

### **DEPARTMENT OF TRANSPORTATION**

1401 EAST BROAD STREET RICHMOND, VIRGINIA 23219-2000

David S. Ekern, P.E.

January 30, 2007

### **MEMORANDUM**

To: All Holders of the Virginia Department of Transportation's 2001 Road and Bridge Standards

The current design standards for Transition Curves (TC-5.01 and TC-5.04) have been revised and the attached revision documents are to be added to your copy of the VDOT <u>2001 Road and Bridge Standards</u>. The revision updates specific terminology in the TC-5.01 Standards to conform to the terminology used in the AASHTO 2004 <u>A Policy on Geometric Design of Highways and Streets</u> ("Green Book"). These changes include:

- The "Crown Runoff" (CR) has been changed to "Tangent Run out" (Lt). This term denotes the transition distance from normal crown to the 0% grade on the high side of the superelevation.
- The "Length of Spiral" (LS) has been changed to "Super Runoff" (Lr). This term denotes the transition distance from 0% grade on the high side of the superelevation to full superelevation.

In addition to these changes, all references to Appendix A of the VDOT <u>Road Design Manual</u> have been revised to reference Chapter 3 of the AASHTO Green Book. An insertable sheet will not be required in plan assemblies for this revision. To avoid confusion, the old TC-5 Standard has also been revised to reflect the AASHTO Green Book terminology.

If you have any questions or comments regarding the listed revisions to this publication, please contact Steve Van Cleef of the Standards and Special Design Section at (804) 786-2532.

Sincerely,

Mohammad Mirshahi, P.E. State Location and Design Engineer

### STANDARD SYMBOLS

LOCATION BALIGNMENT ON WHICH THE PROPOSED RIGHT-OF-WAY AND CONSTRUCTION IS BASED.
STANDARD PAVEMENTTHE TYPICAL PAVEMENT SECTION TO BE SHOWN ON THE ROAD PLANS.
P.CPOINT OF BEGINNING OF BASELINE CIRCULAR CURVE.
P.TPOINT OF ENDING OF BASELINE CIRCULAR CURVE.
P.C.CPOINT OF BASELINE COMPOUND CURVATURE.
P.R.CPOINT OF BASELINE REVERSE CURVE.
T.SPOINT OF CHANGE FROM TANGENT TO TRANSITION CURVE.(TANGENT TO SPIRAL)
S.CPOINT OF CHANGE FROM TRANSITION CURVE TO CIRCULAR CURVE. (SPIRAL TO CIRCULAR)
C.SPOINT OF CHANGE FROM CIRCULAR CURVE TO TRANSITION CURVE. (CIRCULAR TO SPIRAL)
S.TPOINT OF CHANGE FROM TRANSITION CURVE TO TANGENT. (SPIRAL TO TANGENT)
RADIUSRADIUS OF BASELINE CIRCULAR CURVE.
DVAPPROXIMATE MAXIMUM SAFE SPEED IN MILES PER HOUR USING STANDARD RATE OF SUPER
ELEVATION.
NCAPPROXIMATE MAXIMUM SAFE SPEED IN MILES PER HOUR WITH NO SUPERELEVATION.
FACTORS APPLY ONLY TO URBAN LOW SPEED CONDITIONS.
LrLENGTH OF TRANSITION CURVE MEASURED ALONG BASELINE. WHERE NO TRANSITION CURVE
IS APPLIED Lr IS LENGTH OF SUPERELEVATION RUNOFF SECTION.
W OR PWWIDTH OF STANDARD PAVEMENT.
ZTDISTANCE FROM TRANSITIONED BASELINE TO EDGES OF TRANSITIONED PAVEMENT $(rac{W}{2} + rac{W}{2})$
wMAXIMUM TOTAL PAVEMENT WIDENING.
ERATE OF SUPERELEVATION.
FSAFE SIDE FRICTION FACTOR.
SAMOUNT OF SUPERELEVATION TO BE APPLIED TO THE BASELINE GRADE TO OBTAIN THE
ELEVATIONS OF THE EDGES OF TRANSITIONED PAVEMENT.
CDIFFERENCE IN ELEVATION BETWEEN BASELINE (CENTER) AND EDGE OF PAVEMENT FOR
STANDARD PAVEMENT CROWN.
LtSTANDARD PAVEMENT CROWN TRANSITION OR TANGENT RUNOUT SECTION.
CPCHORD POINT (1/10 INCREMENTS OF TRANSITION CURVE).
NPCNORMAL PAVEMENT CROWN.

ALL DISTANCES (HORIZONTAL AND VERTICAL) ARE MEASURED IN FEET.

SPECIFICATION REFERENCE TRANSITION CURVES FOR RURAL AND URBAN HIGHWAYS AND STREET CONDITIONS

REV. 1/07

## URBAN CONDITION

URBAN CONDITIONS APPLY TO URBAN <u>STREET</u> SYSTEMS AND ANY OTHER ROAD WITH PRESENT OR FUTURE URBAN STREET OPERATING CONDITIONS.

THESE TABLES CONTAIN SUPERELEVATION RATES AND TRANSITION LENGTHS FOR STANDARD URBAN PAVEMENT WIDTHS THOUGH A RANGE OF CURVES AND DESIGN VELOCITIES CONSIDERED MOST LIKELY TO BE USED IN URBAN ROAD DESIGN.

DEFINITIONS FOR THE STANDARD SYMBOLS USED THROUGHOUT THESE TABLES ARE FOUND ON SHEET 801.01.

A TABLE FOR "LOW SPEED URBAN" DESIGNS IS ON SHEET 801.20 WITH A RANGE OF STANDARD PAVEMENT WIDTHS (W), TRANSITION LENGTHS (Lr), AND RADII OF CURVE WHEN SUPERELEVATED BY AN AMOUNT EQUAL TO THE NORMAL CROWN AND THE APPROXIMATE MAXIMUM SAFE SPEEDS (DV) AFFORDED THEREBY. VALUES IN THIS TABLE CAN BE USED ON STREETS WITH OPERATING SPEEDS LESS THAN OR EQUAL TO 45 MPH. ALSO SHOWN ARE THE APPROXIMATE MAXIMUM SAFE SPEEDS (NC) WITH NO SUPERELEVATION. VALUES FOR (NC) CAN BE USED ON URBAN ARTERIAL, COLLECTOR, AND LOCAL STREETS.

FOR MINIMUM DESIGN FACTORS FOR VARIOUS DESIGN SPEEDS FOR URBAN CONDITIONS SEE SHEETS 801.21 THRU 801.29

WHEN URBAN CONDITIONS APPLY THERE <u>WILL</u> BE NO BASELINE TRANSITION OR PAVEMENT WIDENING. THE LENGTH OF SUPERELEVATION RUNOFF (Lr) DETERMINES THE LENGTH OF SUPERELEVATION TRANSITION THROUGH WHICH THE OUTER EDGE OF PAVEMENT IS RAISED ABOVE THE BASELINE GRADE TO A MAXIMUM OF E  $(\frac{W}{2})$ . SEE SHEET 801.06 FOR A GRAPHICAL ILLUSTRATION OF THE APPLICATION OF THIS CORRECTION.

FOR CURVE RADII NOT LISTED IN TABLES REFER TO SHEET 801.18 TO CALCULATE TRANSITION LENGTHS (Lr).

Lr SHOULD BE SHOWN ON THE PLANS FOR ALL CURVES.

E SHOULD BE SHOWN ON THE PLANS FOR ALL CURVES WITH URBAN STREET CONDITIONS.

FOR GRAPHICAL ILLUSTRATION OF DESIGN SUPERELEVATION RATES FOR URBAN CONDITIONS SEE SHEET 801.15.

FOR ADDITIONAL GENERAL INSTRUCTIONS (BOTH URBAN AND RURAL) SEE SHEET 801.04.

EXPLANATION OF TABLES AND INSTRUCTIONS FOR USE URBAN CONDITION

## RURAL CONDITION

RURAL CONDITIONS APPLY TO INTERSTATE, ARTERIAL, PRIMARY AND SECONDARY SYSTEMS OR TO ANY OTHER ROAD WITH RURAL TYPE DESIGN AND OPERATING CONDITIONS.

THESE TABLES CONTAIN SUPERELEVATION AND WIDENING CORRECTIONS FOR STANDARD RURAL PAVEMENT WIDTHS THROUGH A RANGE OF RADII AND DESIGN VELOCITIES CONSIDERED MOST LIKELY TO BE USED IN RURAL HIGHWAY DESIGN.

DEFINITIONS FOR THE STANDARD SYMBOLS USED THROUGHOUT THESE TABLES ARE FOUND ON SHEET 801.01.

FOR MINIMUM DESIGN FACTORS FOR VARIOUS DESIGN SPEEDS FOR RURAL CONDITIONS SEE SHEETS 801.30 THRU 801.40.

ON CURVES WITH GREATER THAN 2865 FT RADIUS THERE WILL BE NO SPIRAL TRANSITION OR PAVEMENT WIDENING. PAVEMENT WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE RATE SHOWN IN THE TABLES. SEE SHEET 801.06 FOR A GRAPHICAL ILLUSTRATION OF THE APPLICATION OF THIS CORRECTION.

