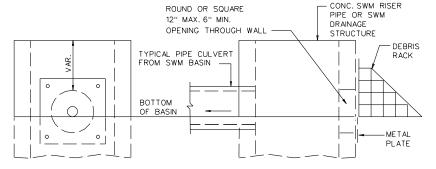


PIPE SIZE INCHES	CRADLE BOTTOM WIDTH (INCHES)	CRADLE HEIGHT (INCHES)	CRADLE TOP WIDTH (INCHES)	INCREMENT, IN CUBIC YARDS, PER LINEAR FOOT OF PIPE
12	34	14	32	0.093
15	38	15.75	35.5	0.110
18	42	17.5	39	0.129
24	50	21	46	0.168
30	58	26	53	0.233
36	66	31	60	0.307
42	74	36	67	0.390

- CONCRETE SHALL BE CLASS A3
- * BUT NOT LESS THAN 6"
- ** IF THE PIPE IS LAID IN AN EXCAVATED TRENCH, THEN THE SIDE WALLS MAY CONFORM TO THE TRENCH SHAPE (IE THE TRENCH MAY BECOME THE CRADLE FORM).

CONCRETE CRADLE IS TO BE INSTALLED UNDER THE ENTIRE LENGTH OF CULVERT AT EACH STORMWATER MANAGEMENT BASIN. CONCRETE CRADLE IS TO BE PAID FOR AS MISCELLANEOUS CONCRETE AND SUMMARIZED IN CUBIC YARDS FOR EACH PIPE LOCATION





DETAIL FOR METAL PLATE AND SIDE VIEW WITH DEBRIS RACK WATER QUALITY ORIFICE

TYPICAL SWM DRAINAGE STRUCTURE

STORMWATER MANAGEMENT (SWM)

DEBRIS RACK, METAL PLATE, WATER QUALITY ORIFICE, CONCRETE CRADLE (FOR SWM DRAINAGE STRUCTURES, SWM RISER PIPES AND SWM DAMS)

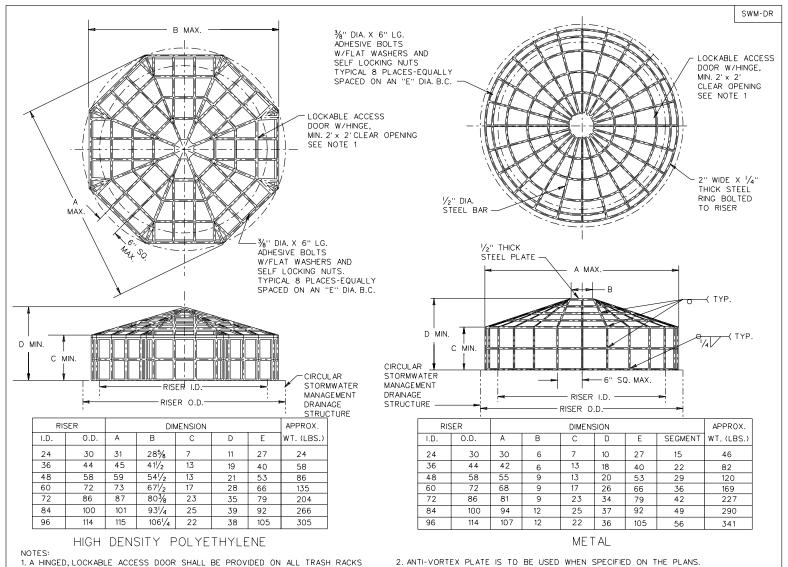
VIRGINIA DEPARTMENT OF TRANSPORTATION

SPECIFICATION REFERENCE

302

REV. 3/03 116.06

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1. A HINGED, LOCKABLE ACCESS DOOR SHALL BE PROVIDED ON ALL TRASH RACKS IF THE TOTAL WEIGHT OF THE TRASH RACK IS GREATER THAN 75 LBS OR IF THE TRASH RACK IS TO BE PLACED ON A SWM-1 WITH AN "H" DIMENSION GREATER THAN 7"-2". . ANTI-VORTEX PLATE IS TO BE USED WHEN SPECIFIED ON THE PLAN
COST OF FURNISHING AND PLACING THE ANTI-VORTEX PLATE IS TO
BE INCLUDED IN THE BID PRICE FOR THE STRUCTURE.

SHEET 4 OF 5

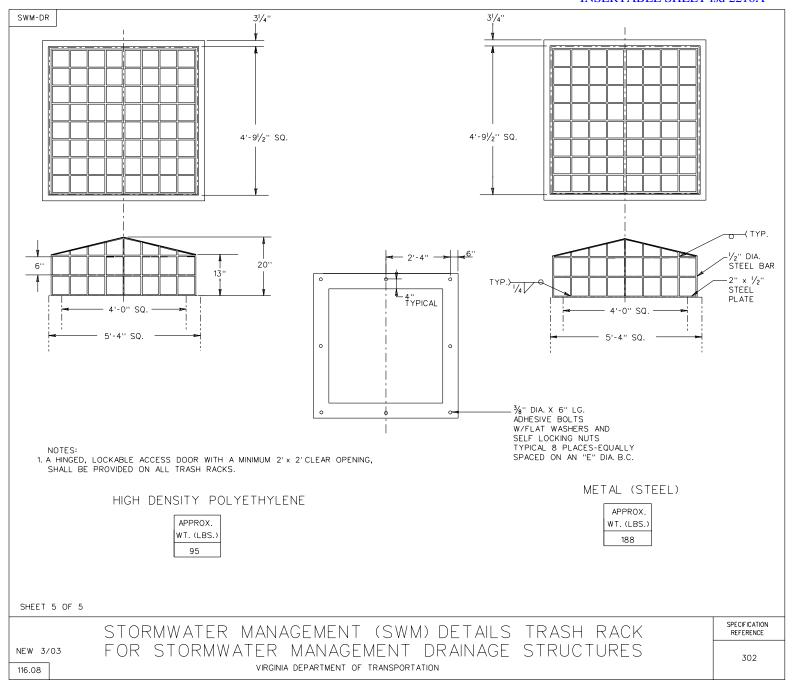
SPECIFICATION REFERENCE	
302	

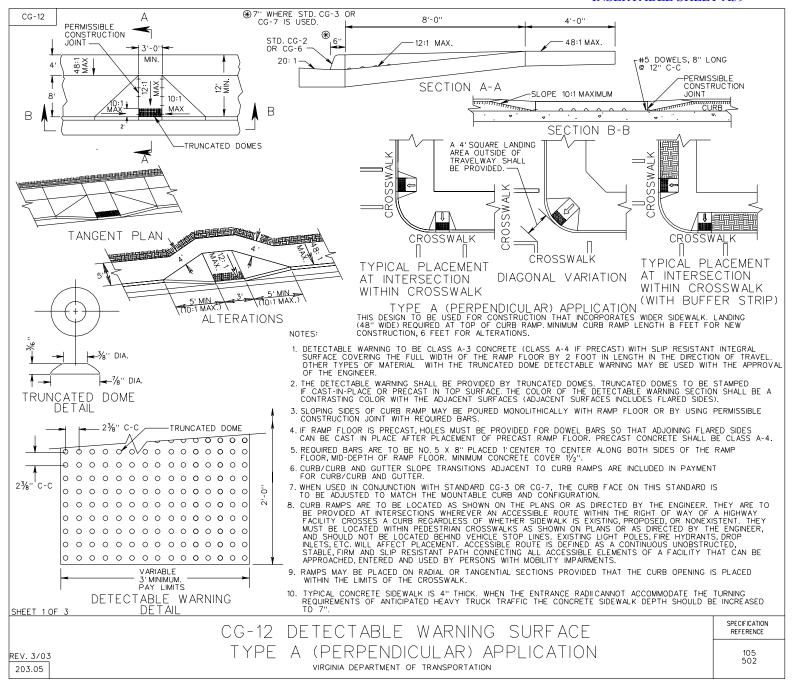
STORMWATER MANAGEMENT (SWM) DETAILS TRASH RACK FOR STORMWATER MANAGEMENT DRAINAGE STRUCTURES

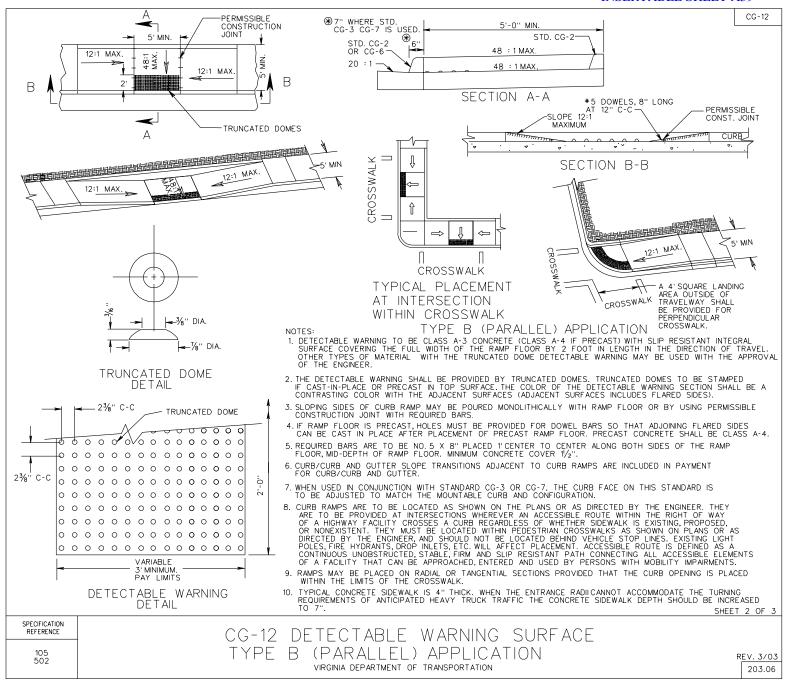
NEW 3/03

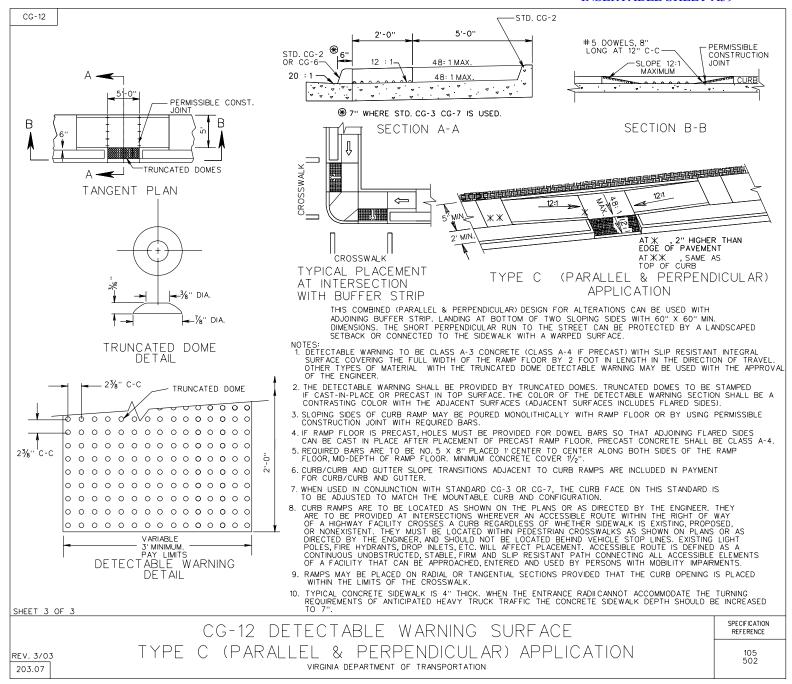
116.07

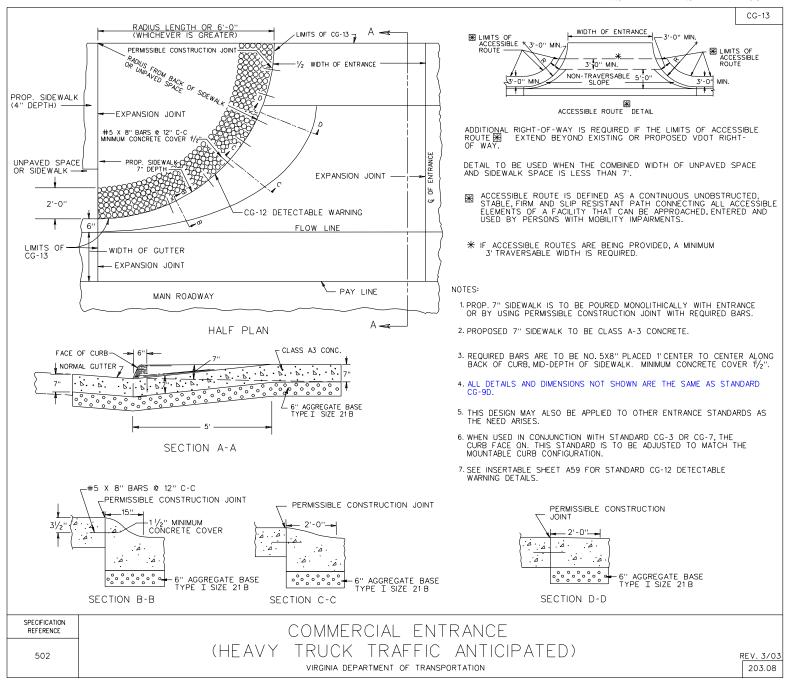
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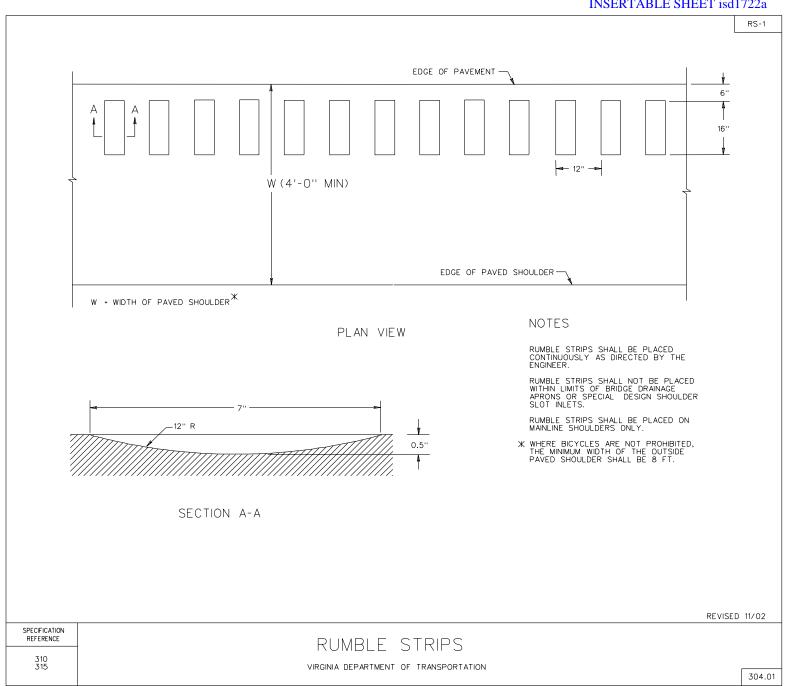