ON CURVES WITH PAVEMENT WIDTHS OF 24'OR WIDER AND A RADIUS OF 881 FT. OR GREATER, THERE WILL BE NO SPIRAL TRANSITION OR PAVEMENT WIDENING. PAVEMENT WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE RATE SHOWN IN THESE TABLES.

FOR CURVE RADII NOT LISTED IN TABLES REFER TO SHEET 801.18 TO CALCULATE SUPERELEVATION RUNOFF LENGTHS (Lr) AND PAVEMENT WIDENING (w).

Lr AND E SHOULD BE SHOWN ON THE PLANS FOR ALL CURVES ..

FOR GRAPHICAL ILLUSTRATION OF DESIGN SUPERELEVATION RATES FOR RURAL CONDITIONS SEE SHEET 801.16.

FOR ADDITIONAL GENERAL INSTRUCTIONS (BOTH URBAN AND RURAL) SEE SHEET 801.04.

EXPLANATION OF TABLES AND INSTRUCTIONS FOR USE RURAL CONDITION

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 1/07 801.03

## GENERAL CONDITION

ALL ORIGINAL CROSS SECTIONS SHALL BE TAKEN FROM THE BASELINE AT STATIONS, PLUS FIFTIES, AND UNUSUAL BREAKS IN THE GROUND AS ON TANGENT ALIGNMENT.

WHERE A PART OR ALL OF A SUPERELEVATION TRANSITION CURVE FALLS ON A VERTICAL CURVE, ELEVATIONS ON THE VERTICAL CURVE SHOULD BE COMPUTED FOR THE POSITIONS GIVEN ON SHEET 801.12 FOR CROWN TRANSITIONS, SHEET 801.13 FOR URBAN PROJECTS AND SHEET 801.14 FOR RURAL PROJECTS. THESE ELEVATIONS AND PLUSES SHOULD BE SHOWN ON THE PLANS FOR THE CONVENIENCE OF THE SURVEY PARTY IN STAKING OUT THE PROJECT. THROUGHOUT THESE SECTIONS OF THE GRADE, ELEVATIONS AT EVEN STATIONS AND PLUS FIFTIES SHOULD BE OMITTED.

SLOPE STAKES SHOULD BE SET AT THE POSITIONS ON THE TRANSITION GIVEN ON SHEETS 801.12, 801.13 AND 801.14 AND GROUND CROSS SECTIONS TAKEN AT THESE POSITIONS OMITTING THE STATIONS AND PLUS FIFTIES THROUGHOUT THE TRANSITION. IF UNUSUAL BREAKS IN THE GROUND OCCUR, ADDITIONAL SECTIONS SHOULD, OF COURSE, BE TAKEN. ADDITIONAL SECTIONS SHOULD ALSO BE TAKEN WHERE LOCATION IS THROUGH ROCK CUT IN ANTICIPATION OF UNUSUAL BREAKAGE WHICH MAY OCCUR DURING CONSTRUCTION.

AFTER ROUGH GRADING HAS BEEN DONE, FINE GRADING (BLUE TOP) AND FORM STAKES SHOULD BE SET AT THE POSITIONS GIVEN ON SHEET 801.12 FOR CROWN TRANSITIONS, SHEET 801.13 FOR URBAN PROJECTS OR AS GIVEN ON SHEET 801.14 FOR RURAL PROJECTS.

FINAL CROSS SECTIONS SHOULD, OF COURSE, BE TAKEN AT THOSE POSITIONS AT WHICH THE SLOPE STAKE SECTIONS WERE TAKEN. WHERE UNUSUAL BREAKAGE IN ROCK OCCURS AND THIS WAS NOT ANTICIPATED, ADDITIONAL FINAL SECTIONS SHOULD BE TAKEN AND ORIGINAL GROUND SECTIONS INTERPOLATED.

BASELINE STAKES SHOULD BE SET AT ALL P.C.'S, P.T.'S, T.S.'S, S.T.'S, S.C.'S, AND C.S.'S IN STAKING OUT ALIGNMENT, BUT SLOPE STAKES NEED NOT BE SET NOR CROSS SECTIONS TAKEN AT P.C.'S OR P.T.'S EXCEPT WHERE CALLED FOR IN THE ACCOMPANYING TABLES. THE TRANSITION WILL TAKE ITS FORM FROM THE POSITIONS GIVEN ON SHEETS 801.13 AND 801.14.

THE RIGHT OF WAY SHALL, IN ALL CASES, BE REFERENCED FROM THE BASELINE.

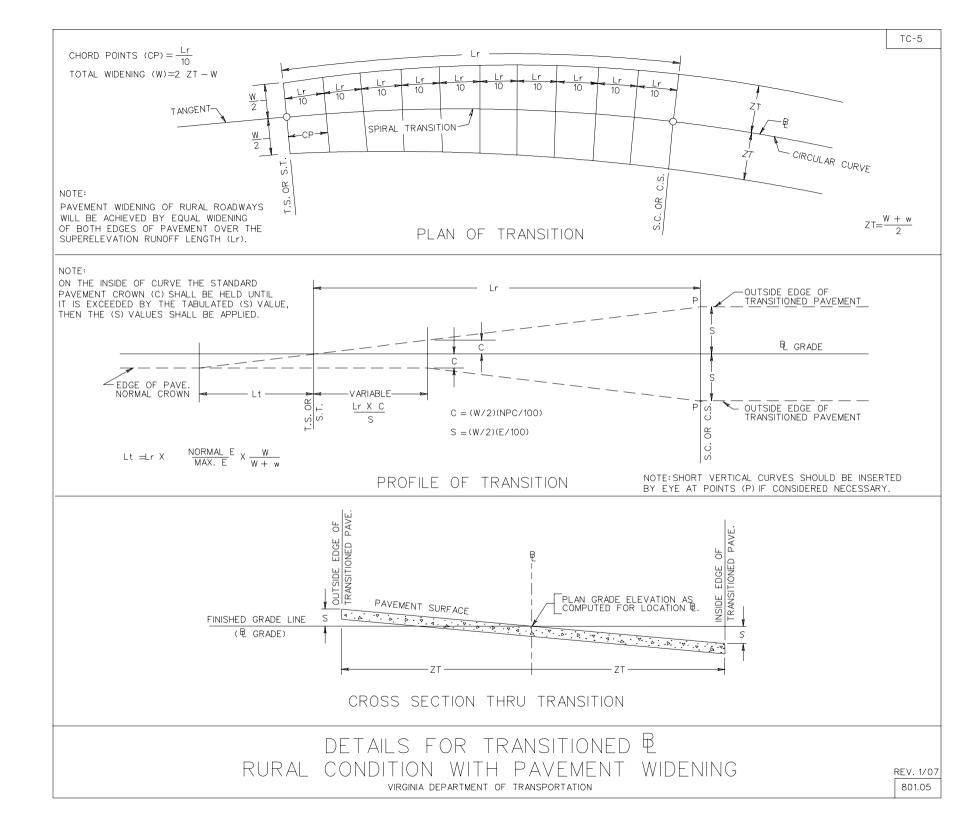
THE DESIGNER SHOULD AVOID SITUATIONS NECESSITATING REVERSE CURVES AND CURVES WITH OVERLAPPING TRANSITIONS WHERE POSSIBLE.

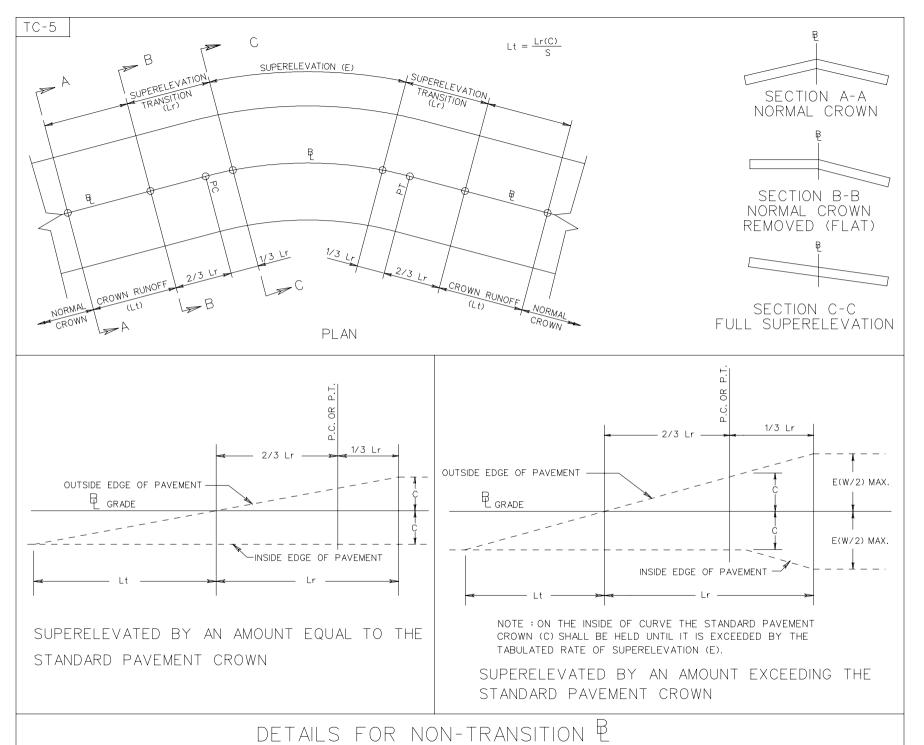
A DESIGN EXCEPTION IS NOT REQUIRED WHEN USING VALUES FROM SHEETS 801.21 THRU 801.40 SINCE THESE TABLES WERE DERIVED WITHIN AASHTO GUIDELINES.