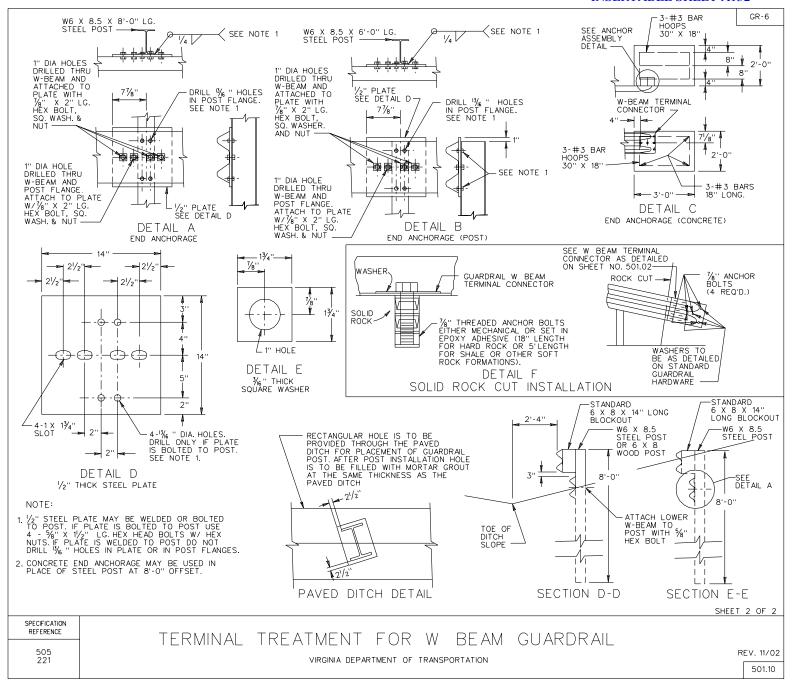


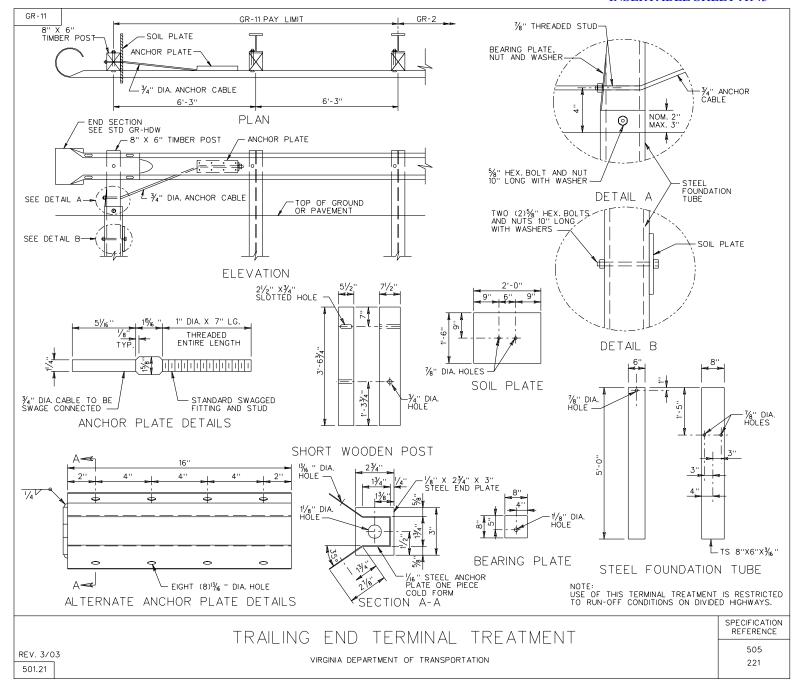


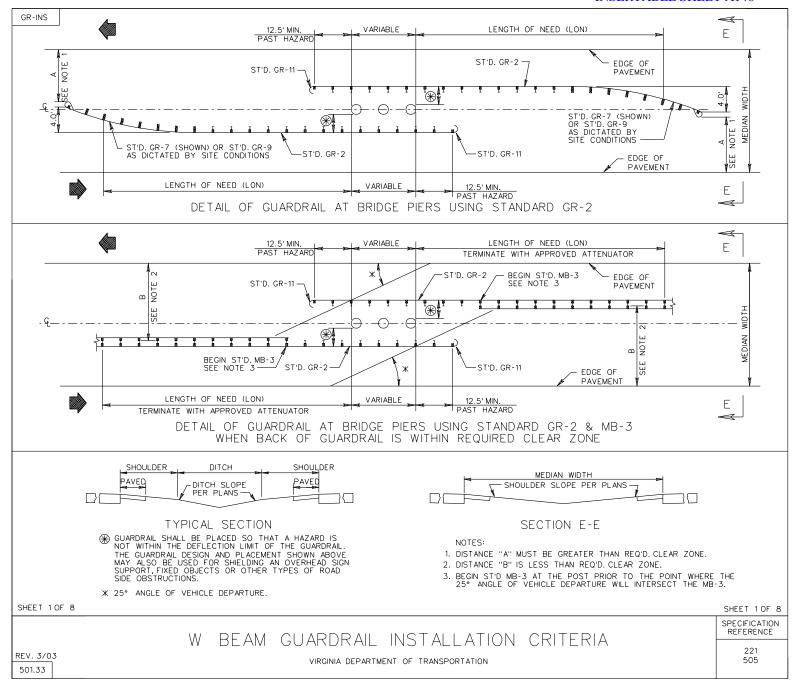


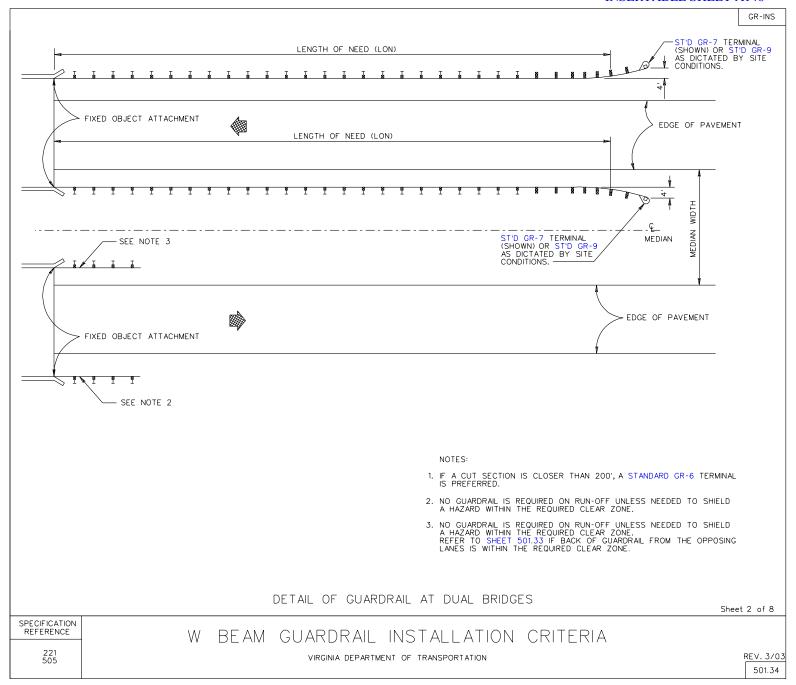
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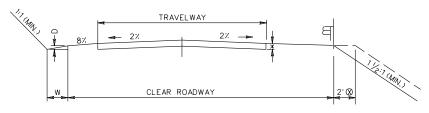












X SEE PLANS FOR BASE DEPTH AND TYPE AND PAVED SURFACE TREATMENT WHERE REQUIRED.

TYPICAL SECTION

BRIDGE WIDTH - APPROACH ROADWAY WIDTH (CLEAR ROADWAY).

	WIDTHS FOR TWO WAY TRAFFIC							
	(LESSER WIDTH MAY BE USED FOR ONE-WAY)							
TYPE	CURRENT	* TRAVELWAY	SURF		MIN. Ø ROADWAY SHOULDER	DITCH WIDTH	DITCH DEPTH	PAY ITEM
	ADT	WIDTH	UNPAVED	PAVED	TO SHOULDER	(W)	(D)	
А	0-250	18'	/		22'	4'	16''	LF.
В	251- 750	20'	/		24' ABS. 30' DES.	4'	16''	LF.
С	751- 2000	22'		/	30' ABS. 34' DES.	4'	16''	* *
D	2001- 5500	24'		/	40'	4'	16''	* *
Е	5501- 15,000	24'		/	40'	4'	16''	* *
F	15,000- ABOVE	24'		/	40'	6'	18''	* *

	GEOMETRICS						
DESIGN SPEE	D M.P.H.	20	30	40	50	60	70
MIN. RADII		108' R	251' R	465' R	760'R	1204' R	1821' R
MAX. % GRADE	DES. ABS.	8% 16%	7% 14%	7% 13%	6% 10%	5% 6%	5% 6%
STOPPING SIGHT DISTANCE	DES. MIN.	125'	200'	325' 305'	475' 425'	650' 570'	850' 730'
MAXIMUM SUPERELEVATION		8%	8%	8%	8%	8%	8%

IF GEOMETRICS AND WIDTHS SHOWN IN THESE CHARTS ARE GREATER THAN THE FINISHED CONTRACT DESIGN, APPROVAL MAY BE GRANTED BY THE DEPARTMENT FOR LESSER VALUES.

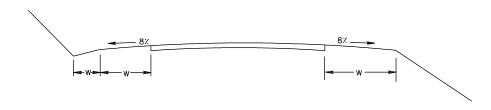
- * CURVES TO BE WIDENED IN ACCORDANCE WITH ST'D. TC-5.01R.
- ** PAID FOR BY INDIVIDUAL QUANTITIES.

SPECIFICATION REFERENCE
REFERENCE

MINIMUM DESIGN CRITERIA FOR TEMPORARY DETOURS (MAINTENANCE OF TRAFFIC)

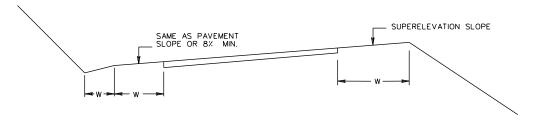
GRADED MEDIAN SHOULDERS	OUTSIDE SHOULDERS					
** WHERE MAINLINE IS 6 OR MORE LANES GRADED SHOULDER WIDTH IS TO BE THE SAME AS THAT SHOWN FOR FILL SHOULDER FOR INDEPENDENT GRADING.	7% ALG. DIFF. W FILL					
HIGH SIDE - SUPERELEVATED	HIGH SIDE - SUPERELEVATED					
SAME RATE AS PAVEMENT SLOPE OR 5% MINIMUM—————————————————————————————————	SAME RATE AS PAVEMENT SLOPE OR 5% MINIMUM W FILL					
LOW SIDE - SUPERELEVATED	LOW SIDE - SUPERELEVATED					
NOTE: FOR WIDTH OF SHOULDERS AND DITCH	HES (W) SEE GEOMETRIC DESIGN STANDARDS.					
STANDARD SHOULDER DESIGN FOR ALL SYSTEMS REV. 3/03 EXCEPT LOCAL ROADS AND STREETS VIRGINIA DEPARTMENT OF TRANSPORTATION						

TANGENT SECTION



FOR WIDTHS OF SHOULDERS AND DITCHES (W) SEE STANDARDS..

SUPERELEVATED SECTION

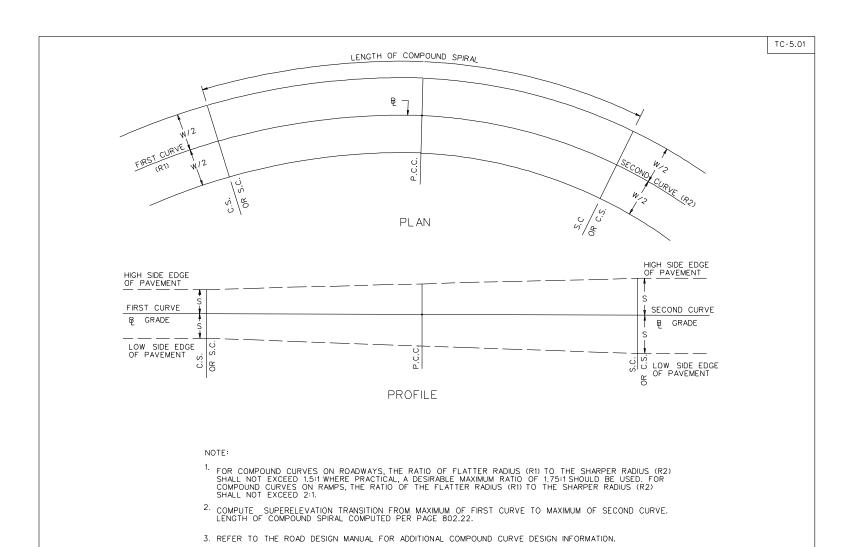


FOR WIDTHS OF SHOULDERS AND DITCHES (W) SEE STANDARDS.

STANDARD SHOULDER DESIGNS FOR LOCAL ROADS & STREETS

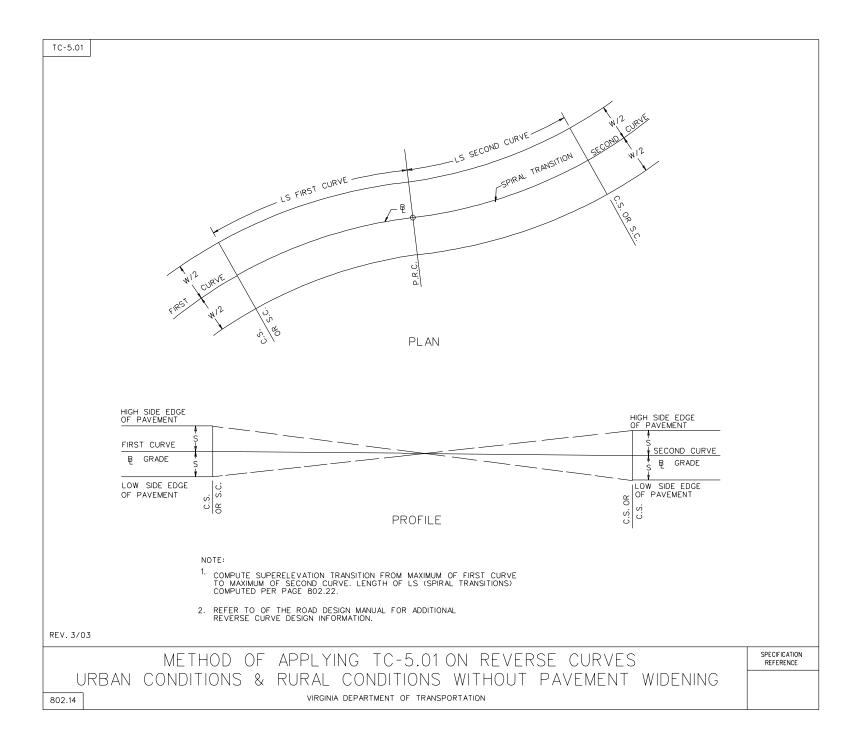
VIRGINIA DEPARTMENT OF TRANSPORTATION

REV 3/03



SPECIFICATION REFERENCE METHOD OF APPLYING TC-5.01 ON COMPOUND CURVES URBAN CONDITIONS & RURAL CONDITIONS WITHOUT PAVEMENT WIDENING

REV. 3/03



TC-5.01

CURVE WIDENING TABLES

SU DESIGN VEHICLE

COMPONENT	SIZE
OVERALL WIDTH (u)	8.0 ft
WHEELBASE (L)	20 ft
FRONT OVERHANG (A)	4 ft

LATERAL CLEARANCE

LANE WIDTH	CLEARANCE (C)
9 ft	1.5 ft
10 ft	2 ft
11 ft	2.5 ft
12 ft	3 ft
16 ft	5 ft

ADJUSTMENT FACTORS

NUMBER OF LANES ROTATED	ADJUSTMENT FACTOR (b _w)
1	1.00
1.5	0.8333
2	0.75
2.5	0.70
3	0.6667
3.5	0.6425

RELATIVE GRADIENTS

DESIGN SPEED VD MPH	MAXIMUM RELATIVE GRADIENT (rg)	MIN. TRANSITION LENGTH IN FEET RURAL CONDITIONS WITH PAVEMENT WIDENING AND REVERSE CURVES FOR ALL CONDITIONS (2 SECOND RULE)
20	0.74	59
25	0.70	74
30	0.66	88
35	0.62	103
40	0.58	117
45	0.54	132
50	0.50	147
55	0.47	161
60	0.45	176
65	0.43	191
70	0.40	205

A - FRONT OVERHANG OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

bw - ADJUSTMENT FACTOR FROM TABLE.

C - LATERAL CLEARANCE OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

E - SUPERELEVATION RATE FROM APPROPRIATE TABLE.

 F_A - CALCULATED WIDTH OF OVERHANG FOR DESIGN VEHICLE.

 WHEELBASE OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

LS - LENGTH OF SPIRAL OR SUPERELEVATION TRANSITION LENGTH.

DEFINITIONS

M - MULTIPLE LANE FACTOR.

N - NUMBER OF LANES.

n₁- NUMBER OF LANES ROTATED (FROM TABLES).

Pw - PAVEMENT WIDTH.

R - RADIUS OF CURVE.

rg - RELATIVE GRADIENT FROM APPROPRIATE TABLE.

U - CALCULATED TRACK WIDTH OF DESIGN VEHICLE.

u - TRACK WIDTH OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

Vn - DESIGN VELOCITY.

w - CALCULATED WIDENING.

W - PAVEMENT WIDTH

WC - CALCULATED TOTAL CURVE WIDTH.

W. - WIDTH OF LANE.

Z - CALCULATED EXTRA WIDTH ALLOWANCE.

GENERAL DESIGN CONSIDERATIONS

- WHERE PAVEMENT WIDENING IS REQUIRED, THE APPROPRIATE WIDENING IS ADDED TO THE LANE WIDTH WHEN CALCULATING THE TRANSITION LENGTH (LS).
- 2. THE COMPUTED TRANSITION LENGTH (LS) IS ROUNDED UP TO THE NEAREST FOOT.
- 3. WHEN THE TRANSITION LENGTH (LS) IS CALCULATED, IT MUST BE COMPARED WITH THE MINIMUM VALUE LISTED IN THE APPROPRIATE COLUMN ON THE RELATIVE GRADIENT TABLE.
- 4. CROWN RUNOFF IS ALWAYS ACHIEVED OUTSIDE OF THE TRANSITION.
- 5. NO PAVEMENT WIDENING IS REQUIRED FOR URBAN ROADWAYS.
- NO PAVEMENT WIDENING IS REQUIRED FOR RURAL ROADWAYS WITH A CURVE RADIUS GREATER THAN 2865 FEET.

- 7. NO PAVEMENT WIDENING IS REQUIRED FOR RURAL ROADWAYS WITH 12 FOOT WIDE LANES AND A CURVE RADIUS GREATER THAN 881 FEET.
- 8. PAVEMENT WIDENING IS APPLIED ONLY WHEN CALCULATED WIDENING (w) IS EQUAL TO OR GREATER THAN 2 FEET.
- 9. WHEN CALCULATING WIDENING (w) FOR MULTI-LANE RURAL ROADWAYS, WIDENING IS FIRST CALCULATED USING THE SINGLE LANE WIDTH FOR "W".
- 10. AN ALTERNATE METHOD FOR MULTI-LANE UNDIVIDED PAVEMENTS (48°). THE LS IS 1.5 TIMES (M-1.5) THE CORRESPONDING LENGTH FOR TWO LANE HIGHWAYS; AND FOR SIX LANE UNDIVIDED PAVEMENTS (72°), THE LS IS TWO TIMES (M-2) THE CORRESPONDING LENGTH FOR TWO LANE HIGHWAYS.
- 11. CALCULATED WIDENING IS ROUNDED UP TO THE NEAREST 0.1 FOOT.
- 12. CURVES WITH SPIRAL CURVE TRANSITIONS MUST HAVE A MINIMUM TRANSITION LENGTH (LS) EQUAL TO 2 SECONDS OF TRAVEL TIME AT THE ROADWAY'S DESIGN SPEED AS NOTED IN THE RELATIVE GRADIENT TABLE.

NO WIDENING REQUIRED FORMULAS USED TO CALCULATE TRANSITION LENGTH (LS) AND WIDENING (W)

 $LS = b_w(W_n E/rg)$

LS = M(WE/rg) (ALT. MULTI-LANE)

WIDENING REQUIRED

 $LS = b_w[E n_1(W_n + w/N)/rg]$

LS = m[E(W + w/N)/rg] (ALT. MULTI-LANE)

 $U = u + R - \sqrt{R^2 - L^2}$

 $F_{A} = \sqrt{R^2 + A(2L + A)} - R$

 $Z = (V_D / \sqrt{R})$

 $w = W_C - 2W_D$

 $W_C = N(U + C) + F_A + Z$

FOR SOLVED PROBLEMS USING THIS METHODOLOGY, SEE THE EXAMPLES ON PAGE 802.23

METHODOLOGIES FOR CALCULATING TC-5.01 VALUES

REV. 3/03 802.22

VIRGINIA DEPARTMENT OF TRANSPORTATION

MPS		S	0 4	43	45	4 6 4	51	53	55	29	61	63	65	69	71	73	77	79	81	83	85	80 80	92	94	96	100	102	104	108	110	112	116	118	120	124	126	128	132	134	136	140	142	144	148	150	152	156	158	162	
ANGE RAMPS	α		0 4	41	41	1 4	41	41	L 4 L 4	14	14	41	4 4	41	41	14	4 4	14	41	14	41	4 4	14	14	4 4	41	14	4 4	41	41	41	- 4	41	14	1 4	41	14	4 4	14	41	4	14	4 4	41	41	41	41	14	1 4	
INTERCHANGE	1	- S	0 %	40	42	44	84	20	52	56	28	9	63	65	67	69	77	75	77	79	80	82	98	88	90	94	96	200	10	103	105	109	111	113	11	119	120	122	126	128	132	134	138	140	141	14.5	147	149	153	į
INTER	7	. $-$	0 %	39	39	39	39	39	39	39	39	39	39	39	39	39	50 50 00 00	39	39	39	39	39	39	39	95 05	39	39	50 50 00 00	39	39	39	39	39	39	80 %	39	39	39	39	39	39	39	39	39	39	39	39	39	39	
F		>	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.2	4.7	2.8	3.0	3.2	3.6	3.8	5.4	4.4	9.4	5.2	5.6	8.0	9.9	7.0	9.7	- !
WIDTH=48 I	12.	LS L	0 8	+	54	+	+	H	99	2 2	73	9/	8 2	83	98	88	0 20	95	86	100	-	201 801	+	\forall	115	+-	Н	125	+	132	134	137	\vdash	_	101	+	\vdash	17.7	185	189	198	202	206	217	222	227	239	246	270	_ ,
MIDTH	(` I	0 4	49	49	0 4	64	49	04 4	49	49	64	0 4	49	49	49	94 9	49	49	49	49	64 9	49	49	94 4	64	64	24 0	64	49	49	40	53	54	5.5	55	55	56	57	57	286	28	5 5	09	09	61	63	64	0 89 0 89	
I I ц	Ĭ Ĭ	>		+	+	-	0.0		0.0	+	+	0.0	0.0	0.0	Н	+	0.0	+	Н			0.0		Н	0.0	0	0.0	0 0	0.0	0	-	0.0	Н		0.0	+		0.0		0.0) -	2.2	2.3	9 9	-	6.7	5.3	5.5	0 9 0 9	-
WIDTH=24 FT	1.0 1.7		0 25	+	+	+	41	Н	44	+	+	_	52	+	Н	+	9 6	+	65 (Н	+	9 6	+	75 () (c	\vdash	Н	+	+		+	91	Н	-	0,00	+	\Box	104	H	601	+	124	127	+	134	137	143	145	155 4	-
WIDTH	, C -			+	33	+	+	Н	N 10	2 2	3 2	2	2 2	2 2	2	20	2 6	2 2	3	2	2	~) r	3 2	3	2 4	2 22	2	2 6	2 2	3	50	2 2	3	20, 00	2 12	3 2	2	2 5	3	53	1		36	7	7	7 7	38		39	
		+	0 2		\perp	-	+	Н	0 0	0 0	3 0	0 3	0 0	3 6	3	3	2 6	2 0	3	3	3 3	2 6	3 3	0 3	2 6	3 0	3	2 6	3 0	3	0	0 0	0 3	7 3	2 K	3 5	5	5 5	3	9 0	1	2 3	ε τ ε τ	3 6	8 3	9 2	- 6	Ĥ	2 0	-
H=22 FT	11. I	*	000	+			+	H	o c	0	0		0 0	+		1	0.0	+	H	Н		0 0	+	Н	5 C	o	o ·	5 C	6	0.0	_	o c	H		2 0	2 4	2	2 2	2	2 4	J W	3.	W 4	2 6	3.6	ω, _z	t 4	4.	4. 7.	5
		- -	0 %	+	1		1	H	4 5	+	Н	-	4 5	+	H	+	55	+	\vdash	Н	_	64	+	Н	+	73	75	7/6	79	2	- 82	8 8	95	97	5 5	H		107		113	1	120	122	Ľ	129	13,5	13 5	140	150	_
FT WIDT	- L	S	0 5			_	\perp	П	30	117	11	- 7	30	1.7			205	1.,	Ľ			2000	_	30	3 5	300	30	2 5	8 8	30	30	30	33	333	0 2	34		34	34	34	1.7		35	1.7	35	36	36	36	38	
		*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.0	2.1	2.2	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.7	3.4	3.5	3.7	3.8	3.9	4	4.2	4 4 5 7	4.6	4.8	4.0 6.1	5.3		0.0	
WIDTH=20	101	S	0 %	29	30	33	34	36	37	40	5 14	42	4 4 7 4	46	48	49	200	53	55	99	63	64	89	69	7,7	74	9/	× &	8 2	83	82	8 8	91	93	62	66	101	105	107	109	13	115	117	122	124	127	132	135	0 4	
0	5	S	0 %	28	28	28	28	28	28	28	78	28	28	28	28	28	28	28	28	28	30	200 %	31	30	2 5	315	31	2 5	31	31	31	32	32	32	32	32	33	33	33	33	33	33	33	34	34	34	35	35	36	
FT	7L 515	>	0.0	2.1	2.1	2.2	2.2	2.3	2.3	2.4	2.4	2.5	2.5	2.6	2.6	2.7	7.7	2.8	2.9	2.9	3.0	3.0	3.1	3.2	2.5	3.3	3.4	ر د ک	3.6	3.7	3.8	6.5	0.4	4.1	4 4 7 4	4.4	4.5	4.6	8.4	6.4	5.1	5.2	5.3 7.3	5.6	5.8	5.9	6.3	6.5	0.0	
∞	0 0	1 (0	0 %	59	59	59	59	59	50	59	59	59	59	59	59	59	50	59	59	59	09	62	65	99	80 5	7.	73	37	78	80	82	83	87	83	9 %	94	96	100	102	104	90	110	112	117	119	122	127	130	139	
-MIDTH=		S	0 %	52	54	50	48	46	4 4 7	t +	40	39	37	35	34	33	32	31	30	29	29	29	29	29	202	29	30	2000	300	30	30	30	30	31	S 15	315	31	15 5	31	32	32	32	32	33	33	33	33	34	35	1
-		F(%)	S C	2.1	2.2	2.4	2.5	2.6	2.7	2.9	3.0	3.1	3.2	3.4	3.5	3.6	ر. م	3.9	4.0	4.1	4.2	2. 4 2. 4	4.5	4.6	7. 4 0. 4	6.4	5.0	- 0 6	5.3	5.4	5.5	5.6	5.8	5.9	0.0	6.2	6.3	6.5	9.9	ν. α	0.0	7.0	7.7	7.3	7.4	7.5	7.7	7.8	». %	
DESIGN	-20	RADIUS(FT)	1800	1148	1090	987	941	899			759		701	650	626	604	582	543	524	909	489	473	442	427	415	385	372	345	332	320	308	297	276	266	238	240	232	225	209	202	189	183	176	164	158	152	139	132	108	
																T	R	_ 1Д	//	<u> </u>	Т	10	 N		CI	JF	<u>۲</u>	/ F	- <		_	F	 21	JR	Α														SF	PECIF REFE

20 MPH DESIGN SPEED

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REV. 3/03 802.34

		LS	_ M	2	_∞	0	N 4	ي .	00		3	2	_	л ,	- ~	2	· 0	0	۸,	4 (0 00		3	2	_	D =	- m	Ō.	∞		4	9	_∞ <	2 10	2	- 0	2 5	_ا	ဂ္ကဏ္ဏ	0	2	4 (4	000	o	ا رَب	ت ا ت	. o	1.5	r) i	ρ (α <u>ς</u>	170	2
AMP.	18 FT	\vdash	0 4.3			-	5 5			9	5 63	\dashv		69		2	7		+	+	8 8	+	36	-	6 6	2 6 2 6	5 5	105	108	= =	11	= :	2 18	123	125	120	13 12	5 13.	5 5	140	142	144	2 42	15	\exists	15.	+		5 163	168	Н	172
WIDTH	_	\sqcup	0 4.3	+		+	2 4 2 4	+		43		\dashv		+	0 4 5	╀	H		+	4 6	+	+	Н	43	4	4 4	4	4	4 4	t 4	4.7	4	4 4	4	4	4 4	4	43	4 4	4	4	4 4	4	43	\dashv	4 4 5	+		4	+	43	43
INTERCHANGE RAMPS WIDTH	16 FT		0 04		\dashv	_	20 48	+		99	58	\dashv	-	+	208	+	ŀ.		1	0 0	+	84	98	88	8 8	92	96	86	9 5	104	106	108	5 3	114	116	118	122	124	126	130	132	134	138	140	-	14 4	Ŧ.	<u> </u>	152	+	Н	160
Ĭ	_	Ĭ	⊃ ⁴	\perp	\dashv	-	0 4 0	+	-	40		\dashv	+	04	4 Q	╀	\vdash	_	+	4	4 0	40	40	40	4 0	4 4	4	40	0 4	4 6	40	40	0 4	4	40	0 4 0	4 6	40	0 4	4 0	40	04	4	40	\dashv	04	4	4	+	4 0	Н	40
8 FT	12.	> (5 0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	2.0	2.4	2.4	2.6	2.8	3.2	3.4	3.6	D.4 7	4	5
WIDTH=48 H)	2 @	LS.	2 C	54	57	9	62	67	70	72	75	78	80	83	20 00	06	93	96	8	<u> </u>	106	108	111	114	91	2 3	124	126	129	134	137	139	142	147	150	152	157	160	162	168	170	187	1961	198	203	207	216	221	225	152	243	254
WIC		R (5,0	52	52	52	52	52	52	52	52	52	52	22	52	52	52	52	25	52	5,5	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	56	57	57	58	28	59	29	09	9 5	62	64
FT ANE V		≥ (0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	9 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.3	2.8
WIDTH=24 FT LANES AT LANE	1@ 12	LS	٥ ۲	36	38	40	43	45	47	48	50	52	54	22	20	09	62	64	99	۵ م	71	72	74	9/	78	<u>د</u> ک	83	84	98	806	91	93	92	98	100	102	105	107	108	112	114	115	119	120	122	124	127	129	131	146	149	154
		R)	ر الم	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	رئ 12	35	35	35	35	35	3,5	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	20 20	38	39
F I SER OF		> 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.2	2.2	2.3	2.4	2.6	2.7	2.8	2.0	3.3	3.8
WID I H= ZZ NTS (NUMB	10 11	LS	2 C	33	35	37	80 04	2 14	43	44	46	48	49	ر 2	54	55	57	59	00 5	79	55	99	89	70	7 :	2/ 2/	76	77	79	0 6	84	85	0 0 0 0	8 8	92	95	96	86	99	103	104	115	120	121	124	126 128	131	133	135	2021	143	148
ENTS		S G	2 5	32	32	33	32	32	32	32	32	32	32	32	32	32	32	32	32	22	32	32	32	32	32	22	32	32	32	32	32	32	32	32	32	52	32	32	32	32	32	35	35	35	35	35	36	36	36	26	37	37
WIDTH=ZO FI WIDTH=ZZ FI SOFTWARE EQUIVALENTS (NUMBER		> 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.0	2.1	2.2	2.2	2.4	2.4	2.5	2.6	2.7	2.7 0 0	2.9	2.9	3.0	3.2	3.2	3.3	4. د	3.6	3.7	3.8	0.4	4.3	8.4
4-20 FT ARE EQ	1@ 10'	LS.	2 0	30	32	33	36	38 28		40	42	43	45	46	δ 4 0	50	52	53	55	200	00 00	9	62	63	65	9 00 00 00	69	70	79	- 63	84	98	8 8	92	93	95	66	101	105	103	108	11 11	15	116	119	121	125	127	130	135	138	142
WIDTH-20 SOFTWARE	-		2 0	29	29	29	239	29	29	29	29	29	29	53	5000	29	29	29	29	67 6	5000	29	29	29	23	500	29	29	32	32	32	32	32	33	33	55	33	33	33	33	33	34	34	34	34	34	34	34	35	35	Н	36
DESIGN 3			0.0		2.0	2.0	2.1	2.1	2.1	2.2	2.2	2.2	2.3	5.5	5 4 5 4	2.4	4.	5.5	5.5	9.0	0 6	2 /	7.7	7.2	ω c	Σ 0	0 0	6.9	0.0	3.0	3.1	5.2	2.5	5.4.	5.4	5.5	2.6	5.7	/. a	0.0	6.5	0	- 2	1.2	1.3	4.4	4.6	7		5.0	5.3	∞
<u>∞</u>	1@ 9'		7 90	+	+	1	4 4 4 7	+		74 2	74 2	\dashv		74	74 7	74	H	74 2	74	4 / 4	74	74	74 2	74 2	47	74 7	747	75 2	75	// 6/	80	82	86 5	88	89	91	95	97	38	102	104 3	106	100	111	\dashv	118 4	+	\vdash		120	+	
-HLQIM	-		0 26	+	89	65	79	57	55	53	52	20	8 1	7 4 7	C 4 4 4	43	42	40	39	200	2 2	36	35	34	53	3 5	31	31	202	2 5	31	15	2 2	212	31	12 12	22	32	2 2 2	32	32	32	32	32	33	53	3 53	33	53	27 45	Н	
		Н) NC		2.2		2.4				2.9 5			4	3.4		3.6		3.8	1	0.4	1.		4.4	5.4	0.4	. 8.4	6.4	5.0	5.2	5.3	5.4	2.5	5.7	5.8	5. G	6.1	6.2	6.5	6.5	6.6	6.7	0.0	7.0	7.1	7.2	4.	7.5	7.6		7.9	
DESIGN VELOCITY	52						\dagger												+	\dagger				+		\dagger			$^{+}$					t			+								H	+	1	-		$^{+}$	Н	
DES		RADIUS(FT)	2500	1664	1579	1502	1366	1306	1250	1198	114 §	1104	1061	1021	985	914	882	852	823	760	744	720	969	674	652	632	592	573	555	519	502	485	468	437	423	409	383	371	359	336	326	315	295	286	276	267 258	248	239	229	209	196	172