ALL TANGENT RUNOUT SECTION VALUES LISTED IN THE TABLES HAVE BEEN ROUNDED UP TO THE NEAREST FOOT. ALL Lt VALUES ARE BASED ON A 2% CROWN.

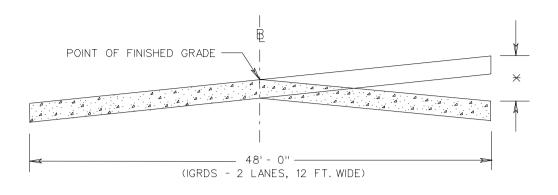
EXPLANATION OF TABLES AND INSTRUCTIONS FOR USE GENERAL CONDITION

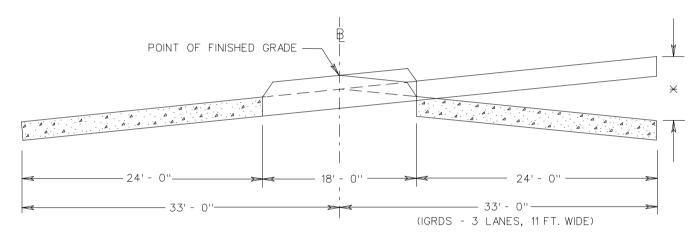
801.04 VIRGINIA DEPARTMENT OF TRANSPORTATION





REV. 1/07 URBAN CONDITIONS AND RURAL CONDITIONS WITHOUT PAVEMENT WIDENING 801.06

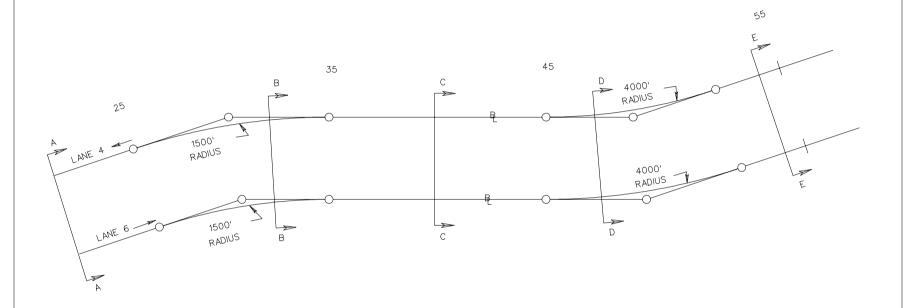




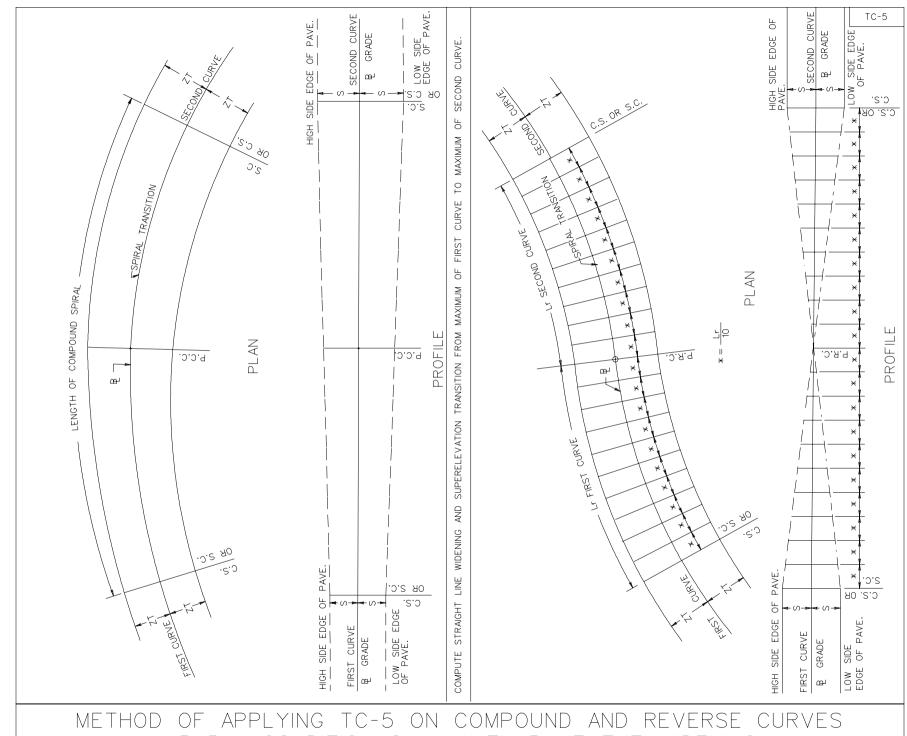
\* THE ELEVATION DIFFERENTIAL BETWEEN NORMAL CROWN AND MAXIMUM SUPERELEVATION, RELATIVE TO THE BASELINE PROFILE.

ADDITIONAL INFORMATION MAY BE OBTAINED FROM A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (AASHTO) BOOK, CHAPTER III - ELEMENTS OF DESIGN (SUPERELEVATION RUNOFF).

ON STANDARD TC-5ULS, TC-5U , AND TC-5R (WITHOUT PAVEMENT WIDENING) SUPERELEVATED CURVES, POSITION THE Lr TWO THIRDS (2/3) ON THE TANGENT AND ONE THIRD (1/3) INTO THE CURVE. STATIONS AND ELEVATIONS FOR THESE TRANSITIONS WILL NEED TO BE COMPUTED FOR ALL CHORD POINTS AND SHOWN ON THE PROFILES.



EXAMPLE FOR FOUR LANE ROADWAYS



RURAL CONDITION WIDENING

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 1/07 801.11

## TRANSITION TABLE

LENGTH OF TANGENT RUNOUT (Lt)	START/END OF SUPERELEVATION RUNOFF SECTION	START/END	NORMAL CROWN			
(20)	(Lr)	1	4			
220	0	44	88	132	176	220
200	0	40	80	120	140	200
180	0	36	72	108	144	180
160	0	32	64	96	128	160
140	0	28	56	84	112	140
120	0	24	48	72	96	120
100	0	20	40	60	80	100
90	0	18	36	54	72	90
80	0	16	32	48	64	80
60	0	15	30	45		60
40	0	20				40

#### NOTE:

TABLE LISTS POSTIONS ON TRANSITIONS AT WHICH SLOPE STAKES SHOULD BE SET, CONSTRUCTION AND FINAL CROSS-SECTIONS TAKEN, FINE GRADING STAKES (BLUE TOP) SET, AND FORM STAKES SET (CONCRETE PAVEMENT ONLY).

SUPERELEVATION RUNOFF (Lr) / TANGENT RUNOUT (Lt) TABLE

# URBAN CONDITIONS RURAL CONDITIONS WITHOUT PAVEMENT WIDENING

FOR USE WITH FLEXIBLE AND CONCRETE PAVEMENT (Lr POSITIONED 2/3 ±0N TANGENT, 1/3 ±0N CURVE)

LENGTH OF SUPERELEVATION RUNOFF SECTION RUNO				DISTANCE IN				P.C. OR P.T.	DIST P.C	FULL SUPER ELEVATION (E)		
(Lr)	(Lt)	1	2	3	4	5	6		7	8	9	
480	320	272	224	176	128	80	32	STAKE	16	64	112	160
460	307	261	215	169	123	77	31	STAKE	15	61	107	153
440	293	249	205	161	117	73	29	STAKE	15	59	103	147
420	280	238	196	154	112	70	28	STAKE	14	56	98	140
400	267	227	187	147	107	67	27	STAKE	13	53	93	133
380	253	215	177	139	101	63	25	STAKE	13	51	89	127
360	240	204	168	132	96	60	24	STAKE	12	48	84	120
340	227	193	159	125	91	57	23	STAKE	11	45	79	113
320	213	181	149	117	85	53	21	STAKE	11	43	75	107
300	200	170	140	110	80	50	20	STAKE	10	40	70	100
280	187	159	131	103	75	47	19	STAKE	9	37	65	93
260	173	147 ×	121	95 ×	69	43 ×	17	STAKE *	9	35 ×	61	87
240	160	136 ×	112	88 X	64	40 *	16	STAKE *	8	32 ×	56	80
220	147	125 <sup>Ж</sup>	103	81 ×	59	37 ×	15	STAKE *	7	29 X	51	73
200	133	113 ×	93	73 ×	53	33 ×	13	STAKE *	7	27 *	47	67
180	120	102 <sup>Ж</sup>	84	66 ×	48	30 ×	12	STAKE *	6	24 X	42	60
160	107	91 <sup>Ж</sup>	75	59 ×	43	27 ×	11	STAKE *	5	21 *	37	53

#### NOTE :

TABLE GIVING POSITIONS ON CURVES AT WHICH SLOPE STAKES SHOULD BE SET, CONSTRUCTION AND FINAL CROSS-SECTIONS TAKEN, FINE GRADING STAKES (BLUE TOP) SET, AND FORM STAKES SET (CONCRETE PAVEMENT ONLY).

\* DENOTES ADDITIONAL STAKING POSITIONS FOR USE WITH CONCRETE PAVEMENT ONLY.

TABLE I

## RURAL CONDITIONS WITH PAVEMENT WIDENING

FOR USE WITH FLEXIBLE AND CONCRETE PAVEMENT

SUPERELEVATION RUNOFF SECTION	T.S. OR S.T.	DISTANCE IN FEET FROM T.S. OR S.T.  ALONG SPIRAL TRANSITION											
(Lr)		1	2	3	4	5	6	7	8	9			
480	0	48	96	144	192	240	288	336	384	432	480		
460	0	46	92	138	184	230	276	322	368	414	460		
440	0	44	88	132	176	220	264	308	352	396	440		
420	0	42	84	126	168	210	252	294	336	378	420		
400	0	40	80	120	160	200	240	280	320	360	400		
380	0	38	76	114	152	190	228	266	304	342	380		
360	0	36	72	108	144	180	216	252	288	324	360		
340	0	34	68	102	136	170	204	238	272	306	340		
320	0	32	64	96	128	160	192	224	256	288	320		
300	0	30	60	90	120	150	180	210	240	270	300		
280	0	28	56	84	112	140	168	196	224	252	280		
260	0	26 X	52	78 X	104	130 *	156	182 X	208	234 X	260		
240	0	24 X	48	72 X	96	120 X	144	168 X	192	216 X	240		
220	0	22 Ж	44	66 X	88	110 *	132	154 *	176	198 X	220		
200	0	20 Ж	40	60 X	80	100 ×	120	140 X	160	180 X	200		
180	0	18 X	36	54 X	72	90 X	108	126 X	144	162 X	180		
160	0	16 X	32	48 X	64	80 X	96	112 *	128	144 X	160		

#### NOTE :

TABLE GIVING POSITIONS ON TRANSITION CURVES AT WHICH SLOPE STAKES SHOULD BE SET, CONSTRUCTION AND FINAL CROSS-SECTIONS TAKEN, FINE GRADING STAKES (BLUE TOP) SET, AND FORM STAKES SET (CONCRETE PAVEMENT ONLY).

\* DENOTES ADDITIONAL STAKING POSITIONS FOR USE WITH CONCRETE PAVEMENT ONLY.

TABLE 2

### CURVE WIDENING TABLES

#### SU DESIGN VEHICLE

COMPONENT	SIZE		
OVERALL WIDTH (u)	8.5 ft		
WHEELBASE (L)	20 ft		
FRONT OVERHANG (A)	4 ft		

#### LATERAL CLEARANCE

LANE WIDTH	CLEARANCE (C)
8 ft	1 ft
9 ft	1.5 ft
10 ft	2 ft
11 ft	2.5 ft
12 ft	3 ft
16 ft	5 ft

### IGRDS HA.TBL TABLES

### RELATIVE GRADIENTS

### EFFECTIVE WIDTHS

NUMBER		EF	FECTIVE	WIDTHS (	W)		EFFECTIVE
OF LANES	8 ft LANES	9 ft LANES	10 ft LANES	11 ft LANES	12 ft LANES	16 ft LANES	WIDTH FACTOR (f)
1	8.0	9.0	10.0	11.0	12.0	16.0	1
1.5	9.6	10.8	12.0	13.2	14.4	19.2	1.2
2	12.0	13.5	15.0	16.5	18.0	24.0	1.5
3	16.0	18.0	20.0	22.0	24.0	32.0	2
4	32.0	36.0	40.0	44.0	48.0	64.0	4
5	40.0	45.0	50.0	55.0	60.0	80.0	5
6	48.0	54.0	60.0	66.0	72.0	96.0	6
7	56.0	63.0	70.0	77.0	84.0	112.0	7
8	64.0	72.0	80.0	88.0	96.0	128.0	8

DESIGN		ATIVE NT (rg)	MIN. TRANSITION LENGTH IN FEET				
SPEED VD MPH	UP TO	4 OR MORE	2 SECOND RULE				
	LANES	LANES	URBAN	RURAL			
20	0.75	1.14	100	60			
25	0.71	1.07	100	80			
30	0.67	1.00	100	100			
35	0.63	0.93	120	120			
40	0.58	0.86	120	120			
45	0.54	0.81	140	140			
50	0.50	0.75	160	160			
55	0.47	0.69	180	180			
60	0.45	0.67	180	180			
65	0.41	0.62	200	200			
70	0.40	0.60	220	220			

#### **DEFINITIONS**

- A FRONT OVERHANG OF DESIGN VEHICLE FROM APPROPRIATE TABLE.
- C LATERAL CLEARANCE OF DESIGN VEHICLE FROM APPROPRIATE TABLE.
- E SUPERELEVATION RATE IN DECIMAL FROM APPROPRIATE TABLE OR CALCULATED PER AASHTO METHOD 5.
- FA CALCULATED WIDTH OF OVERHANG FOR DESIGN VEHICLE.
- L WHEELBASE OF DESIGN VEHICLE FROM APPROPRIATE TABLE.
- U CALCULATED TRACK WIDTH OF DESIGN VEHICLE.

- Lr LENGTH OF SPIRAL OR SUPERELEVATION RUNOFF SECTION.
- Lt LENGTH OF TANGENT RUNOUT SECTION.
- M MULTIPLE LANE (2 + ) FACTOR.
- N NUMBER OF LANES.
- Pw PAVEMENT WIDTH.
- R RADIUS OF CURVE.
- rg RELATIVE GRADIENT FROM APPROPRIATE TABLE.

- u TRACK WIDTH OF DESIGN VEHICLE FROM APPROPRIATE TABLE.
- V<sub>D</sub> DESIGN VELOCITY.
- w CALCULATED WIDENING.
- W EFFECTIVE WIDTH FROM APPROPRIATE TABLE.
- WC CALCULATED TOTAL CURVE WIDTH.
- Wn WITDH OF LANE.
- Z CALCULATED EXTRA WIDTH ALLOWANCE.

### GENERAL DESIGN CONSIDERATIONS

- WHERE PAVEMENT WIDENING IS REQUIRED, THE APPROPRIATE WIDENING IS ADDED TO THE LANE WIDTH WHEN CALCULATING THE SUPERELEVATION RUNOFF SECTION (Lr).
- THE COMPUTED TRANSITION LENGTH (Lr) IS ROUNDED UP TO THE NEAREST TWENTY
  FOOT INCREMENT. COMPUTED LENGTHS THAT FALL ON THE TWENTY FOOT
  INCREMENT ARE NOT ROUNDED.
- 3. WHEN THE SUPERELEVATION RUNOFF SECTION (Lr) IS CALCULATED, IT MUST BE COMPARED WITH THE MINIMUM VALUE LISTED IN THE APPROPRIATE COLUMN ON THE RELATIVE GRADIENT TABLE.
- 4. TANGENT RUNOUT SECTION (Lt) IS ALWAYS ACHIEVED OUTSIDE OF THE TRANSITION.
- 5. NO PAVEMENT WIDENING IS REQUIRED FOR URBAN ROADWAYS.
- NO PAVEMENT WIDENING IS REQUIRED FOR RURAL ROADWAYS WITH A CURVE RADIUS GREATER THAN 2865 FEET.

- 7. NO PAVEMENT WIDENING IS REQUIRED FOR RURAL ROADWAYS WITH 12 FOOT WIDE LANES AND A CURVE RADIUS GREATER THAN 881 FEET.
- 8. PAVEMENT WIDENING IS APPLIED ONLY WHEN CALCULATED WIDENING (w) IS EQUAL TO OR GREATER THAN 2 FEET.
- 9. WHEN CALCULATING WIDENING (W) FOR MULTI-LANE RURAL ROADWAYS, WIDENING IS FIRST CALCULATED USING THE SINGLE LANE WIDTH FOR "W" AND THE ANSWER (W) IS THEN MUTIPLIED BY THE MULTIPLE LANE FACTOR (M). FOR FOUR LANE UNDIVIDED PAVEMENTS (48"), THE Lr IS 1.5 TIMES (M=1.5) THE CORRESPONDING LENGTH FOR TWO LANE HIGHWAYS; AND FOR SIX LANE UNDIVIDED PAVEMENTS (72"), THE Lr IS TWO TIMES (M=2) THE CORRESPONDING LENGTH FOR TWO LANE HIGHWAYS.
- 10. CALCULATED WIDENING IS ROUNDED UP TO THE NEAREST 0.1 FOOT.

## FORMULAS USED TO CALCULATE TRANSITION LENGTH (Lr) AND WIDENING (W)

Lr=(100WE)/rg (NO WIDENING REQUIRED)

Lr = [100(W + w/2) E]/rg (WIDENING REQUIRED)

$$U = u + R - \sqrt{R^2 - L^2}$$

$$Z = (V_D / \sqrt{R})$$

$$W = W_C - 2W_n$$

Lr=M[100(Pw/N +w/N) E]/rg (MULTI-LANE WIDENING REQUIRED)

$$F = \sqrt{R^2 + A(2L + A)} - R$$

$$W_C = N(U + C) + F + Z_A$$

FOR SOLVED PROBLEMS USING THIS METHODOLOGY, SEE THE EXAMPLES ON PAGE 801.19.