25 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

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802.35

TC	-5.01																		_			_						_					_			_								_	_		_	_	_
	PS	FT	LS	45	48	52	54	57	19	63	99	802	72	75	77	2 2	84	98	8 6	93	98	26	102	104	108	=	113	711	120	122	126	129	133	135	140	142	144	147	151	153	158	160	162	165	169	171	174	176	180
. :	WIDTH	1 ∞ 1	S.	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45
MAX	INTERCHANGE RAMPS WIDTH	FT	LS	43	45	50	52	54	28	09	62	67	69	71	73	77	79	28	88	88	90	92	96	66	101	105	107	11	114	118	120	122	126	128	133	135	137	139	143	146	150	152	154	156 87	160	163	165	167	171
%%	INTER	16.1	R c	43	43	43	43	43	43	43	43	54	43	43	43	5 4	43	4 د د د	5 4	43	43	5 4 7	43	43	43	54	43	2 4 5	43	43	43	43	5 4 3	43	0 4 × 4	43	43	43	43	43	43	43	43	2 4 6	5 4 2	43	43	43	5 4
ٿا د	E		≥ (0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.2	2.4	2.6	2.8	5 M
SING	WIDTH=48 FT H)	0 12	LS.	55	28	63	99	69	- 4/	77	80	85	88	8	93	66	101	401	9 6	112	115	8 5	123	126	129	134	137	140	14.5	148	153	156	161	164	170	172	175	178	183	186	191	194	197	200	224	228	233	238	253
n (]	MIDTH)	2	R 6	55	55	55	55	55	55	55	55	22	55	55	55	55	55	25 25	55	55	55	55	55	55	55	-	\vdash	55	55	55	55	55	55	55	0 5	55	55	55	+	55	55	55	55	22 20 20 20 20 20 20 20 20 20 20 20 20 2	000	. 09	\pm	+	707
(RURAL) USING				+	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	+	0.0	+	0.0	0.0	0.0	\vdash	0.0	0.0		0.0	0.0	+		+	0.0	0.0	+	0.0	0.0	0.0	0.0	0.0		0.0	\vdash	+	0.0		0.0	0.0	0.0	0.0	+	_	
1 1	WIDTH=24 FT LANES AT LANE	1@ 12.			+	42	H	+	50 0	Н	+	57		+	62 0	+	Н	+	. 2.	75 0		2 6	+	Н	98 88	+	\vdash	25.	\Box	+	+	104	+	01:	113	+	Н	119	\vdash	+	28	-	131	355	37	39 C	+	142	+
МРН	WIDTH:	100	+	37 3	V L	1 4	7	7 7	/ L	7	7 7	, ,	7	7	7 7	, /	7	,	, ,	7	7		, 1	7	7 7		~ I	, ,	200	7 7	7 10	7 7	,	1,	, ,	, ,	7 -	7 7	7	7 1	7 7	7	7	\ \ \	, ,	7 1.	, <u>, , , , , , , , , , , , , , , , , , </u>	+	27 1
30	<u></u> ⊢	Н		-	0 0	0 0	0	0 0	0 0	0	0 3	0 0	0 3	0	0 0	0 0	0 3	0 0	2 0	0 3	0 3	0 0	3 0	0 3	00	0 3	0 3	2 0	0 3	00	0 3	0 0	0 0	0 3	0 0	0 0	0 3	0 0	0 3	0 0	2 0	0 3	0 3	0 0	0 -	2 3	5 ,	+	5.0
OF	22 FT JMBER	11.			-	0		+	0.0	Н	-	0.0	+	1	0.0		H	+	0.0	+		2 0.0	+	7 0.0	0.0		\vdash	+	H	0.0		0.0			0.0	+	Н	0.0	+	+	0.0		0	0 0	2 6	0 2.	2 2.	+	+
SPEED	WIDTH=22 FT NTS (NUMBER	1 @ 11	_	+	35	39			4 4 4	Н	+	52	1 54	+	50	+	Н	تَ مُ	29			72		1 2	79		Н	+	68	6 6		95	+	100	104	+	Н	109	+	114	11	ļ.		122	7 5	7 140	\perp	-	15,
1 1	FT WIDTH=22 FT EQUIVALENTS (NUMBER		\dashv	+	34	1			34	ľ	34	1.7	34	\dashv	34	1	34	2 2	34		. ,	34	3,5	34	34	1	Н	34	32	20 20	34	34	34	3,	2 5	34	34	34	$\frac{1}{1}$	3,	34	, ,	34	2 4	9 60	3,		+	2 00
DESIGN				0.0	0.0		0.0	0.0	0.0	0	0 0	0.0	0.0	+	0 0	+	H	0 0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	+	2.0	2.1	2.2	7.7	2.3	2.4	2.5	2.5		2.7	2.8	2.8	2.9	3.1	3.2	ω, r	+	5 6
A DE	WIDTH=20 FT SOFTWARE EQ	1 @ 10	LS	31	32	35	37	38	4 4	43	44	4 4	49	20	52	55	57	200	3 6	63	64	99	69	70	72	75	76	2 0	∞	9 82	94	95	66	101	2 5	107	109	111	115	1	121	123	125	127	132	134	136	139	+
FOR /	0		유 (31	2 2	5 E	31	31	3 15	31	31	<u>ب</u> ک	31	31	2 2	2 5	31	2 5	2 50	31	31	31	2 5	31	2 2	31	31	2 15	2	ي ا	34	34	34	34	24 47	34	35	35	35	35	35	35	35	35	36	36	36	+	200
	PE SIGN		≥ 0	0.0	0.0	0.0	2.0	2.0	2.1	2.1	2.1	2.2	2.2	2.2	2.3	2.3	2.3	4.7	2.4	2.5	2.5	2.5	2.6	2.6	2.7	2.7	2.8	2.8	2.9	2.9	3.0	3.0	. N	3.2	3.0	3.3	3.4	3.5	3.5	3.6	3.7	3.8	3.8	ა 4 ა ⊂	4	4.2	4.3	4.4	5 4
FACTORS	WIDTH= 18 FT	1@9	LS.	28	29	32	88	88	88	88	88	88	88	88	88 8	88	88	20 a	88	88	88	8	88	88	88 88	88	88	20 00 00 00	88	80 83	06	91	95	97	S 5	102	104	106	110	112	116	118	119	122	126	128	131	133	130
F AC	MID		8	28	28	28	74	71	99	63	19	57	55	54	52	49	48	4 4	44	43	42	41	40	39	38	36	36	34	34	33	33	32	33	33	33	33	33	33	33	33	34	34	34	54	34	34	35	35	3,5
l i	<u>.</u> ≻		3	2.0	2.1	2.3	2.4	2.5	2.7	2.8	2.9	3.1	3.2	3.3	4. د ب	3.6	3.7	ν, ν ο	0.4	4.1	4.2	5.4	5.4		V 4 8	6.4	5.0	5.2	5.3	4. C	5.6	5.7 8	5.9	6.0	- 6	6.3	6.4	6.6	6.7	6.8	0.0	7.1	7.2	ر. / 4 /	7.5	7.6	7.7	7.8) C
DESIGN	DESIGN VELOCITY	-30	RADIUS(FT)	2402	2276	2056	1960	1871	1713	1643	1577	1457	1403	1352	1303 1258	1214	1173	1007	1061	1028	995	964	905	877	851	800	775	727	706	684	641	621	583	565	531	515	499	484	455	441	427	400	387	3/4	348	334	320	305	251

REV. 3/03 802.36 TRANSITION CURVES - RURAL 30 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

SPECIFICATION REFERENCE

NOTE: CR, LS & w VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, CR, LS, AND w VALUES.

-35			2	DESIGN SOFTWARE	I COLTWAL		EOHVALENTS	WALENTO	CALLIABED	90	OF ANIES	TV O	JANE -	ANE WINTEN	- 5	2	7/ 11/01#			TOW	
		1@ 9			10 10	- L	2	10 11		2	LANC		2	@ 12	<u> </u>	ω,	3 @ 12	ā.	16	FT	18 FT
E(;;)	S, c	LS	≥ (CR	LS	≥ 0	R)	S o	> 0	S. C	LS	≥ 0	S, c	LS C	≥ 0	8	LS	≥ 0	8	S	R)
2.0	30	30	0.0	33	33	0.0	36	36	0.0	39	39	0.0	29	29	0.0	78	78	0.0	46	46	84
2.1	8 8	32	0.0	33	34	0.0	36	38	0.0	39	41	0.0	59	64	0.0	78	88	0.0	46	20 48	4 8 4 8
2.2	30	32	0.0	33	36	0.0	36	40	0.0	39	43 ع	0.0	59	64	0.0	78	98	0.0	46	50	8 4
	8 8	35	0.0	33	39	0.0	36	43	0.0	33	5 4	0:0	29	52	0:0	78	93	0.0	46	55	48
2.5	83	103	2.0	33	41	0.0	36	45	0.0	39	49	0.0	59	73	0.0	78	101	0.0	46	57	48
2.7	77	103		33	44	0.0	36	48	0.0	39	53	0.0	29	79	0.0	78	105	0.0	46	61	48
2.8	74	103	2.0	33	46	0.0	36	50	0.0	39	55	0.0	59	82	0.0	78	109	0.0	46	64	8 4 8
2 0	7/	10.5	2.7	33	4 4	0.0	2 2	54	0.0	30) o	0.0	5 G	0 80	0.0	0 00	11	000	40	200	0 4 6
3.1	67	103	2.1	33	50	0.0	36	55	0.0	39	9	0.0	59	06	0.0	78	120	0.0	46	70	48
3.2	65	103	2.1	33	52	0.0	36	57	0.0	39	62	0.0	59	93	0.0	78	124	0.0	46	73	48
5.5 4.5	89 19	103	2.2	33	55	0.0	36	59	0.0	95 95	64	0.0	50 00	96	0.0	28 /82	132	0 0	46	77	8 4 8
3.5	59	103	2.2	33	57	0.0	36	63	0.0	39	89	0.0	59	102	0.0	78	136	0.0	46	79	84
3.6	28	103	2.2	33	59	0.0	36	64	0.0	39	2/2	0.0	59	105	0.0	78	140	0.0	46	82	48
N 20	55	103	2.3	33	09	0.0	36	99	0.0	259	74	0.0	20	108	0.0	ω ×	444	0 0	46	84	8 4 8
3.9	53	103	2.3	33	63	0.0	36	70	0.0	39	76	0.0	59	114	0.0	78	151	0.0	46	88	48
6:	52	103	2.3	33	65	0.0	36	F :	0.0	39	8 2	0.0	59	117	0.0	78	155	0.0	46	91	84 9
4.1	50	10.5	2.4	33	/9	0.0	36	75	0.0	39	80	0.0	59	120	0.0	20 00	15.3	0.0	46	95	x 4 x 0
	8 4	103	2.4	33	70	0.0	36	77	0.0	39	84	0.0	59	125	0.0	78	167	0.0	46	97	84
	47	103	2.4	33	71	0.0	36	79	0.0	39	98	0.0	59	128	0.0	78	171	0.0	46	001	48
t 4	4 5	103	2.5	33	75	0.0	36	82	0.0	39	8 6	0.0	20 00	134	0.0	0 8	179	0.0	46	104	φ φ φ φ
4.7	44	103	2.5	33	9/	0.0	36	84	0.0	39	91	0.0	59	137	0.0	78	182	0.0	46	106	48
8 0	43	103	2.6	33	8 0	0.0	36	86	0.0	39	93	0.0	59	140	0.0	8 2	186	0.0	46	109	φ 4 α
	42	103	2.6	33	81	0.0	36	89	0.0	39	97	0.0	59	146	0.0	78	194	0.0	46	113	48
5.1	41	103	2.6	33	83	0.0	36	16	0.0	39	66	0.0	29	149	0.0	78	198	0.0	46	115	48
5.2	39	103	2.7	33	84	0.0	36	93	0.0	39	101	0.0	59	151	0.0	78	202	0.0	46	118	8 4 8
5.4	39	103	2.7	33	88	0.0	36	96	0.0	39	105	0.0	59	157	0.0	78	210	0.0	46	122	48
5.5	38	103	2.8	33	89	0.0	36	88	0.0	39	701	0.0	59	160	0.0	78	213	0.0	46	124	48
5 2	37	103	0.7	33	92	0.0	36	102	0.0	39	11 5	0.0	59	166	0.0	0 82	221	0.0	46	129	0 4 6
5.8	36	103	2.9	33	94	0.0	36	103	0.0	39	113	0.0	59	169	0.0	78	225	0.0	46	131	48
0.0	35	103	2.9	33	96	0.0	36	105	0.0	39	115	0.0	59	172	0.0	8/ 8/	229	0.0	46	133	φ 4 α
0.1	35	104	3.0	36	109	2.0	36	109	0.0	39	119	0.0	59	178	0.0	78	237	0.0	46	138	48
6.2	34	105	3.0	36	110	2.0	36	110	0.0	39	120	0.0	59	180	0.0	78	240	0.0	46	140	48
6.4 5.4	35	109	3.1	36	115	2.1	36	114	0.0	39	122	0.0	59	186	0.0	28 / 82	244	0.0	46	14.2	φ φ φ
6.5	35	112	3.2	36	117	2.2	36	116	0.0	39	126	0.0	59	189	0.0	78	252	0.0	46	14.7	48
9.9	35	£ £	3.2	37	119	2.2	36	21 13	0.0	39	128	0.0	50	192	0.0	20 00	256	0.0	46	149	8 4
8.9	35	11	3.3	37	123	2.3	36	121	0.0	39	132	0.0	59	198	0.0	78	264	0.0	46	154	8 4 8
6.9	35	119	3.3	37	125	2.3	36		0.0	39	134	0.0	59	201	0.0	78	268	0.0	46	156	48
0./	35	121	3.4	37	127	2.4	36	125	0.0	39	138	0.0	29	207	0.0	20 00	275	0.0	46	150	φ 4 8 8
7.2	35	125	3.5	37	131	2.5	36	128	0.0	39	140	0.0	59	210	0.0	78	279	0.0	46	163	48
ر: د ک	35	127	3.5	2/2	155	2.5	36	130	0.0	250	142	0.0	20 0	212	0.0	20 20	283	0.0	46	165	20 0
7.5	35	132	3.7	37	138	2.7	36	134	0.0	39	146	0.0	59	218	0.0	83	308	2.1	46	170	2 4 8
7.6	35	133	3.7	37	140	2.7	36	135	0.0	39	148	0.0	59	221	0.0	83	312	2.1	46	172	48
/:/	36	138	8.8	38	142	2.8	36	137	0.0	39	150	0.0	29	224	0.0	84	325	2.7	46	174	8 4 8
7.9	36	141	4.0	38	147	3.0	39	153	2.0	39	153	0.0	64	249	2.0	82	332	3.0	46	179	48
χ Ο.	уę	144	4.5	28	[5]	5.5	04	15/	7.3	59	CCL	0.0	69	228	7.0	αç	344	ن. ن	46	100	84

TRANSITION CURVES - RURAL 35 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03

-5.01		MPS	FT	LS C	252	57	09	65	67	6 6	72	ψ Ω	80	83	88	90	96	98	10.5	106	108	114	116	121	124	129	132	134	139	142	147	150	155	157	162	165 168	170	175	178	180 283	186	188	193	196	201	204	207
		INTERCHANGE RAMPS	ω	8	252	52	52	52 52	52	52 52	52	52 52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52 52	52	52	52	52	52	52	20
		CHANGE	FT	LS	64	54	56	59	64	99	89	73	9/	80 08	83	85	06	93	95	100	10.5	107	110	114	117	122	124	127	131	134	139	141	146	148	153	158	160	165	168	170	175	177	182	185	190	192	ž Ž
	MAX.	INTER	16	R) c	64	49	49	49	49	49	49	49	49	49	49	49	49	49	49	49	64	49	49	64	49	64	46	6 4 0	49	49	49	64	49	49	49	64	49	49	49	49	49	49	49	49	49	49	υ -
				≥ 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0 0	0.0	2.1	ر. د.د
	E= 8	WIDTH-72 FT	@ 12.	S c		92	\vdash	100	\vdash	-	_	120	\vdash	133	+	145	+		162	+	+	2 10	187	+		207	+	216	224	228	236	240	249	253		-	274	282	_	290	+	_	+	315	323	346	202
	16	WIDT	ъ	8 0	833	83		83	\vdash	+	++	+	Н	832	2 2		3 6	+	83	2 0	833			83		83	_	, 833 73	83	833	83	83	83	83				83		83	\Box	+	83	83	83	88 6	
	NSING	<u>-</u>		> C	+	_	\vdash	0.0	\vdash	_	\vdash	+	\vdash	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	+	\vdash	0.0	0.0	0.0	0.0	0.0	+	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	\vdash	+	+	0.0	0.0	0.0	- -
		WIDTH-48 FT	Ø 12'	LS C		99		78 (_		+		001	+	109 (15	2	22 0	28 (331	+	-	146	149 (2 92	\vdash	162 (0 00	171 (+	180	+	90	\vdash	-	205	2 8	\vdash	218 (24 (27	33 (36 (43 (46	200
	(RURAL)	WIDTH		S C	+	63 6	\vdash		H	63 8	Н	20 20	53	5 5	5.3	63 10	5.5	1	5 5	53	53 2	5.53		63	55 2	2 12	53	5 5	3 5	5 5	5 55	55 52	5 15	5 5	53	53 2	53.5	63 2	H	63 2	3 2	2 2	2 2 2	5 5	2 2	2 2	2 2
				* 0	++	+	\vdash	0.0	\vdash	_	\perp	0 0	0.0	0 0	0	00	0	9	0 0	0.	0.0	0	0 0	+	0.0	0 0	0,0	0.0	0.0	0.0	0	0.0	0	0 0	0.	0 0	0.0			0 0	0	0 0	0 0	0 0	0	0.0) - -
	МРН	WIDTH-24 FT	12		+	+	\vdash	+	\vdash	0 0	8	0 0	0	0 0	0.0	0.0	0 2	0	7 0	0	0 0	0.0	+	+	\vdash	4 4	9	∞ c	0.0	0 0	0 0	0 0	5 0	0 0	0	3 0		+		+	H	0 0	+ 9	∞ c	H	4 %	-
	40	DIH.	0	S C	<u> </u>	+	Н			<u> </u>	Š	9 9	9	2 0	0	7 7	7	2	∞ α	0 00	00 a	9 6		88	100	9 2	2 :	1 9	= ==	===	= =	2 2	12	2 2	13	51 5	13.5	141	14.3	145	149	را ر	5 5	री द	162	164	2
	님	− ĕ	<u> </u>	8 0	++	+	Н	42	\vdash	+	\sqcup	+	4 2	4 4	4	4 4	4,	4.2	4 4	4 2	4 4	4	_	42	4 4	4 4	4	4 4	4 4	4 4	4	4 4	4	4 4	4	4 4	4	4 4	4 2	4 4	4	4 ,	4 4	4 4	0 4	0 0	ţ
	- QE	a . I	-	> 0	+	_	\vdash	0.0	+	+	++	+	+	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		_	+	\vdash	0.0	0.0	0 0	0.0	0.0	+	0.0	+	0.0	0.0	0.0	++	0.0	0.0	0.0	0.0	0.0		0.0	0	0 0	7
	SPEED	WIDTH-22	10 11	LS C	82	42	44	46	20	52	54	55	29	61	65	67	7 2	73	74	78	88	84	86	8 8	92	3 5	97	99	103	105	109	110	114	118	120	122	126	129	131	13.5	137	139	143	145	148	150	100
	Z.		5	당 c	-	38 88	38	38 88	38	38 38	38	38 88	38	38 38	38	38 %	38	38	38 38	38	38	38	38	38	38	388	38	38	38	82 82	38	38	38	38 38	38	38	38 2	38	38	38 38	38	38	38	38 38	38	38	47
	DESIGN	FT (≥ 0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.1	2.1	2.2	2.3	2.3	2.4	2.5	2.6	2.7	ر ک
	A DI	WIDTH-20 FT	1@ 10	S	35	38	40,	44	45	47	49	20	54	56	59	61	64	99	80 00	71	73	9/	28	8	83	8 0	88	99	94	95	66	001	104	106	109	111	126	130	132	134	139	141	145	150	152	155	2
	FOR ,		5	R c	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	39	39	39	39	39	39	39	39	39	40	5
		8 FT N	2	≥ 0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.0	2.1	2.1	2.1	2.2	2.2	2.2	2.2	2.3	2.3	2.4	2.4	2.4	2.5	2.5	2.5	2.6	2.6	2.7	2.7	2.7	2.8	8.2	2.9	2.9	3.0	3.1	3.1	3.2	3.3	3.3	4 4	3.5	3.6	3.7	4 ⊃
	ACTORS	WIDTH- 18 FT	1@ 9'	LS	32	35	36	39	14	42	117	117	117	117	11	117	117	117	11 11	117	117	117	11 2	11	117	1	117	11,	117	117	11	711	117	117	117	717	120	124	126	128	133	135	139	141	146	148	701
	Ĭ	MID	,	8 0	32	32	32	52 32	32	32	84	78	9/	74	69	67	64	62	09 05	58	56	54	52	20	49	47	46	45	4 4	43	42	14 0	39	38	38	37	37	37	37	37	37	37	38	38 88	38	38	ဂ္ဂ
	ഥ			E(;;)	2.0	2.2	2.3	2.5	2.6	2.7	2.8	3.0	3.1	3.2	3.4	3.5	3.7	3.8	0.0	4.1	2.4	4	6.5	4.7	8. 6	5.0	5.1	5.2	5.4	5.5	5.7	5.8 0	6.0	6.2	6.3	4.9	9.0	8.9	6.9	7.1	7.2	7.3	7.5	7.7	7.8	0.0	
	DESIGN	DESIGN	-40	F	П	3603		3271	2990	2865	2748	2640	2443	2354	2190	2115	1977	1913	1852	1739	1686			1452	1411	1332	1294	1258		1154	П	1058		971				794		†	703	681	635	587	260		

REV. 3/03 802.38 TRANSITION CURVES - RURAL 40 MPH DESIGN SPEED VIRGINIA DEPARTMENT OF TRANSPORTATION SPECIFICATION REFERENCE

10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10<	W CR LANCEL 0.0 0 0 0.0 0 0 0 0.0 0 0 0 0 0.0 45 45 0 0 0.0 45 47 0 0 0.0 45 47 0 0 0.0 45 54 0 0 0.0 45 56 0 0 0.0 45 60 0 0 0.0 45 67 0 0 0.0 45 67 0 0 0.0 45 67 0 0 0.0 45 74 0 0 0.0 45 74 0 0 0.0 45 74 0 0 0.0 45 85 0 0 0.0 45 83 0 0 <t< th=""><th>CR LS 40 CO CO</th><th>CR LS</th><th> C N N N N N N N N N</th><th>1.1 T.1 T.1 T.1 T.1 T.1 T.1 T.1 T.1 T.1</th></t<>	CR LS 40 CO	CR LS	C N N N N N N N N N	1.1 T.1 T.1 T.1 T.1 T.1 T.1 T.1 T.1 T.1
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45 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03

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TRANSITION CURVES - RURAL 50 MPH DESIGN SPEED