## METHODOLOGIES FOR CALCULATING TC-5 VALUES

REV. 1/07 801.18

VIRGINIA DEPARTMENT OF TRANSPORTATION

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$$U = u + R - \sqrt{R^2 - L^2}$$

$$U = 8.5 + 1000 - \sqrt{(1000)^2 - (20)^2}$$

$$U = 8.70002$$

$$F_A = \sqrt{R^2 + A (2L + A)} - R$$

$$F_A = \sqrt{(1000)^2 + 4E 2(20) + 4J} - 1000$$

$$F_A = .087996$$

$$Z = (V_D / \sqrt{R})$$
  
 $Z = (50 / \sqrt{1000})$   
 $Z = 1.58$ 

$$W_C = 2 (U + C) + F_A + Z$$
  
 $W_C = 2(8.70002 + 2) + 0.08996 + 1.58$   
 $W_C = 23.0692$ 

$$w = W_C - 2W_n = 23.069 - 2(10) = 3.069$$

(R<2865 & w>2 THEREFORE WIDENING IS REQUIRED)
Lr = [100 (W +w/2) E] / rg
Lr = [100 (10 +3.068/2) .076] / 0.50
Lr = 175.56 (180 ROUNDED)

## RURAL EXAMPLE 72 FT PAVEMENT WIDTH (IGRDS - 3 LANES AT 12 FT)

## COMPUTE FOR 24' PAVEMENT WIDTH (IGRDS 1@ 12')

$$U = u + R - \sqrt{R^2 - L^2}$$

$$U = 8.5 + 600 - \sqrt{(600)^2 - (20)^2}$$

$$U = 8.8334$$

$$F_{A} = \sqrt{R^{2} + A (2L + A)} - R$$

$$F_{A} = \sqrt{(600)^{2} + 4[2(20) + 4] - 600}$$

$$F_{A} = .14665$$

$$Z = (V_D / \sqrt{R})$$
  
 $Z = (40 / \sqrt{600})$   
 $Z = 1.6329$ 

$$W_C = 2 (U + C) + F_A + Z$$
  
 $W_C = 2(8.8334 + 3.0) + .14665 + 1.632$   
 $W_C = 25.4464$ 

$$W = W_C - 2W_D = 25.4455 - 2(12) = 1.4464(1.5)$$

FOR 72' PAVEMENT WIDTH w = 3(1.5) = 4.5

## (R<881 & w>2 THEREFORE WIDENING IS REQUIRED)

Lr = M[100(Pw/N +w/N) E]/rg Lr = 2[100(72/6 +4.5/6) 0.077]/0.58 Lr = 2[100(12.75)0.77]/0.58Lr = 2(98.175/0.58)

Lr = 2(169.2672414)

Lr = 338.5344828 (ROUNDED TO 340)

### URBAN EXAMPLES

24 FT PAVEMENT WIDTH (IGRDS - 1 LANE AT 12 FT)

## 66 FT PAVEMENT WIDTH (IGRDS - 3 LANES AT 11 FT)

$$V_D = 40 \text{ MPH}$$
 R = 600 FT  
 $W_n = 22 \text{ FT}$  rg = 0.58  
F = 0.04 (4% PFR PAGE 801.25)

TC-5

						PAVEMENT WIDTH								
RADIUS	E	F	DV	NC	W <u>≤</u> 72 FT.	W > 72 FT								
(FEET)	(%)		(MPH)	(MPH)		Lr (FEET)								
<u>&gt;</u> 975	2.1	.161	45	45	140									
750	2.1	.161	45	41	140									
700	2.1	.164	44	40	120									
550	2.1	.178	40	37	120	NOTE:								
475	2.1	.186	38	35	120	FOR PAVEMENTS WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN								
375	2.1	.197	35	32	120	ABSOLUTE MINIMUM Lr OF 90 FEET.								
300	2.1	.211	32	30	100									
250	2.1	.221	30	28	100									
200	2.1	.240	27	25	100									
175	2.1	.252	25	24	90									
100	2.1	.290	21	20	90									
90	2.1	.300	20	20	90									

SUMMARY OF STD. TC-5ULS (URBAN-LOW SPEED) DESIGN FACTORS

## DESIGN FACTORS FOR A DESIGN SPEED OF 20 MPH (URBAN) USING E= 4% MAX.

				TOND		MENT W		47. 1	/////				
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)	IGRD	S EQUI	L	S (NUM	IBER OF	LANES	S AT LA	ANE WID	TH)			
		1@	12'	1.5	⊉ 12'	2 @	12'	3 @	10'	3 @	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
15000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
10000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
7000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
5000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
4000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
3000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2500	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2250	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1750	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1500	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1300	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1150	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
900	2.1	100	100	100	100	100	100	100	100	100	100	100	100
800	2.3	92	100	92	100	92	100	92	100	92	100	92	100
750	2.3	92	100	92	100	92	100	92	100	92	100	92	100
700	2.4	88	100	88	100	88	100	88	100	88	100	88	100
650	2.5	84	100	84	100	84	100	84	100	84	100	84	100
600	2.5	84	100	84	100	84	100	84	100	84	100	84	100
550	2.6	81	100	81	100	81	100	81	100	81	100	81	100
500	2.7	78	100	78	100	78	100	78	100	78	100	78	100
475	2.7	78	100	78	100	78	100	78	100	78	100	78	100
450	2.8	75	100	75	100	75	100	75	100	75	100	75	100
425	2.8	75	100	75	100	75	100	75	100	75	100	75	100
400	2.9	73	100	73	100	73	100	73	100	73	100	73	100
375	3.0	70	100	70	100	70	100	70	100	70	100	70	100
350	3.1	68	100	68	100	68	100	68	100	68	100	68	100
325	3.1	68	100	68	100	68	100	68	100	68	100	68	100
300	3.2	66	100	66	100	66	100	66	100	66	100	79	120
280	3.3	64	100	64	100	64	100	64	100	64	100	77	120
265	3.4	62	100	62	100	62	100	62	100	62	100	75	120
250	3.5	60	100	60	100	60	100	60	100	72	120	72	120
235	3.5	60	100	60	100	60	100	60	100	72	120	72	120
220	3.6	59	100	59	100	59	100	59	100	70	120	70	120
205	3.7	57	100	57	100	57	100	57	100	69	120	69	120
190	3.8	56	100	56	100	56	100	67	120	67	120	78	140
175	3.9	54	100	54	100	54	100	65	120	65	120	76	140
160	3.9	54	100	54	100	54	100	65	120	65	120	76	140
145	4.0	53	100	53	100	53	100	63	120	63	120	74	140
130	4.0	53	100	53	100	53	100	63	120	63	120	74	140
<b>9</b> 127	4.0	53	100	53	100	53	100	63	120	63	120	74	140

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE LT VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM LT OF 100 FEET.

#### LEGEND

- C- RATE OF CHANGE OF SIDE FRICTION (f) IN FT./SEC.
- e- SUPERELEVATION RATE IN PERCENT.
- f- FRICTION FACTOR.
- Lr- LENGTH OF SUPERELEVATION RUNOFF SECTION.
- Lt- LENGTH OF TANGENT RUNOUT SECTION
- R- RADIUS OF CURVE.
- DV- DESIGN VELOCITY UTILIZING SUPERELEVATION.
- NC- MAXIMUM VELOCITY WITH NO SUPERELEVATION (NORMAL CROWN).

#### URBAN LOW SPEED DESIGN TABLE

DV/NC	MAX. f	С	Lr
45	0.161	2.75	140
40	0.178	3.00	120
35	0.197	3.25	120
30	0.221	3.50	100
25	0.252	3.75	90
20	0.300	4.00	90

FRICTION FACTORS (f) FOR ODD VELOCITIES NOT LISTED SHOULD BE DERIVED BY INTERPOLATION.

FOR Lr LENGTHS FOR INTERMEDIATE VELOCITIES NOT LISTED IN TABLE USE THE Lr FOR NEXT LOWER VELOCITY IN TABLE.

#### GENERAL DESIGN CONSIDERATIONS

- WHEN "URBAN LOW SPEED" DESIGNS UTILIZE SUPERELEVATION, THEY WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE NORMAL CROWN (TYPICALLY 2%) AND THE APPROXIMATE MAXIMUM SAFE SPEED (DV) AFFORDED THEREBY.
- 2. WHEN "URBAN LOW SPEED DESIGN" WITH NO SUPERELEVATION, THE APPROXIMATE MAXIMUM SAFE SPEED (NC) IS CALCULATED USING A NEGATIVE NORMAL CROWN (TYPICALLY -2%).
- 3. WHEN THE CURVE IS SUPERELEVATED, THE Lr IS APPLIED IN THE SAME MANNER AS IN URBAN CONDITIONS WITH THE TANGENT RUNOUT SECTION (Lt) BEING EQUAL TO THE Lr VALUE. THE CROWN RUNOUT SECTION (Lt) IS ALWAYS ACHIEVED OUTSIDE OF THE TRANSITION (Lr).
- 4. PLEASE NOTE THAT THE RADIUS VALUES LISTED ON PAGE 801.20 HAVE BEEN ROUNDED UP TO THE NEAREST TWENTY FIVE FOOT INCREMENT.

#### EXAMPLES

 $DV = 21 \, mph$ 

e = +2.1 %

f = 300-[1/5(0.300-0.252)]=0.2904 (ROUND TO 0.29)

Lr = 47.2 f DV/C = 47.2(0.29)(21)/4 = 71.862 FT.

- 71.862 <90 THEREFORE Lr-90 FT.