REV. 3/03

802.40

VIRGINIA DEPARTMENT OF TRANSPORTATION

SPECIFICATION REFERENCE

55 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03

802.41

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4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.1 0.0 4.2 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 <td></td> <td>4030 3</td> <td>ο ο 4 4</td> <td>7 2</td> <td>9 0</td> <td>45</td> <td>+</td> <td>0.0</td> <td>94 94</td> <td>93</td> <td>0.0</td> <td>54</td> <td>7 4</td> <td>0.0</td> <td>000</td> <td>156</td> <td>0.0</td> <td>10/</td> <td>208</td> <td>0.0</td> <td>63 1</td> <td>07.0</td> <td>7 2 2</td> <td></td>		4030 3	ο ο 4 4	7 2	9 0	45	+	0.0	94 94	93	0.0	54	7 4	0.0	000	156	0.0	10/	208	0.0	63 1	07.0	7 2 2	
	4.1 4.0 8.2 0.0 4.5 9.1 0.0 0.0 9.1 1.0 0.0 9.1 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	3911 4	0	0 0	0.0	7 45	\vdash	0.0	49	86	0.0	54	_	0.0	80	160	0.0	107	214	0.0	63 12	9 97	7	4
4.2 4.0 84 0.0 4.5 0.0 4.5 0.0 9.0 1.2 0.0 80 0.0 4.5 0.0 4.5 4.0 84 0.0 4.5 9.0 0.0 4.5 0.0 9.0 1.5 0.0 9.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 1.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	4.3 4.0 8.9 0.0 4.9 10.5 0.0 5.4 1.2 0.0 5.9 1.0 4.9 10.5 0.0 5.4 1.0 0.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 </td <td>3798 4</td> <td>4</td> <td>0 8</td> <td>\vdash</td> <td>0 45</td> <td>Н</td> <td>0.0</td> <td>49</td> <td>101</td> <td>0.0</td> <td>54</td> <td>110</td> <td>0.0</td> <td>08</td> <td>164</td> <td>0.0</td> <td>107</td> <td>219</td> <td>0</td> <td>63 12</td> <td>9 67</td> <td>7 13</td> <td>[2]</td>	3798 4	4	0 8	\vdash	0 45	Н	0.0	49	101	0.0	54	110	0.0	08	164	0.0	107	219	0	63 12	9 67	7 13	[2]
4.4 4.0 88 0.0 4.5 1.0 5.4 1.0 5.0 1.0 4.9 1.0 5.4 1.0 0.0 4.5 4.0 88 0.0 4.5 1.0 0.0 54 1.0 0.0 80 1.6 0.0 9.0 4.6 4.0 9.0 0.0 4.5 1.0 0.0 80 1.6 0.0 1.0 2.2 0 0.0 1.0 0.0 2.0 9.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	4.4 4.0 88 0.0 4.5 98 0.0 4.4 108 0.0 4.5 108 0.0 4.5 108 0.0 4.5 118 0.0 80 176 0.0 10 2.5 4.0 4.0 10 0.0 4.5 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 10 0.0 </td <td>3587 4</td> <td>2 5</td> <td>+</td> <td>+</td> <td>45</td> <td>+</td> <td>0.0</td> <td>9 4</td> <td>103</td> <td>0.0</td> <td>5 4</td> <td>112</td> <td>0.0</td> <td>00 00</td> <td>168</td> <td>0.0</td> <td>107</td> <td>224</td> <td>0 0</td> <td>63 1.</td> <td>32 6 35 6</td> <td>4 4</td> <td>0 4</td>	3587 4	2 5	+	+	45	+	0.0	9 4	103	0.0	5 4	112	0.0	00 00	168	0.0	107	224	0 0	63 1.	32 6 35 6	4 4	0 4
4.5 4.0 9.0 0.0 4.5 1.0 0.0 4.1 0.0 0.0 4.1 0.0 0.0 4.6 0.0 0.0 1.5 0.0 0.0 4.6 0.0 0.0 4.0 0.0 0.0 4.0 0.0 0.0 4.0 0.0 4.0 0.0 0.0 4.0 0.0 0.0 4.0 0.0 0.0 4.0 0.0 0.0 4.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 <td>4.5 4.0 9.0 9.0 1.0 9.0 9.0 9.0 1.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0<td>3488 4</td><td>4</td><td>Н</td><td>+</td><td>7 45</td><td>+</td><td>0.0</td><td>49</td><td>108</td><td>0.0</td><td>54</td><td>2 2</td><td>0.0</td><td>8 8</td><td>176</td><td>0.0</td><td>107</td><td>235</td><td></td><td>63 1.</td><td>39 6</td><td>4</td><td><u> -</u></td></td>	4.5 4.0 9.0 9.0 1.0 9.0 9.0 9.0 1.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 <td>3488 4</td> <td>4</td> <td>Н</td> <td>+</td> <td>7 45</td> <td>+</td> <td>0.0</td> <td>49</td> <td>108</td> <td>0.0</td> <td>54</td> <td>2 2</td> <td>0.0</td> <td>8 8</td> <td>176</td> <td>0.0</td> <td>107</td> <td>235</td> <td></td> <td>63 1.</td> <td>39 6</td> <td>4</td> <td><u> -</u></td>	3488 4	4	Н	+	7 45	+	0.0	49	108	0.0	54	2 2	0.0	8 8	176	0.0	107	235		63 1.	39 6	4	<u> -</u>
4.7 4.0 9.0 4.9 11.5 0.0 4.1 9.0 0.0 4.9 11.5 0.0 4.1 9.0 0.0 4.2 1.0 0.0 4.9 11.5 0.0 4.1 1.0 0.0 4.9 11.5 0.0 5.4 12.6 0.0 19.2 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0	4.7 4.0 54 0.0 4.7 1.0 0.0 4.0 0.0 0.0 4.0 0.0 0.0 4.0 0.0 4.0 4.0 0.0 4.0 4.0 0.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	3394 4	رن 4 م	ر ا م	0.0	0 45	100	0.0	64	110	0.0	54	120	0.0	080	176	0.0	107	240	0.0	63 1/	12 6	7 5	0 5
4.8 4.0 96 0.0 4.5 10.0 4.9 11.0 5.0 4.0 96 0.0 4.5 10.0 0.0 4.0 96 0.0 4.5 10.0 0.0 4.0 96 0.0 4.0 96 0.0 4.0 10.0 0.0 4.0 10.0 0.0 4.0 10.0 0.0 4.0 10.0 0.0 4.0 10.0 0.0 0.0 10.0 10.0 2.0 4.0 10.0 0.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0 2.0 10.0	4.8 4.0 96 0.0 4.5 107 0.0 49 118 0.0 96 0.0 4.5 107 0.0 49 120 0.0 44 124 0.0 96 0.0 4.5 100 0.0 49 100 0.0 49 100 0.0 49 100 0.0 40 100 0.0 40 100 0.0 40 100 0.0 40 100 0.0 40 100 0.0 80 204 0.0 0.0 80 204 0.0 0.0 100 0.0 100 0.0 100 0.0 100 0.0 100 0.0 100 100 0.0 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 10	3216 4	5 V	6 6	+	7 45	105	0.0	64	115	0.0	54	126	0.0	8 8	188	0.0	107	251	0.0	63 14	9 9	7 5	4 7
4.9 4.0 98 0.0 4.5 1.5 0.0 54 1.5 0.0 54 1.5 0.0 54 1.5 0.0 99 0.0 4.9 1.5 0.0 54 1.36 0.0 90 0.0 4.5 1.0 0.0 4.5 11.4 0.0 4.5 11.4 0.0 4.5 11.4 0.0 4.5 11.4 0.0 4.5 11.6 0.0 4.5 11.6 0.0 4.5 11.6 0.0 4.5 11.6 0.0 4.5 11.6 0.0 4.5 11.6 0.0 4.5 11.6 0.0 4.5 11.2 0.0 5.4 13.9 0.0 80 20.8 0.0 10.7 22.8 0.0 6.0 10.7 22.8 0.0 10.0 20.9 0.0 4.7 10.0 80 20.8 0.0 80 20.8 0.0 80 10.0 20.0 10.7 22.8 0.0 10.7	4.9 4.0 9.0 0.0 4.9 12.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 13.0 0.0 54 10.0 10.0 22.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0 0.0 10.7 25.0	3133 4	Н	6	9.0		\vdash	+	49	118	0.0	54	128	0.0	80	192	0.0	107	+	0.0	63 1	51	7 16	0
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5.2 4.0 104 0.0 45 128 0.0 54 139 0.0 50 208 0.0 107 278 0.0 63 4 5.2 68 176 2.4 45 116 0.0 49 128 0.0 54 139 0.0 80 208 0.0 107 278 0.0 63 18 0.0 107 278 0.0 63 18 0.0 107 288 0.0 107 288 0.0 63 18 0.0 107 288 0.0 63 18 0.0 107 288 0.0 63 18 0.0 107 288 0.0 63 18 0.0 64 18 0.0 60 18 0.0 80 20 0.0 18 0.0 80 20 0.0 18 0.0 80 20 0.0 18 0.0 80 20 0.0 10 <td>5.2 40 104 106 49 128 0.0 54 139 0.0 80 208 0.0 107 278 0.0 63 138 0.0 80 208 0.0 107 278 0.0 63 138 0.0 80 208 0.0 107 278 0.0 63 18 5.3 68 176 2.4 45 116 0.0 49 128 0.0 80 208 0.0 107 228 0.0 63 176 0.0 107 288 0.0 63 18 0.0 80 208 0.0 107 228 0.0 63 18 0.0 80 208 0.0 107 288 0.0 63 18 0.0 80 20 80 0.0 107 288 0.0 60 63 18 0.0 80 20 80 0.0 107 288 0.0 <td< td=""><td>2901 5</td><td></td><td>+</td><td>0</td><td>+</td><td>114</td><td>0.0</td><td>49</td><td>125</td><td>0.0</td><td>54</td><td>136</td><td>0.0</td><td>+</td><td>204</td><td>0.0</td><td>107</td><td>272</td><td>+</td><td>) W</td><td>9 00</td><td>15</td><td>. 0</td></td<></td>	5.2 40 104 106 49 128 0.0 54 139 0.0 80 208 0.0 107 278 0.0 63 138 0.0 80 208 0.0 107 278 0.0 63 138 0.0 80 208 0.0 107 278 0.0 63 18 5.3 68 176 2.4 45 116 0.0 49 128 0.0 80 208 0.0 107 228 0.0 63 176 0.0 107 288 0.0 63 18 0.0 80 208 0.0 107 228 0.0 63 18 0.0 80 208 0.0 107 288 0.0 63 18 0.0 80 20 80 0.0 107 288 0.0 60 63 18 0.0 80 20 80 0.0 107 288 0.0 <td< td=""><td>2901 5</td><td></td><td>+</td><td>0</td><td>+</td><td>114</td><td>0.0</td><td>49</td><td>125</td><td>0.0</td><td>54</td><td>136</td><td>0.0</td><td>+</td><td>204</td><td>0.0</td><td>107</td><td>272</td><td>+</td><td>) W</td><td>9 00</td><td>15</td><td>. 0</td></td<>	2901 5		+	0	+	114	0.0	49	125	0.0	54	136	0.0	+	204	0.0	107	272	+) W	9 00	15	. 0
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5.4 66 176 2.4 45 120 0.0 49 132 0.0 54 144 0.0 80 216 0.0 107 288 0.0 65 176 0.0 80 226 0.0 107 284 0.0 65 176 0.0 80 224 0.0 107 284 0.0 65 176 0.0 80 224 0.0 107 284 0.0 65 176 0.0 107 284 0.0 107 284 0.0 65 176 0.0 80 226 0.0 107 284 0.0 65 176 0.0 80 226 0.0 107 284 0.0 65 176 0.0 80 232 0.0 107 284 0.0 65 186 0.0 80 286 0.0 80 286 0.0 107 284 0.0 80 286 0.0 107	5.4 66 176 2.4 45 120 0.0 49 132 0.0 54 144 0.0 80 216 0.0 107 284 0.0 65 4 47 0.0 80 226 0.0 107 284 0.0 65 175 0.0 49 135 0.0 54 160 0.0 80 224 0.0 107 289 0.0 63 176 0.0 107 209 0.0 63 176 0.0 107 210 0.0 107 230 0.0 63 176 0.0 107 230 0.0 63 176 0.0 107 230 0.0 63 176 0.0 107 230 0.0 63 176 0.0 60 60 60 80 226 0.0 107 230 0.0 60 60 60 60 60 60 60 60 60 <t< td=""><td>2759 5</td><td>+</td><td>Н</td><td>+</td><td>4 45</td><td>118</td><td>0.0</td><td>49</td><td>130</td><td>0.0</td><td>54</td><td>142</td><td>0.0</td><td>80</td><td>212</td><td>0.0</td><td>107</td><td>283</td><td>+</td><td>) W</td><td>37 6</td><td>7</td><td>- [-</td></t<>	2759 5	+	Н	+	4 45	118	0.0	49	130	0.0	54	142	0.0	80	212	0.0	107	283	+) W	37 6	7	- [-
5.6 6.2 7.4 4.5 1.25 0.0 4.9 1.50 0.0 5.4 1.60 0.0 0.0 2.24 0.0 0.0 2.9 0.0 0.0 0.0 2.24 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	5.7 6.2 1.7 2.4 4.5 1.25 0.0 4.9 1.25 0.0 54 1.0 0.0 2.2 0.0 0.0 7.2 0.0 5.7 1.0 0.0 0.0 54 1.0 0.0 2.2 0.0 0.0 0.0 5.0 1.0 4.0 1.0 0.0 54 1.0 0.0 2.2 0.0 1.0 2.2 0.0 1.0 2.2 0.0 1.0 2.0 0.0 6.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	2692 5		17	6 2.4	45	120	0.0	49	132	0.0	54		0.0	80	216	0.0	107	288	0.0	63 17	9 02	7 18	0
5.7 6.2 176 2.4 4.5 127 0.0 49 142 0.0 54 152 0.0 80 228 0.0 107 304 0.0 63 18 5.9 61 176 2.5 45 129 0.0 49 142 0.0 54 150 0.0 80 232 0.0 107 310 0.0 63 18 6.9 59 176 2.5 45 136 0.0 64 145 0.0 54 160 0.0 80 240 0.0 107 310 0.0 63 18 6.1 58 176 2.5 45 136 0.0 49 150 0.0 80 244 0.0 107 331 0.0 63 18 6.2 55 176 2.6 45 152 0.0 54 162 0.0 80 246 0.0 10	5.7 62 176 2.4 45 127 0.0 49 162 0.0 54 162 0.0 49 162 0.0 54 162 0.0 49 176 2.5 45 127 0.0 49 142 0.0 54 152 0.0 80 232 0.0 107 310 0.0 63 18 6.0 59 176 2.5 45 134 0.0 49 147 0.0 54 160 0.0 80 240 0.0 107 310 0.0 63 18 6.0 59 176 2.5 45 134 0.0 49 150 0.0 54 160 0.0 80 240 0.0 107 316 0.0 60 58 160 0.0 80 240 0.0 107 316 0.0 60 50 0.0 80 248 0.0 107	2565 5	+	3 (2.7	4 40	125	0.0	2 4 6 4	13.7	0.0	54	+	0.0	000	224	0.0	107	+	0.0	53	0 9/	2 2	4 7
5.8 61 176 2.5 45 129 0.0 49 142 0.0 54 155 0.0 80 236 0.0 107 310 0.0 63 18 6.0 59 176 2.5 45 132 0.0 49 145 0.0 54 160 0.0 80 236 0.0 107 316 0.0 63 18 0.0 107 310 0.0 63 18 6.0 59 176 2.5 45 136 0.0 54 160 0.0 80 240 0.0 107 310 0.0 63 18 6.3 56 57 176 2.6 45 143 0.0 54 162 0.0 80 286 0.0 107 331 0.0 63 18 6.3 55 176 2.6 45 145 0.0 54 174 0.0 </td <td>5.8 61 176 2.5 45 139 0.0 49 142 0.0 54 155 0.0 80 236 0.0 107 310 0.0 63 18 6.0 5.9 6.0 176 2.5 45 132 0.0 49 145 0.0 54 160 0.0 80 240 0.0 107 310 0.0 63 18 6.1 58 176 2.5 45 136 0.0 49 150 0.0 54 160 0.0 80 244 0.0 107 310 0.0 63 18 6.3 56 176 2.6 45 143 0.0 49 152 0.0 54 162 0.0 54 168 0.0 80 244 0.0 107 331 0.0 63 38 6.3 55 176 2.6 45 143 0.0</td> <td>2504 5</td> <td></td> <td>2 17</td> <td>6 2.4</td> <td>4 45</td> <td>127</td> <td>0.0</td> <td>49</td> <td>140</td> <td>0.0</td> <td>54</td> <td>152</td> <td>0.0</td> <td>80</td> <td>228</td> <td>0.0</td> <td>107</td> <td>304</td> <td>0.0</td> <td>63 1</td> <td>9 6/</td> <td>7 19</td> <td>0</td>	5.8 61 176 2.5 45 139 0.0 49 142 0.0 54 155 0.0 80 236 0.0 107 310 0.0 63 18 6.0 5.9 6.0 176 2.5 45 132 0.0 49 145 0.0 54 160 0.0 80 240 0.0 107 310 0.0 63 18 6.1 58 176 2.5 45 136 0.0 49 150 0.0 54 160 0.0 80 244 0.0 107 310 0.0 63 18 6.3 56 176 2.6 45 143 0.0 49 152 0.0 54 162 0.0 54 168 0.0 80 244 0.0 107 331 0.0 63 38 6.3 55 176 2.6 45 143 0.0	2504 5		2 17	6 2.4	4 45	127	0.0	49	140	0.0	54	152	0.0	80	228	0.0	107	304	0.0	63 1	9 6/	7 19	0