Rmin. =  $(21)^2/15(0.021+0.29)=94.53376206$  FT.

NC = 37 mph

e = -2.1 %

f = 0.197-[2/5(0.197-0.178)]=0.1894 (ROUND TO 0.189)

Rmin. =  $(37)^2 / 15(-0.021 + 0.189) = 543.2539683$  FT.

TC-5	DESIG	GN F									25	MPH	
				(URB	AN) (	JSIN	3 E=	4 %	MAX	•			
					F	PAVEME	IW TM:	HTC					
RADIUS	E	24	FT	36 F	Т	48 F	T	60 F	Ŧ	66 F	T	72 F	· T
(FEET)	(%)		IGF	RDS EQ	UIVALEI	NTS (N	UMBER	OF LA	NES A	T LANE	WIDTH	1)	
		1@	12'	1.5 @	12'	2 @	12'	3 @	10'	3 @	2 11'	3 ⊚	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
15000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
10000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
7000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
5000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
4000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
3000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2500	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2250	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1750	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1500	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1300	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1150	2.3	92	100	92	100	92	100	92	100	92	100	92	100
1000	2.4	88	100	88	100	88	100	88	100	88	100	88	100
900	2.5	84	100	84	100	84	100	84	100	84	100	84	100
800	2.6	81	100	81	100	81	100	81	100	81	100	81	100
750	2.7	78	100	78	100	78	100	78	100	78	100	78	100
700	2.8	75	100	75	100	75	100	75	100	75	100	75	100
650	2.9	73	100	73	100	73	100	73	100	73	100	73	100
600	2.9	73	100	73	100	73	100	73	100	73	100	73	100
550	3.0	70	100	70	100	70	100	70	100	70	100	84	120
500	3.2	66	100	66	100	66	100	66	100	66	100	79	120
475	3.2	66	100	66	100	66	100	66	100	66	100	79	120
450	3.3	64	100	64	100	64	100	64	100	77	120	77	120
425	3.4	62	100	62	100	62	100	62	100	75	120	75	120
400	3.4	62	100	62	100	62	100	62	100	75	120	75	120
375	3.5	60	100	60	100	60	100	60	100	72	120	72	120
350	3.6	59	100	59	100	59	100	70	120	70	120	82	140
325	3.7	57	100	57	100	57	100	69	120	69	120	80	140
300	3.8	56	100	56	100	56	100	67	120	67	120	78	140
280	3.9	54	100	54	100	54	100	65	120	76	140	76	140
265	3.9	54	100	54	100	54	100	65	120	76	140	76	140
250	4.0	53	100	53	100	63	120	63	120	74	140	74	140
235	4.0	53	100	53	100	63	120	63	120	74	140	74	140
220	4.0	53	100	53	100	63	120	63	120	74	140	74	140
<b>⊕</b> 204	4.0	53	100	53	100	63	120	63	120	74	140	74	140

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 100 FEET.

**⊕**MINIMUM ALLOWABLE RADIUS

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 1/07 801.22

## DESIGN FACTORS FOR A DESIGN SPEED OF 30 MPH (URBAN) USING E=4% MAX.

							F	PAVEMEN	IT WIDT	Н			
RADIUS	E	24	FT	36 F	Т	48 F	Т	60 F	Т	66 F	Т	72 F	Т
(FEET)	(%)				IGRDS E	QUIVALE	ENTS (N	IUMBER	OF LANE	S AT L	ANE WIL	TH)	
		1@	12'	1.5	⊉ 12'	2 @	12'	3 @	10'	3 @	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
15300	2.1	100	100	100	100	100	100	100	100	100	100	100	100
10000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
7000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
5300	2.1	100	100	100	100	100	100	100	100	100	100	100	100
4000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
3000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2530	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2250	2.1	100	100	100	100	100	100	100	100	100	100	100	100
2000	2.1	100	100	100	100	100	100	100	100	100	100	100	100
1750	2.2	96	100	96	100	96	100	96	100	96	100	96	100
1500	2.4	88	100	88	100	88	100	88	100	88	100	88	100
1000	2.5	84	100	84	100	84	100	84	100	84	100	84	100
1150	2.6	81	100	81	100	81	100	81	100	81	100	81	100
1000	2.8	75	100	75	100	75	100	75	100	75	100	90	120
900	2.9	73	100	73	100	73	100	73	100	73	100	87	120
800	3.0	70	100	70	100	70	100	70	100	70	100	84	120
750	3.1	68	100	68	100	68	100	68	100	82	120	82	120
700	3.2	66	100	66	100	66	100	66	100	79	120	79	120
650	3.3	64	100	64	100	64	100	64	100	77	120	77	120
600	3.4	62	100	62	100	62	100	75	120	75	120	87	140
570	3.5	60	100	60	100	60	100	72	120	72	120	84	140
500	3.6	59	100	59	100	59	100	70	120	70	120	82	140
475	3.7	57	100	57	100	57	100	69	120	80	140	80	140
450	3.8	56	100	56	100	67	120	67	120	78	140	78	140
425	3.8	56	100	56	100	67	120	67	120	78	140	78	140
400	3.9	54	100	54	100	65	120	65	120	76	140	76	140
375	3.9	54	100	54	100	65	120	65	120	76	140	76	140
350	4.0	53	100	53	100	63	120	63	120	74	140	84	160
325	4.0	53	100	53	100	63	120	63	120	74	140	84	160
<b>⊕</b> 300	4.0	53	100	53	100	63	120	63	120	74	140	84	160

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 100 FEET.

TC-5

## DESIGN FACTORS FOR A DESIGN SPEED OF 35 MPH (URBAN) USING E= 4% MAX.

							PAVE	MENT W	IDTH				
RADIUS	E	24	FT	36 F1	-	48 F	Т	60 F	Т	66 F	Т	72 F	Т
(FEET)	(%)			IGRDS E	EQUIVALE	ENTS (N	UMBER	OF LAN	ES AT L	ANE WI	OTH)		
		1@	12'	1.5 @	12'	2 @	12'	3 @	10'	3 @	2 11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
15000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
10000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
7000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
5000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
4000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
3000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
2500	2.1	120	120	120	120	120	120	120	120	120	120	120	120
2250	2.2	115	120	115	120	115	120	115	120	115	120	115	120
2000	2.4	105	120	105	120	105	120	105	120	105	120	105	120
1750	2.5	101	120	101	120	101	120	101	120	101	120	101	120
1500	2.7	94	120	94	120	94	120	94	120	94	120	94	120
1300	2.8	90	120	90	120	90	120	90	120	90	120	90	120
1150	3.0	84	120	84	120	84	120	84	120	84	120	84	120
1000	3.2	79	120	79	120	79	120	79	120	79	120	92	140
900	3.3	77	120	77	120	77	120	77	120	77	120	90	140
800	3.5	72	120	72	120	72	120	72	120	84	140	84	140
750	3.5	72	120	72	120	72	120	72	120	84	140	84	140
700	3.6	70	120	70	120	70	120	70	120	82	140	82	140
650	3.7	69	120	69	120	69	120	69	120	80	140	91	160
600	3.8	67	120	67	120	67	120	78	140	78	140	89	160
550	3.9	65	120	65	120	65	120	76	140	76	140	87	160
500	4.0	63	120	63	120	63	120	74	140	74	140	84	160
475	4.0	63	120	63	120	63	120	74	140	74	140	84	160
450	4.0	63	120	63	120	63	120	74	140	74	140	84	160
425	4.0	63	120	63	120	63	120	74	140	74	140	84	160
<b></b> 420	4.0	63	120	63	120	63	120	74	140	74	140	84	160

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE LT VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM LT OF 120 FEET.

## DESIGN FACTORS FOR A DESIGN SPEED OF 40 MPH (URBAN) USING E= 4 % MAX.

							P#	AVEMEN	T WIDT	Ή			
RADIUS	E	24	FT	36 F	Т	48 F	Т.	60 F	- T	66 F	Т	72 I	ŦΤ
(FEET)	(%)				IGRDS E	QUIVAL	ENTS	(NUMBE	R OF I	ANES	AT LA	NE MID.	ГН)
		1@	12'	1.5 @	12'	2 @	12'	3 @	10'	3 ⊚	11'	3 ⊚	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
15000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
10000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
7000	2.1	120	120	120	120	120	120	120	40	120	120	120	120
5000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
4000	2.1	120	120	120	120	120	120	120	120	120	120	120	120
3000	2.2	115	120	115	120	115	120	115	120	115	120	115	120
2500	2.4	105	120	105	120	105	120	105	120	105	120	105	120
2250	2.5	101	120	101	120	101	120	101	120	101	120	101	120
2000	2.7	94	120	94	120	94	120	94	120	94	120	94	120
1750	2.8	90	120	90	120	90	120	90	120	90	120	90	120
1500	3.0	84	120	84	120	84	120	84	120	84	120	98	140
1300	3.2	79	120	79	120	79	120	79	120	92	140	92	140
1150	3.3	77	120	77	120	77	120	77	120	90	140	90	140
1000	3.5	72	120	72	120	72	120	84	140	84	140	96	160
900	3.7	69	120	69	120	69	120	80	140	91	160	91	160
800	3.8	67	120	67	120	67	120	78	140	89	160	89	160
750	3.9	65	120	65	120	76	140	76	140	87	160	97	180
700	3.9	65	120	65	120	76	140	76	140	87	160	97	180
650	4.0	63	120	63	120	74	140	74	140	84	160	95	180
600	4.0	63	120	63	120	74	140	74	140	84	160	95	180
<b>⊛</b> 563	4.0	63	120	63	120	74	140	74	140	84	160	95	180

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 120 FEET.

TC-5

## DESIGN FACTORS FOR A DESIGN SPEED OF 45 MPH (URBAN) USING E= 4% MAX.

							PAVE	MENT W	IDTH				
RADIUS	E	24	FT	36 F	Γ	48 F	Т	60 F	Т	66 F	Т	72 F	Т
(FEET)	(%)			IGRDS I	EQUIVALI	ENTS (N	UMBER	OF LANE	S AT L	ANE WIE	OTH)	•	
		1 @	12'	1.5 @	⊉ 12'	2 @	12'	3 @	10'	3 @	11'	3 ⊚	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	140	140	140	140	140	140	140	140	140	140	140	140
15000	2.1	140	140	140	140	140	140	140	140	140	140	140	140
10000	2.1	140	140	140	140	140	140	140	140	140	140	140	140
7000	2.1	140	140	140	140	140	140	140	140	140	140	140	140
5000	2.1	140	140	140	140	140	140	140	140	140	140	140	140
4000	2.1	140	140	140	140	140	140	140	140	140	140	140	140
3000	2.5	118	140	118	140	118	140	118	140	118	140	118	140
2500	2.7	109	140	109	140	109	140	109	140	109	140	109	140
2250	2.8	105	140	105	140	105	140	105	140	105	140	105	140
2000	2.9	102	140	102	140	102	140	102	140	102	140	102	140
1750	3.1	95	140	95	140	95	140	95	140	95	140	95	140
1500	3.3	90	140	90	140	90	140	90	140	90	140	102	160
1300	3.5	84	140	84	140	84	140	84	140	96	160	96	160
1150	3.7	80	140	80	140	80	140	80	140	91	160	103	180
1000	3.9	76	140	76	140	76	140	87	160	87	160	97	180
900	4.0	74	140	74	140	74	140	84	160	95	160	95	180
800	4.0	74	140	74	140	74	140	84	160	95	180	95	180
750	4.0	74	140	74	140	74	140	84	160	95	180	95	180
<b>⊕</b> 732	4.0	74	140	74	140	74	140	84	160	95	180	95	180

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 140 FEET.

## DESIGN FACTORS FOR A DESIGN SPEED OF 50 MPH (URBAN) USING E= 4 % MAX.

							PAVE	MENT	WIDTH				
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)			IGRI	OS EQU	IIVALEN	TS (NU	MBER	OF LAN	IES AT	LANE	WIDTH:	)
		1 @	12'	1.5 @	⊉ 12'	2 @	! 12'	3 @	10'	3 @	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	160	160	160	160	160	160	160	160	160	160	160	160
15000	2.1	160	160	160	160	160	160	160	160	160	160	160	160
10000	2.1	160	160	160	160	160	160	160	160	160	160	160	160
7000	2.1	160	160	160	160	160	160	160	160	160	160	160	160
5000	2.1	160	160	160	160	160	160	160	160	160	160	160	160
4000	2.4	140	160	140	160	140	160	140	160	140	160	140	160
3000	2.7	125	160	125	160	125	160	125	160	125	160	125	160
2500	2.9	116	160	116	160	116	160	116	160	116	160	116	160
2250	3.1	109	160	109	160	109	160	109	160	109	160	109	160
2000	3.2	105	160	105	160	105	160	105	160	105	160	105	160
1750	3.4	99	160	99	160	99	160	99	160	99	160	112	180
1500	3.6	94	160	94	160	94	160	94	160	94	160	105	180
1300	3.8	89	160	89	160	89	160	89	160	100	180	111	200
1150	3.9	87	160	87	160	87	160	87	160	97	180	108	200
1000	4.0	84	160	84	160	84	160	84	160	95	180	105	200
929 🛞	4.0	84	160	84	160	84	160	84	160	95	180	105	200

#### NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 160 FEET.

TC-5

## DESIGN FACTORS FOR A DESIGN SPEED OF 55 MPH (URBAN) USING E= 4% MAX.

						PAVE	MENT W	IDTH				
E	24 1	- T	36 F	Г	48 F	Т	60 F	Т	66 F	Т	72 F	Т
(%)			IGRDS E	EQUIVALE	ENTS (N	UMBER (	OF LANE	S AT L	ANE WIE	)TH)		
	1@	12'	1.5 @	12'	2 @	12'	3 @	10'	3 @	11'	3 @	12'
	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
2.1	180	180	180	180	180	180	180	180	180	180	180	180
2.1	180	180	180	180	180	180	180	180	180	180	180	180
2.1	180	180	180	180	180	180	180	180	180	180	180	180
2.1	180	180	180	180	180	180	180	180	180	180	180	180
2.3	165	180	165	180	165	180	165	180	165	180	165	180
2.6	146	180	146	180	146	180	146	180	146	180	146	180
3.0	126	180	126	180	126	180	126	180	126	180	126	180
3.3	115	180	115	180	115	180	115	180	115	180	115	180
3.4	112	180	112	180	112	180	112	180	112	180	112	180
3.6	105	180	105	180	105	180	105	180	105	180	117	200
3.8	100	180	100	180	100	180	100	180	100	180	111	200
3.9	97	97 180 97		180	97	180	97	180	108	200	108	200
4.0	95	180	95	180	95	180	95	180	105	200	116	220
4.0	95	180	95	180	95	180	95	180	105	200	116	220
	2.1 2.1 2.1 2.1 2.3 2.6 3.0 3.3 3.4 3.6 3.8 3.9 4.0	1 @ Lt   2.1	(%)  1 @ 12'  Lt	(%) IGRDS E  1 @ 12'	(%)	(%)	E	E	(%)   IGRDS EQUIVALENTS (NUMBER OF LANES AT L   1 @ 12'   1.5 @ 12'   2 @ 12'   3 @ 10'   Lt   Lr   Lt   Lr   Lt   Lr   Lt   Lr   Lt   Lr   Lt   Lr   Ls   Lr   Ls   Ls   Ls   Ls   Ls	E	E	E

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 180 FEET.

## DESIGN FACTORS FOR A DESIGN SPEED OF 60 MPH (URBAN) USING E= 4 % MAX.

					F	PAVEME	NT WID	TH					
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)			IGRI	DS EQL	JIVALEN	TS (NU	MBER	OF LAN	IES AT	LANE	WIDTH:	)
		1@	12'	1.5 @	⊉ 12'	2 @	12'	3 @	10'	3 @	2 11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
20000	2.1	180	180	180	180	180	180	180	180	180	180	180	180
15000	2.1	180	180	180	180	180	180	180	180	180	180	180	180
10000	2.1	180	180	180	180	180	180	180	180	180	180	180	180
7000	2.1	180 180 180 180		180	180	180	180	180	180	180	180	180	180
5000	2.6	146	180	146	180	146	180	146	180	146	180	146	180
4000	2.9	131	180	131	180	131	180	131	180	131	180	131	180
3000	3.3	115	180	115	180	115	180	115	180	115	180	115	180
2500	3.6	105	180	105	180	105	180	105	180	105	180	117	200
2250	3.7	103	180	103	180	103	180	103	180	114	200	114	200
2000	3.9	97	180	97	180	97	180	97	180	108	200	119	220
1750	4.0	95	180	95	180	95	180	95	180	105	200	116	220
<b>⊕</b> 1505	4.0	95	180	95	180	95	180	95	180	105	200	116	220

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS WITH AN ABSOLUTE MINIMUM Lr OF 180 FEET.