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6.1 58 176 2.5 45 136 0.0 54 163 0.0 80 244 0.0 107 326 0.0 63 186 0.0 80 244 0.0 107 331 0.0 63 186 0.0 80 248 0.0 107 331 0.0 63 186 0.0 80 252 0.0 107 331 0.0 63 186 0.0 80 252 0.0 107 331 0.0 63 13 6.4 55 176 2.6 45 143 0.0 64 152 0.0 54 174 0.0 80 250 0.0 107 342 0.0 63 32 0.0 63 32 0.0 63 32 0.0 63 63 32 0.0 63 48 60 60 60 60 60 60 60 60 60 60 <td>6.1 58 176 2.5 45 136 0.0 49 150 0.0 54 165 0.0 80 244 0.0 107 331 0.0 63 18 6.2 57 176 2.5 45 148 0.0 49 152 0.0 54 160 0.0 80 252 0.0 107 31 0.0 63 17 6.4 55 176 2.6 45 143 0.0 49 152 0.0 80 252 0.0 107 342 0.0 63 3 6.5 55 176 2.6 45 145 0.0 49 152 0.0 54 174 0.0 80 256 0.0 107 342 0.0 63 3 3 60 63 3 3 60 63 13 60 63 13 60 63 10 63 <t< td=""><td>2332 6</td><td>0.0</td><td>9 1</td><td>6 2.5</td><td>5 45</td><td>134</td><td>0.0</td><td>49</td><td>147</td><td>0.0</td><td>54</td><td>+</td><td>0.0</td><td>8 8</td><td>240</td><td>0.0</td><td>107</td><td>320</td><td>0.0</td><td>) W</td><td>39 68</td><td>2 2</td><td>. 0</td></t<></td>	6.1 58 176 2.5 45 136 0.0 49 150 0.0 54 165 0.0 80 244 0.0 107 331 0.0 63 18 6.2 57 176 2.5 45 148 0.0 49 152 0.0 54 160 0.0 80 252 0.0 107 31 0.0 63 17 6.4 55 176 2.6 45 143 0.0 49 152 0.0 80 252 0.0 107 342 0.0 63 3 6.5 55 176 2.6 45 145 0.0 49 152 0.0 54 174 0.0 80 256 0.0 107 342 0.0 63 3 3 60 63 3 3 60 63 13 60 63 13 60 63 10 63 <t< td=""><td>2332 6</td><td>0.0</td><td>9 1</td><td>6 2.5</td><td>5 45</td><td>134</td><td>0.0</td><td>49</td><td>147</td><td>0.0</td><td>54</td><td>+</td><td>0.0</td><td>8 8</td><td>240</td><td>0.0</td><td>107</td><td>320</td><td>0.0</td><td>) W</td><td>39 68</td><td>2 2</td><td>. 0</td></t<>	2332 6	0.0	9 1	6 2.5	5 45	134	0.0	49	147	0.0	54	+	0.0	8 8	240	0.0	107	320	0.0) W	39 68	2 2	. 0
6.7 57 1/6 2.5 42 128 0.0 49 152 0.0 54 160 0.0 80 256 100 331 0.0 65 163 0.0 54 162 0.0 54 160 0.0 80 256 0.0 107 342 0.0 63 184 0.0 54 171 0.0 80 256 0.0 107 342 0.0 63 184 0.0 64 154 0.0 54 171 0.0 80 256 0.0 107 342 0.0 63 26 6.5 55 176 2.6 45 145 0.0 49 162 0.0 80 266 0.0 107 342 0.0 63 28 6.7 54 176 0.0 54 176 0.0 80 286 0.0 107 342 0.0 63 28	6.3 5.5 176 2.5 45 180 0.0 80 248 10.7 351 0.0 65 18 6.4 5.5 176 2.6 45 143 0.0 49 152 0.0 54 16 0.0 80 256 0.0 107 342 0.0 63 2 6.5 5.5 176 2.6 45 145 0.0 54 171 0.0 80 256 0.0 107 347 0.0 63 2 6 6.0 107 347 0.0 63 2 6 0.0 107 347 0.0 63 2 0 6 6 3 1 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 <	2277 6	c	2 1	6 2.5	5 45	136	0.0	49	150	0.0	54	\vdash	0.0	08 8	244	0.0	107	326	0.0	. ,	92 6	7 20	4
6.4 55 176 2.6 45 143 0.0 49 157 0.0 54 171 0.0 80 256 0.0 107 342 0.0 63 26 6.5 55 176 2.6 45 145 0.0 49 159 0.0 54 174 0.0 80 260 0.0 107 347 0.0 63 26 6.5 54 176 0.0 80 264 0.0 107 352 0.0 63 28 0.0 107 352 0.0 63 28 0.0 107 352 0.0 63 28 0.0 107 358 0.0 63 28 0.0 107 352 0.0 63 28 0.0 107 352 0.0 63 38 0.0 89 128 0.0 80 280 0.0 80 280 0.0 107 362	6.4 55 176 2.6 45 143 0.0 49 157 0.0 54 171 0.0 80 256 0.0 107 342 0.0 63 2 6.5 55 176 2.6 45 145 0.0 49 159 0.0 54 174 0.0 80 266 0.0 107 347 0.0 63 2 6.7 53 176 2.6 45 149 0.0 54 179 0.0 80 268 0.0 107 352 0.0 63 2 6.8 52 176 2.7 45 162 0.0 54 182 0.0 80 280 0.0 107 352 0.0 63 28 0.0 107 352 0.0 63 28 0.0 107 352 0.0 63 107 362 0.0 63 20 60 63 <td>2173 6.</td> <td>2 K</td> <td>5 17</td> <td>5 2.6 6 2.6</td> <td>5 45</td> <td>140</td> <td>0.0</td> <td>e 4 9</td> <td>154</td> <td>0.0</td> <td>54</td> <td>+</td> <td>0.0</td> <td>000</td> <td>252</td> <td>0.0</td> <td>107</td> <td>336</td> <td></td> <td>63 1s</td> <td>98 6</td> <td>2 2</td> <td>3 0</td>	2173 6.	2 K	5 17	5 2.6 6 2.6	5 45	140	0.0	e 4 9	154	0.0	54	+	0.0	000	252	0.0	107	336		63 1s	98 6	2 2	3 0
6.5 55 176 2.6 45 145 0.0 49 159 0.0 54 174 0.0 80 260 0.0 107 347 0.0 63 2 6.6 54 176 2.6 54 176 0.0 80 264 0.0 107 352 0.0 63 2 6.8 52 176 2.7 45 164 0.0 80 272 0.0 107 363 0.0 63 2 6.9 52 176 2.7 45 164 0.0 54 182 0.0 80 272 0.0 107 353 0.0 63 2 6.9 52 176 2.7 45 154 0.0 49 164 0.0 56 276 0.0 107 352 0.0 63 28 0.0 63 28 0.0 63 28 0.0 63	6.5 55 176 2.6 45 145 0.0 49 159 0.0 54 174 0.0 80 264 0.0 107 347 0.0 65 2 6.6 54 176 2.6 54 176 0.0 80 264 0.0 107 358 0.0 63 2 6.8 5.2 176 2.6 45 164 0.0 54 176 0.0 80 268 0.0 107 358 0.0 63 2 6.8 5.2 176 2.7 45 164 0.0 54 182 0.0 80 288 0.0 107 358 0.0 63 28 6.9 5.2 176 2.7 45 169 0.0 54 184 0.0 80 286 0.0 107 358 0.0 63 28 7.1 50 166 0.0 <td>2122 6</td> <td>4</td> <td>5 17</td> <td>6 2.6</td> <td>5 45</td> <td>143</td> <td>0.0</td> <td>49</td> <td>157</td> <td>0.0</td> <td>54</td> <td>171</td> <td>0.0</td> <td>80</td> <td>256</td> <td>0.0</td> <td>107</td> <td>342</td> <td>0.0</td> <td>63 2</td> <td>01 6</td> <td>7 21</td> <td>4</td>	2122 6	4	5 17	6 2.6	5 45	143	0.0	49	157	0.0	54	171	0.0	80	256	0.0	107	342	0.0	63 2	01 6	7 21	4
6.7 53 176 2.6 45 149 0.0 49 164 0.0 54 179 0.0 80 268 0.0 107 358 0.0 63 2 6.8 52 176 2.7 45 152 0.0 49 167 0.0 54 182 0.0 80 272 0.0 107 363 0.0 63 2 6.9 52 176 2.7 45 152 0.0 49 169 0.0 54 184 0.0 80 276 0.0 107 368 0.0 63 2 7.0 51 176 2.7 45 158 0.0 54 187 0.0 80 288 0.0 63 2 2 174 0.0 54 189 0.0 80 288 0.0 183 0.0 63 2 2 0.0 107 349 0.0	6.7 5.3 176 2.6 4.5 149 0.0 49 164 0.0 54 179 0.0 80 268 0.0 107 358 0.0 63 2 6.8 5.2 176 2.7 45 152 0.0 49 167 0.0 54 182 0.0 80 272 0.0 107 368 0.0 63 2 7.0 51 176 2.7 45 156 0.0 49 174 0.0 54 184 0.0 80 280 0.0 107 358 0.0 63 28 0.0 107 358 0.0 63 28 0.0 107 374 0.0 63 28 0.0 107 374 0.0 63 28 0.0 107 374 0.0 80 286 0.0 107 374 0.0 63 28 0.0 107 374 <t< td=""><td>2072 6</td><td>C 0</td><td>5 17</td><td>0 2.6</td><td>6 45</td><td>- `</td><td>0.0</td><td>64</td><td>159</td><td>0.0</td><td>5.4</td><td>174</td><td>0.0</td><td>08 8</td><td>260</td><td>0.0</td><td>107</td><td>347</td><td>0.0</td><td>63 20</td><td>0.4</td><td>7 2</td><td><u> </u></td></t<>	2072 6	C 0	5 17	0 2.6	6 45	- `	0.0	64	159	0.0	5.4	174	0.0	08 8	260	0.0	107	347	0.0	63 20	0.4	7 2	<u> </u>
6.8 5.2 176 2.7 4.5 152 0.0 4.9 167 0.0 54 182 0.0 80 272 0.0 107 363 0.0 6.3 2 6.9 52 176 2.7 45 154 0.0 49 172 0.0 54 184 0.0 80 280 0.0 107 368 0.0 63 28 7.0 51 176 2.7 45 156 0.0 54 187 0.0 80 284 0.0 107 349 0.0 63 28 0.0 107 349 0.0 63 28 0.0 107 349 0.0 63 28 0.0 107 349 0.0 63 28 0.0 107 349 0.0 63 28 0.0 107 349 0.0 63 28 0.0 107 349 0.0 63 28 <t< td=""><td>6.8 5.2 176 2.7 4.5 152 0.0 49 167 0.0 54 182 0.0 80 272 0.0 107 363 0.0 6.3 2 6.9 5.2 176 2.7 45 164 0.0 49 169 0.0 54 184 0.0 80 280 0.0 107 368 0.0 63 2 7.1 50 176 2.7 49 174 0.0 54 180 0.0 80 280 0.0 107 378 0.0 63 2 7.2 49 176 0.0 54 172 0.0 80 280 0.0 107 378 0.0 63 2 7.3 49 176 0.0 49 174 0.0 54 192 0.0 80 284 0.0 107 384 0.0 63 2 7.3<td>П</td><td>7 5</td><td>3 17</td><td>6 2.6</td><td>3 45</td><td>Н</td><td>+</td><td>64</td><td>164</td><td>0.0</td><td>54</td><td>179</td><td>0.0</td><td>08</td><td>268</td><td>0.0</td><td>107</td><td>358</td><td>0.0</td><td>63 2</td><td>1 2</td><td>7 22</td><td>7 4</td></td></t<>	6.8 5.2 176 2.7 4.5 152 0.0 49 167 0.0 54 182 0.0 80 272 0.0 107 363 0.0 6.3 2 6.9 5.2 176 2.7 45 164 0.0 49 169 0.0 54 184 0.0 80 280 0.0 107 368 0.0 63 2 7.1 50 176 2.7 49 174 0.0 54 180 0.0 80 280 0.0 107 378 0.0 63 2 7.2 49 176 0.0 54 172 0.0 80 280 0.0 107 378 0.0 63 2 7.3 49 176 0.0 49 174 0.0 54 192 0.0 80 284 0.0 107 384 0.0 63 2 7.3 <td>П</td> <td>7 5</td> <td>3 17</td> <td>6 2.6</td> <td>3 45</td> <td>Н</td> <td>+</td> <td>64</td> <td>164</td> <td>0.0</td> <td>54</td> <td>179</td> <td>0.0</td> <td>08</td> <td>268</td> <td>0.0</td> <td>107</td> <td>358</td> <td>0.0</td> <td>63 2</td> <td>1 2</td> <td>7 22</td> <td>7 4</td>	П	7 5	3 17	6 2.6	3 45	Н	+	64	164	0.0	54	179	0.0	08	268	0.0	107	358	0.0	63 2	1 2	7 22	7 4
7.0 51 176 2.7 45 156 0.0 49 175 0.0 54 187 0.0 80 284 0.0 107 379 0.0 63 2 7.1 50 176 2.8 45 156 0.0 54 197 0.0 80 284 0.0 107 379 0.0 63 2 7.2 49 176 0.0 54 192 0.0 80 288 0.0 107 379 0.0 63 2 7.3 49 176 2.8 45 163 0.0 49 179 0.0 80 286 0.0 107 384 0.0 63 2 7.4 48 176 2.8 45 165 0.0 49 18 0.0 80 286 0.0 107 349 7.5 47 176 2.8 45 165 0.0	7.0 5.7 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 <td></td> <td>8 0</td> <td>2 17</td> <td>6 2.7</td> <td>7 45</td> <td>· `</td> <td>_</td> <td>64</td> <td>167</td> <td>0.0</td> <td>54</td> <td>182</td> <td>0.0</td> <td>08 8</td> <td>272</td> <td>0.0</td> <td>107</td> <td>363</td> <td>0.0</td> <td>63 2</td> <td>14 6</td> <td>7 22</td> <td>77</td>		8 0	2 17	6 2.7	7 45	· `	_	64	167	0.0	54	182	0.0	08 8	272	0.0	107	363	0.0	63 2	14 6	7 22	77
7.1 50 176 2.7 4.5 158 0.0 4.9 174 0.0 54 190 0.0 80 284 0.0 107 339 0.0 63 2 7.2 4.9 176 2.8 1.0 0.0 49 176 0.0 54 192 0.0 80 288 0.0 107 384 0.0 63 2 7.3 4.9 176 2.8 4.5 163 0.0 4.9 181 0.0 54 198 0.0 80 296 0.0 107 395 0.0 63 2 7.4 4.8 176 2.8 4.5 165 0.0 4.9 181 0.0 54 108 0.0 80 296 0.0 107 400 0.0 63 2 108 0.0 63 2 80 0.0 63 2 80 0.0 63 2 80 </td <td>7.1 50 176 2.8 45 158 0.0 49 174 0.0 54 190 0.0 80 284 0.0 107 379 0.0 63 2 7.2 49 176 2.8 45 162 0.0 49 176 0.0 54 192 0.0 80 288 0.0 107 384 0.0 63 2 7.4 48 176 2.8 45 162 0.0 54 189 0.0 80 296 0.0 107 390 0.0 63 2 7.4 48 176 2.8 45 167 0.0 49 184 0.0 54 180 0.0 80 300 0.0 107 40 170 0.0 40 108 0.0 80 300 0.0 107 40 10 0.0 80 300 0.0 107 40 10<td></td><td></td><td></td><td>6 2.7</td><td>7 45</td><td>+</td><td>+</td><td>49</td><td>172</td><td>0.0</td><td>54</td><td>_</td><td>0.0</td><td>80</td><td>280</td><td>0.0</td><td>107</td><td>374</td><td>0.0</td><td>2 10</td><td>20 6</td><td>7 23</td><td>34</td></td>	7.1 50 176 2.8 45 158 0.0 49 174 0.0 54 190 0.0 80 284 0.0 107 379 0.0 63 2 7.2 49 176 2.8 45 162 0.0 49 176 0.0 54 192 0.0 80 288 0.0 107 384 0.0 63 2 7.4 48 176 2.8 45 162 0.0 54 189 0.0 80 296 0.0 107 390 0.0 63 2 7.4 48 176 2.8 45 167 0.0 49 184 0.0 54 180 0.0 80 300 0.0 107 40 170 0.0 40 108 0.0 80 300 0.0 107 40 10 0.0 80 300 0.0 107 40 10 <td></td> <td></td> <td></td> <td>6 2.7</td> <td>7 45</td> <td>+</td> <td>+</td> <td>49</td> <td>172</td> <td>0.0</td> <td>54</td> <td>_</td> <td>0.0</td> <td>80</td> <td>280</td> <td>0.0</td> <td>107</td> <td>374</td> <td>0.0</td> <td>2 10</td> <td>20 6</td> <td>7 23</td> <td>34</td>				6 2.7	7 45	+	+	49	172	0.0	54	_	0.0	80	280	0.0	107	374	0.0	2 10	20 6	7 23	34
7.2 4.9 1/6 2.8 4.5 1.6 0.0 4.9 1/6 2.8 4.5 1.6 0.0 4.9 1/6 2.8 4.5 1.5 0.0 4.9 1/6 2.8 4.5 1.5 0.0 4.9 1/6 0.0 24 1.9 0.0 80 2.96 0.0 107 384 0.0 6.3 2 7.4 4.8 1.76 2.8 4.5 1.67 0.0 4.9 181 0.0 54 198 0.0 80 2.96 0.0 107 4.90 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.0 63 2.8 0.	7.2 49 176 2.8 45 180 0.0 49 176 0.0 54 192 0.0 80 288 0.0 107 384 0.0 65 2 7.4 48 176 2.8 45 163 0.0 64 181 0.0 54 186 0.0 80 296 0.0 107 395 0.0 63 2 7.5 47 176 2.9 45 167 0.0 54 186 0.0 80 304 0.0 107 496 0.0 63 2 0.0 107 496 0.0 63 2 0.0 107 496 0.0 63 2 0 0 63 2 0 0 63 2 0 0 63 2 0 0 63 2 0 0 0 0 0 0 0 0 0 0 0 <td>1782 7</td> <td>1.</td> <td>H</td> <td>\vdash</td> <td>7 45</td> <td>\perp</td> <td>0 0</td> <td>49</td> <td>174</td> <td>0.0</td> <td>54</td> <td>\vdash</td> <td>0.0</td> <td>80</td> <td>284</td> <td>0.0</td> <td>107</td> <td>379</td> <td>\vdash</td> <td>3</td> <td>23 6</td> <td>7 23</td> <td>22</td>	1782 7	1.	H	\vdash	7 45	\perp	0 0	49	174	0.0	54	\vdash	0.0	80	284	0.0	107	379	\vdash	3	23 6	7 23	22
7.4 4.8 176 2.8 4.5 165 0.0 4.9 181 0.0 54 198 0.0 80 296 0.0 107 395 0.0 63 2 7.5 4.7 176 2.9 4.5 167 0.0 4.9 184 0.0 54 200 0.0 80 300 0.0 107 400 0.0 63 2 7.7 4.7 177 2.9 4.5 172 0.0 54 186 0.0 54 206 0.0 80 308 0.0 107 406 0.0 63 2 7.7 4.7 179 2.9 4.5 172 0.0 49 189 0.0 54 208 0.0 80 312 0.0 107 416 0.0 63 2 7.8 4.7 182 3.0 49 194 0.0 54 211 0.0 <	7.4 48 176 2.8 45 165 0.0 49 181 0.0 54 198 0.0 80 296 0.0 107 395 0.0 63 2 7.5 47 176 2.9 45 167 0.0 49 184 0.0 54 200 0.0 80 300 0.0 107 400 0.0 63 2 7.6 47 177 2.9 45 169 0.0 49 186 0.0 54 208 0.0 80 304 0.0 107 406 0.0 63 2 7.7 47 179 2.9 45 194 10.0 54 208 0.0 80 310 0.0 107 41 0.0 63 2 7.8 47 185 3.0 49 194 0.0 54 214 0.0 80 316 0.0 107	7 7891	7 K	9 6	2.2.9	2 & 2 4 1 0 0	+	0.0	2 4 0 4	179	0.0	54	261	0.0	200	292	0.0	107	390		2 6	30 6	7 24	5 4
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TRANSITION CURVES - RURAL 60 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03

802.42

SPECIFICATION REFERENCE

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42 114 0.0 47 126 0.0 52 139 0.0 56 180 0.0 112 302 0.0 66 180 42 116 0.0 47 128 0.0 52 141 0.0 56 154 0.0 84 231 0.0 112 307 0.0 66 180 42 118 0.0 47 135 0.0 52 146 0.0 56 160 0.0 112 319 0.0 66 180 42 118 0.0 52 146 0.0 56 160 0.0 112 319 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 180 0.0 <th< td=""><td>5.4 4.2 114 0.0 4.7 126 0.0 5.4 4.2 114 0.0 4.7 12.6 1.0 4.7 1.2 0.0 5.2 4.2 1.0 5.6 4.2 1.0 1.0 5.0 4.2 1.0 1.0 5.0 4.2 1.0 1.0 5.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0</td><td></td><td>5.2</td><td>42</td><td>109</td><td>0.0</td><td>47</td><td>121</td><td>0.0</td><td>52 1</td><td>134 (</td><td>0.0</td><td>56</td><td>146</td><td>0.0</td><td>84</td><td>218</td><td>0.0</td><td>112</td><td>291 0</td><td>0 0</td><td>1 1</td><td>70 7</td><td></td></th<>	5.4 4.2 114 0.0 4.7 126 0.0 5.4 4.2 114 0.0 4.7 12.6 1.0 4.7 1.2 0.0 5.2 4.2 1.0 5.6 4.2 1.0 1.0 5.0 4.2 1.0 1.0 5.0 4.2 1.0 1.0 5.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		5.2	42	109	0.0	47	121	0.0	52 1	134 (0.0	56	146	0.0	84	218	0.0	112	291 0	0 0	1 1	70 7	
42 116 0.0 47 128 0.0 52 141 0.0 56 154 0.0 84 231 0.0 112 30 0.0 66 183 42 120 0.0 47 133 0.0 52 144 0.0 56 162 0.0 84 235 0.0 112 339 0.0 16 183 0.0 66 183 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 66 180 0.0 84 243 0.0 112 334 0.0 66 180 0.0 86 180 <t< td=""><td>5.5 4.2 118 0.0 4.7 118 0.0 4.7 118 0.0 4.7 119 0.0 52 141 0.0 56 154 0.0 84 236 0.0 112 313 0.0 66 183 70 18 5.7 4.2 120 0.0 4.7 133 0.0 52 146 0.0 56 162 0.0 84 2.35 0.0 112 334 0.0 66 180 70 20 52 149 0.0 56 162 0.0 84 2.43 0.0 112 32.4 0.0 66 180 0.0 84 2.83 0.0 112 3.4 0.0 66 180 0.0 84 2.83 0.0 180 0.0 56 162 0.0 84 2.83 0.0 112 334 0.0 66 180 0.0 112 334 0.0 112<</td><td></td><td>5.4</td><td>42</td><td>114</td><td>0.0</td><td>47</td><td>126</td><td>0.0</td><td>52 1</td><td>39 (</td><td>0.0</td><td>26</td><td>151</td><td>0.0</td><td>84</td><td>227</td><td>0.0</td><td>112</td><td>302</td><td>0.</td><td>36</td><td>77 7</td><td></td></t<>	5.5 4.2 118 0.0 4.7 118 0.0 4.7 118 0.0 4.7 119 0.0 52 141 0.0 56 154 0.0 84 236 0.0 112 313 0.0 66 183 70 18 5.7 4.2 120 0.0 4.7 133 0.0 52 146 0.0 56 162 0.0 84 2.35 0.0 112 334 0.0 66 180 70 20 52 149 0.0 56 162 0.0 84 2.43 0.0 112 32.4 0.0 66 180 0.0 84 2.83 0.0 112 3.4 0.0 66 180 0.0 84 2.83 0.0 180 0.0 56 162 0.0 84 2.83 0.0 112 334 0.0 66 180 0.0 112 334 0.0 112<		5.4	42	114	0.0	47	126	0.0	52 1	39 (0.0	26	151	0.0	84	227	0.0	112	302	0.	36	77 7	
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42 122 0.0 47 135 0.0 52 149 0.0 56 162 0.0 84 243 0.0 112 324 0.0 66 190 7 66 191 2.4 47 135 0.0 52 149 0.0 56 162 0.0 84 243 0.0 112 324 0.0 66 190 7 65 191 2.5 47 135 0.0 52 161 0.0 84 243 0.0 112 324 0.0 66 190 7 64 191 2.5 47 140 0.0 56 162 0.0 84 243 0.0 112 334 0.0 66 190 0.0 66 190 0.0 66 190 0.0 66 190 0.0 66 190 0.0 66 190 0.0 66 190 0.0 </td <td>5.8 4.2 1.22 0.0 4.7 1.35 0.0 5.2 14.9 0.0 56 16.2 0.0 84 24.3 0.0 112 32.4 0.0 66 190 7.0 18 5.8 66 191 2.4 47 135 0.0 52 149 0.0 56 162 0.0 84 24.3 0.0 112 32.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 190 66 190 7.0 18 0.0 52 154 0.0 56 16.0 84 25.2 0.0 112 35.4 0.0 66 190 7.0 10 20 66 10 84 24.7 0.0 112 <th< td=""><td></td><td>5.7</td><td>42</td><td>120</td><td>0.0</td><td>4 4</td><td>133</td><td>0.0</td><td>52</td><td>44</td><td>0.0</td><td>26</td><td>) 091</td><td>0.0</td><td>4 8</td><td>539</td><td>0.0</td><td>112</td><td>219</td><td>5 0</td><td>0 90</td><td>37 /</td><td></td></th<></td>	5.8 4.2 1.22 0.0 4.7 1.35 0.0 5.2 14.9 0.0 56 16.2 0.0 84 24.3 0.0 112 32.4 0.0 66 190 7.0 18 5.8 66 191 2.4 47 135 0.0 52 149 0.0 56 162 0.0 84 24.3 0.0 112 32.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 12 52.4 0.0 66 190 7.0 190 66 190 7.0 18 0.0 52 154 0.0 56 16.0 84 25.2 0.0 112 35.4 0.0 66 190 7.0 10 20 66 10 84 24.7 0.0 112 <th< td=""><td></td><td>5.7</td><td>42</td><td>120</td><td>0.0</td><td>4 4</td><td>133</td><td>0.0</td><td>52</td><td>44</td><td>0.0</td><td>26</td><td>) 091</td><td>0.0</td><td>4 8</td><td>539</td><td>0.0</td><td>112</td><td>219</td><td>5 0</td><td>0 90</td><td>37 /</td><td></td></th<>		5.7	42	120	0.0	4 4	133	0.0	52	44	0.0	26) 091	0.0	4 8	539	0.0	112	219	5 0	0 90	37 /	
66 191 2.4 47 135 0.0 52 149 0.0 56 162 0.0 84 243 0.0 112 324 0.0 66 190 7 66 191 2.4 47 135 0.0 52 149 0.0 56 162 0.0 84 243 0.0 112 324 0.0 66 190 7 64 191 2.5 47 140 0.0 52 154 0.0 56 162 0.0 112 335 0.0 66 190 7 62 191 2.5 47 140 0.0 56 174 0.0 84 256 0.0 112 341 0.0 66 100 66 200 66 200 66 200 66 200 66 200 66 200 66 200 66 200 66 200 66	5.8 66 191 2.4 47 135 0.0 52 149 0.0 56 162 0.0 84 24.3 0.0 112 324 0.0 66 199 70 22 5.9 66 191 2.4 4.7 136 0.0 52 149 0.0 56 162 0.0 84 24.7 0.0 112 334 0.0 66 190 70 2 6.0 6.0 64 191 2.5 47 140 0.0 56 174 0.0 84 267 0.0 112 354 0.0 66 190 70 2 6.0 6.1 191 2.5 47 149 0.0 56 174 0.0 84 266 0.0 112 354 0.0 66 190 70 2 6.0 46 191 0.0 56 174 0.0 84 </td <td></td> <td>5.8</td> <td>42</td> <td>122</td> <td>0.0</td> <td>47</td> <td>135</td> <td>0.0</td> <td>52 1</td> <td>\vdash</td> <td>0.0</td> <td>56</td> <td>162 (</td> <td>0.0</td> <td>84</td> <td>243</td> <td>0.0</td> <td>112</td> <td>24 C</td> <td>0.</td> <td>36 15</td> <td>30 7</td> <td>.,</td>		5.8	42	122	0.0	47	135	0.0	52 1	\vdash	0.0	56	162 (0.0	84	243	0.0	112	24 C	0.	36 15	30 7	.,
66 191 2.4 4 / 135 0.0 52 162 0.0 56 162 0.0 84 243 0.0 112 334 0.0 66 190 7 64 191 2.5 47 136 0.0 56 168 0.0 84 250 0.0 112 335 0.0 66 190 7 62 191 2.5 47 140 0.0 52 154 0.0 66 100 112 347 0.0 66 200 195 7 61 191 2.5 47 142 0.0 56 174 0.0 84 250 0.0 112 347 0.0 66 203 62 191 2.5 47 142 0.0 56 182 0.0 84 256 0.0 112 347 0.0 66 203 60 193 0.0 66 20	5.8 66 191 2.4 47 185 0.0 52.8 66 191 2.4 47 185 0.0 52 182 0.0 84 24.5 0.0 112 53.4 0.0 66 193 7.0 12 6.0 6.4 191 2.5 47 140 0.0 52 154 0.0 56 174 0.0 84 256 0.0 112 343 0.0 66 193 7.0 26 6.1 6.2 191 2.5 47 142 0.0 52 162 0.0 84 256 0.0 112 343 0.0 66 174 0.0 84 256 0.0 112 359 0.0 66 179 0.0 84 256 0.0 112 340 0.0 66 174 0.0 84 256 0.0 112 33 0.0 66 179 0.0		8.6	99	191	2.4	47	135	0.0	52 1	+	0.0	26	162	0.0	48	243	0.0	211	24 0	0.0	90	06	.,
6.3 6.4 7.1 7.2 7.1 7.2 7.1 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 8.2 7.2 7.2 7.2 7.2 8.2 7.2 7.2 7.2 7.2 7.2 7.2 8.2 7.2 7.2 7.2 7.2 7.2 <td>6.0 6.1 191 2.5 4.7 140 0.0 52 151 0.0 56 180 25.0 0.0 11 250 0.0 10 12 25.0 0.0 12 25.0 0.0 12 25.0 0.0 12 34.1 0.0 66 100 0.0 10 12 34.1 0.0 66 100 0.0 10 10 34.1 0.0 66 10 0.0 10 10 34.1 0.0 66 10 0.0 10 10 34.1 0.0 66 10 0.0 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 <</td> <td></td> <td>ο u</td> <td>96</td> <td>5 5</td> <td>4.7</td> <td>14/</td> <td>2 2 2 2 2 2 2 2 2 2</td> <td>0 0</td> <td>22 2</td> <td>+</td> <td>0 0</td> <td>20 %</td> <td>765</td> <td></td> <td>400</td> <td>545</td> <td>0 0</td> <td>7 2 2</td> <td>470</td> <td>5 0</td> <td>Q 9</td> <td>7 2</td> <td>) (</td>	6.0 6.1 191 2.5 4.7 140 0.0 52 151 0.0 56 180 25.0 0.0 11 250 0.0 10 12 25.0 0.0 12 25.0 0.0 12 25.0 0.0 12 34.1 0.0 66 100 0.0 10 12 34.1 0.0 66 100 0.0 10 10 34.1 0.0 66 10 0.0 10 10 34.1 0.0 66 10 0.0 10 10 34.1 0.0 66 10 0.0 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 <		ο u	96	5 5	4.7	14/	2 2 2 2 2 2 2 2 2 2	0 0	22 2	+	0 0	20 %	765		400	545	0 0	7 2 2	470	5 0	Q 9	7 2) (
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6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2 174 0.0 64 260 0.0 112 347 0.0 66 208 0.0 6.2 6.2 174 0.0 56 176 0.0 112 354 0.0 66 208 7 6.2 6.0 176 0.0 84 268 0.0 112 352 0.0 66 208 7 6.0 84 268 0.0 112 352 0.0 66 208 7 6 20 20 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 136 0.0 66 <	6.2 6.2 6.2 6.4 145 0.0 52 159 0.0 56 174 0.0 84 260 0.0 112 347 0.0 66 203 70 2 6.3 61.3 61.3 61.3 61.4 60.0 56 176 0.0 84 266 0.0 112 352 0.0 66 203 70 2 6.5 59 191 2.5 47 149 0.0 52 164 0.0 56 182 0.0 84 268 0.0 112 358 0.0 66 213 70 2 6.6 58 191 2.6 47 16 0.0 52 172 0.0 56 182 0.0 84 289 0.0 112 389 0.0 66 213 0.0 52 174 0.0 56 182 0.0 84 289 0.0 <t< td=""><td></td><td>6.1</td><td>63</td><td>191</td><td>2.5</td><td>47</td><td>7</td><td>0.0</td><td>52 1.</td><td>H</td><td>0.0</td><td>56</td><td>171</td><td>0.0</td><td>84</td><td>556</td><td>0.0</td><td>112</td><td>341 C</td><td>0.0</td><td>36 2</td><td>00 7</td><td></td></t<>		6.1	63	191	2.5	47	7	0.0	52 1.	H	0.0	56	171	0.0	84	556	0.0	112	341 C	0.0	36 2	00 7	
6.5 61 191 2.5 47 147 0.0 52 162 0.0 56 176 0.0 84 264 0.0 112 358 0.0 66 209 7 6.5 59 191 2.6 47 152 0.0 52 167 0.0 56 182 0.0 84 273 0.0 112 358 0.0 66 213 7 6.6 58 191 2.6 47 154 0.0 52 162 0.0 56 182 0.0 112 353 0.0 66 213 7 6.6 58 191 2.6 47 156 0.0 52 182 0.0 84 273 0.0 112 374 0.0 66 220 6.8 57 191 2.6 10 56 180 0.0 84 289 0.0 112 389 0.0 </td <td>6.5 61 191 2.5 47 149 0.0 52 169 0.0 84 264 0.0 176 0.0 84 264 0.0 176 0.0 84 264 0.0 186 179 0.0 66 204 0.0 56 189 0.0 84 273 0.0 112 558 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0</td> <td></td> <td>6.2</td> <td>62</td> <td>191</td> <td>2.5</td> <td>47</td> <td>+</td> <td>0.0</td> <td>52 1.</td> <td>+</td> <td>0.0</td> <td>26</td> <td>_</td> <td>0.0</td> <td>84</td> <td>09</td> <td>0.0</td> <td>112</td> <td>247</td> <td>_</td> <td>36</td> <td>03</td> <td>.,</td>	6.5 61 191 2.5 47 149 0.0 52 169 0.0 84 264 0.0 176 0.0 84 264 0.0 176 0.0 84 264 0.0 186 179 0.0 66 204 0.0 56 189 0.0 84 273 0.0 112 558 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0 66 213 0.0		6.2	62	191	2.5	47	+	0.0	52 1.	+	0.0	26	_	0.0	84	09	0.0	112	247	_	36	03	.,
6.5 59 191 2.6 47 150 2.0 50 182 0.0 84 273 0.0 112 353 0.0 66 213 0.0 66 213 0.0 66 218 0.0 66 218 0.0 66 218 0.0 66 218 0.0 66 218 0.0 66 218 0.0 112 354 0.0 66 218 0.0 66 218 0.0 112 354 0.0 66 218 0.0 66 218 0.0 112 354 0.0 66 218 0.0 66 218 0.0 66 226 174 0.0 56 180 0.0 84 284 0.0 112 374 0.0 66 226 178 0.0 84 284 0.0 112 380 0.0 66 223 0.0 112 384 0.0 112 380	6.5 58 191 2.6 47 152 0.0 52 169 0.0 56 185 0.0 84 273 0.0 112 563 0.0 66 213 70 22 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		6.3	61	191	2.5	47	_	0 0	52 1	+	+	56	_	0.0	48 8	407	0.0	112	+	+	2 2	90	0 0
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7.2 54 191 2.7 47 168 0.0 52 185 0.0 56 201 0.0 84 302 0.0 112 402 0.0 66 236 7 7.3 53 191 2.7 47 170 0.0 52 187 0.0 56 204 0.0 84 310 0.0 112 418 0.0 66 242 7 7.5 51 191 2.8 47 175 0.0 52 192 0.0 56 210 0.0 84 310 0.0 112 414 0.0 66 245 7 7.6 51 191 2.8 47 175 0.0 52 192 0.0 56 213 0.0 84 319 0.0 112 430 0.0 66 245 7 7.5 491 2.9 10.0 56 219 0.0 </td <td>7.2 54 191 2.7 47 168 0.0 52 185 0.0 56 201 0.0 84 302 0.0 112 402 0.0 66 236 70 22 7.3 5.3 191 2.7 47 170 0.0 52 187 0.0 56 204 0.0 84 306 0.0 112 408 0.0 66 245 70 22 7.5 51 191 2.8 47 175 0.0 52 192 0.0 56 20 0.0 84 314 0.0 112 419 0.0 66 245 70 22 7.5 50 191 2.8 47 175 0.0 52 192 0.0 66 213 0.0 84 319 0.0 112 425 0.0 66 245 70 28 7.7 50 192<td>П</td><td>7.1</td><td>54</td><td>191</td><td>2.7</td><td>47</td><td>Н</td><td>0.0</td><td>52 1</td><td>Н</td><td>0.0</td><td>26</td><td>ш</td><td>Н</td><td>84</td><td>867</td><td>0.0</td><td>112</td><td></td><td>-</td><td>36</td><td>32 7</td><td>2</td></td>	7.2 54 191 2.7 47 168 0.0 52 185 0.0 56 201 0.0 84 302 0.0 112 402 0.0 66 236 70 22 7.3 5.3 191 2.7 47 170 0.0 52 187 0.0 56 204 0.0 84 306 0.0 112 408 0.0 66 245 70 22 7.5 51 191 2.8 47 175 0.0 52 192 0.0 56 20 0.0 84 314 0.0 112 419 0.0 66 245 70 22 7.5 50 191 2.8 47 175 0.0 52 192 0.0 66 213 0.0 84 319 0.0 112 425 0.0 66 245 70 28 7.7 50 192 <td>П</td> <td>7.1</td> <td>54</td> <td>191</td> <td>2.7</td> <td>47</td> <td>Н</td> <td>0.0</td> <td>52 1</td> <td>Н</td> <td>0.0</td> <td>26</td> <td>ш</td> <td>Н</td> <td>84</td> <td>867</td> <td>0.0</td> <td>112</td> <td></td> <td>-</td> <td>36</td> <td>32 7</td> <td>2</td>	П	7.1	54	191	2.7	47	Н	0.0	52 1	Н	0.0	26	ш	Н	84	867	0.0	112		-	36	32 7	2
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SPECIFICATION REFERENCE

TRANSITION CURVES - RURAL 65 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03 802.43

TC-5.01		RAMPS	FT	LS	75	79	87	06	98	102	105	113	117	124	128	135	139	143	150	154	162	165	169	177	180	188	192	199	203	210	214	278	225	229	237	240	244	244	252	255	263	267	274	278	282	289	293	300	
			ω	د د	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	Ú L
	MAX.	CHANGE	FT	S	72	75	82	98	89	96	100	107	11 5	138	121	128	132	136	143	146	15.3	157	160	168	171	178	182	185	192	796	203	207	214	217	224	228	232	232	239	242	249	253	256	264	267	274	278	285	14/
	×.	INTERCHANGE	I . [ج ا	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72/	72	72	72	72	72	72	72	72	72/	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	W VALIFS IN FEFT LISTED PADILIS IS THE MINIMIN ALLOWARIE PADILIS FOR THE CORRESPONDING F OF 15 AND W VALIFS
	00	FT		≥ 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	υ -
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		DESIGN VELOCITY	-70	RADIUS(FT)	10731	10194	9260	8851	8474	7805	7506	6967	6724	6281	6079	5708	5537	5376	5076	4937	4679	4558	4443	4226	4125	3933	3843	3673	3592	3439	3366	3296	3163	3099	2977	2919	2865	2862	2753	2699	2590	2535	2480	2365	2305	2175	2100	1821	NOTE:
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70 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 3/03

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