TC-5 DE	ESIGN F	ACT(	DRS	FOF	R A	DESI	IGN	SPE	ED C	)F 2	0 M	PH	RUR	AL)	USIN	IG E	= 8%	: МА	X.	
DESIGN VELC	CITY=20	WIE	)TH=16	FT	WIDT	H= 18	FT	WID	TH=20	FT	WID	TH=22	FT	WID:	TH=24	FT	WID	TH=48	FT	
						IGRE	OS EQU	IIVALEI	NTS (N	IUMBER	OF L	ANES	AT LA	NE WID	TH)					
			1@8	ı		1@ 9	)'		1 @ 10	)'		1 @ 11			1@ 1.	2'	2	2 @ 12		
RADIUS(FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	W	Lt	Lr	W	Lt	Lr	w	Lt	Lr	W	
20000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
15000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
10000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
7000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	NOTE:
5000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
4000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	Lt, Lr & w VALUES IN FEET.
3000	2.1	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
2500	2.1	13	60	3.6	14	60	2.6	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
2250	2.1	13	60	3.7	14	60	2.7	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
2000	2.1	13	60	3.7	14	60	2.7	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
1750	2.1	13	60	3.8	14	60	2.8	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
1500	2.1	13	60	3.9	14	60	2.9	60	60	0.0	60	60	0.0	60	60	0.0	60	60	0.0	
1300	2.1	13	60	4.0	14	60	3.0	15	60	2.0	60	60	0.0	60	60	0.0	60	60	0.0	
1150	2.1	13	60	4.1	14	60	3.1	15	60	2.0	60	60	0.0	60	60	0.0	60	60	0.0	
1000	2.4	13	60	4.2	14	60	3.2	15	60	2.2	53	60	0.0	53	60	0.0	53	60	0.0	
900	2.6	13	60	4.3	14	60	3.3	15	60	2.3	49	60	0.0	49	60	0.0	65	80	0.0	
800	2.9	13	60	4.4	14	60	3.4	15	60	2.4	44	60	0.0	44	60	0.0	58	80	0.0	
750	3.1	13	60	4.4	14	60	3.4	15	60	2.4	41	60	0.0	41	60	0.0	55	80	0.0	
700	3.3	13	60	4.5	14	60	3.5	14	60	2.5	39	60	0.0	39	60	0.0	51	80	0.0	
650	3.4	13	60	4.6	14	60	3.6	14	60	2.6	38	60	0.0	38	60	0.0	62	100	0.0	
600	3.7	13	60	4.7	14	60	3.7	14	60	2.7	35	60	0.0	35	60	0.0	57	100	0.0	
550	3.9	13	60	4.8	14	60	3.8	14	60	2.8	33	60	0.0	44	80	0.0	54	100	0.0	
500	4.2	13	60	4.9	18	80	3.9	19	80	2.9	40	80	0.0	40	80	0.0	60	120	0.0	
475	4.3	16	80	5.0	18	80	4.0	19	80	3.0	20	80	2.0	40	80	0.0	31	120	2.0	∰ MINIMUM ALLOWABLE RADIUS
450	4.5	16	80	5.1	18	80	4.1	19	80	3.1	20	80	2.0	38	80	0.0	31	120	2.2	
425	4.7	16	80	5.2	18	80	4.2	19	80	3.2	20	80	2.2	36	80	0.0	30	120	2.4	
400	4.8	16	80	5.3	17	80	4.3	19	80	3.3	20	80	2.3	35	80	0.0	35	140	2.6	
375	5.0	16	80	5.4	17	80	4.4	18	80	3.4	24	100	2.4	34	80	0.0	35	140	2.8	
350	5.2	16	80	5.5	17	80	4.5	23	100	3.5	24	100	2.5	41	100	0.0	35	140	3.0	
325	5.4	16	80	5.7	21	100	4.7	23	100	3.7	24	100	2.7	39	100	0.0	35	140	3.4	
300	5.6	20	100	5.8	21	100	4.8	23	100	3.8	24	100	2.8	38	100	0.0	40	160	3.6	
280	5.8	20	100	6.0	21	100	5.0	22	100	4.0	24	100	3.0	30	120	2.0	39	160	4.0	
265	6.0	20	100	6.1	21	100	5.1	22	100	4.1	28	120	3.1	29	120	2.0	39	160	4.2	
250	6.1	19	100	6.3	21	100	5.3	22	100	4.3	28	120	3.3	29	120	2.3	44	180	4.6	
235	6.3	19	100	6.4	21	100	5.4	26	120	4.4	28	120	3.4	29	120	2.4	43	180	4.8	
220	6.5	19	100	6.6	25	120	5.6	26	120	4.6	28	120	3.6	29	120	2.6	43	180	5.2	
205	6.7	23	120	6.8	24	120	5.8	26	120	4.8	27	120	3.8	29	120	2.8	43	180	5.6	
190	6.9	22	120	7.1	24	120	6.1	26	120	5.1	31	140	4.1	33	140	3.1	47	200	6.2	
175	7.2	22	120	7.4	24	120	6.4	29	120	5.4	31	140	4.4	33	140	3.4	46	200	6.8	
160	7.4	22	120	7.7	27	140	6.7	29	140	5.7	31	140	4.7	32	140	3.7	51	220	7.4	
145	7.6	25	140	8.1	27	140	7.1	29	140	6.1	30	140	5.1	36	160	4.1	50	220	8.2	
130	7.9	24	140	8.6	26	140	7.6	32	160	6.6	34	160	5.6	36	160	4.6	53	240	9.2	
105	8.0	24	140	9.2	26	140	8.2	31	160	7.2	33	160	6.2	35	160	5.2	52	240	10.4	
115	0.0																			

REV. 1/07 801.30

## DESIGN FACTORS FOR A DESIGN SPEED OF 25 MPH (RURAL) USING E= 8% MAX.

DESIGN VELC	CITY=25	WIE				TH=18	FT	WIE	TH=20	) FT	WID	TH=22	FT	WIE	TH=24	FT	WID.	TH=48	FT
					IGRD:	S EQU	IVALEN	ITS (N	IUMBEF	ROF	_ANES	AT L	ANE W	IDTH)			•		
			1@8	ı		1@ 9'			1 @ 10	1		1 @ 11	1		1@	12'		2 @ 12	2'
RADIUS(FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
15000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
10000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
7000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
5000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
4000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
3000	2.1	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
2500	2.1	18	80	3.7	19	80	2.7	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
2250	2.1	17	80	3.8	19	80	2.8	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
2000	2.1	17	80	3.9	19	80	2.9	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
1750	2.1	17	80	3.9	19	80	2.9	80	80	0.0	80	80	0.0	80	80	0.0	80	80	0.0
1500	2.4	17	80	4.0	18	80	3.0	20	80	2.0	70	80	0.0	70	80	0.0	70	80	0.0
1300	2.7	17	80	4.1	18	80	3.1	20	80	2.0	63	80	0.0	63	80	0.0	63	80	0.0
1150	2.9	17	80	4.2	18	80	3.2	19	80	2.2	58	80	0.0	58	80	0.0	58	80	0.0
1000	3.3	17	80	4.3	18	80	3.3	19	80	2.3	51	80	0.0	51	80	0.0	64	100	0.0
900	3.6	17	80	4.4	18	80	3.4	19	80	2.4	47	80	0.0	47	80	0.0	59	100	0.0
800	3.9	17	80	4.5	18	80	3.5	19	80	2.5	44	80	0.0	44	80	0.0	54	100	0.0
750	4.1	17	80	4.6	18	80	3.6	19	80	2.6	41	80	0.0	41	80	0.0	62	120	0.0
700	4.3	17	80	4.7	18	80	3.7	19	80	2.7	40	80	0.0	40	80	0.0	59	120	0.0
650	4.6	17	80	4.8	18	80	3.8	19	80	2.8	37	80	0.0	37	80	0.0	55	120	0.0
600	4.8	17	80	4.9	18	80	3.9	19	80	2.9	35	80	0.0	44	100	0.0	62	140	0.0
550	5.1	16	80	5.0	18	80	4.0	23	100	3.0	25	100	2.0	42	100	0.0	36	140	2.0
500	5.3	20	80	5.1	22	100	4.1	23	100	3.1	24	100	2.0	39	100	0.0	41	160	2.2
475	5.5	20	100	5.2	22	100	4.2	23	100	3.2	24	100	2.2	39	100	0.0	40	160	2.4
450	5.7	20	100	5.3	22	100	4.3	23	100	3.3	24	100	2.3	37	100	0.0	40	160	2.6
425	5.8	20	100	5.4	22	100	4.4	23	100	3.4	24	100	2.4	37	100	0.0	40	160	2.8
400	6.0	20	100	5.5	21	100	4.5	23	100	3.5	29	120	2.5	42	120	0.0	45	180	3.0
375	6.2	20	100	5.6	21	100	4.6	27	120	3.6	29	120	2.6	41	120	0.0	45	180	3.2
350	6.4	20	100	5.8	25	120	4.8	27	120	3.8	28	120	2.8	40	120	0.0	44	180	3.6
325	6.7	24	120	5.9	25	120	4.9	27	120	3.9	28	120	2.9	38	120	0.0	49	200	3.8
300	6.9	23	120	6.1	25	120	5.1	27	120	4.1	33	140	3.1	34	140	2.0	49	200	4.2
280	7.1	23	120	6.3	25	120	5.3	31	140	4.3	32	140	3.3	34	140	2.3	48	200	4.6
265	7.3	23	120	6.4	29	140	5.4	31	140	4.4	32	140	3.4	34	140	2.4	53	220	4.8
250	7.4	23	120	6.6	29	140	5.6	30	140	4.6	32	140	3.6	34	140	2.6	53	220	5.2
235	7.6	26	140	6.8	28	140	5.8	30	140	4.8	32	140	3.8	38	160	2.8	52	220	5.6
220	7.7	26	140	7.0	28	140	6.0	30	140	5.0	36	160	4.0	38	160	3.0	52	220	6.0
205	7.9	26	140	7.2	28	140	6.2	34	160	5.2	36	160	4.2	38	160	3.2	56	240	6.4
190	8.0	26	140	7.4	28	140	6.4	34	160	5.4	35	160	4.4	37	160	3.4	56	240	6.8
175	8.0	25	140	7.7	27	140	6.7	33	160	5.7	35	160	4.7	37	160	3.7	55	240	7.4
171 🛞	8.0	25	140	7.8	27	140	6.8	33	160	5.8	35	160	4.8	37	160	3.8	55	240	7.6

NOTE:

Lt, Lr & w VALUES IN FEET.

## DESIGN FACTORS FOR A DESIGN SPEED OF 30 MPH (RURAL) USING E= 8% MAX.

DESIGN VELO	DESIGN VELOCITY=30 WIDTH=16 FT				WIE	DTH=18			)TH=20			)TH=22			H=24	FT	WID.	TH=48	FT
						IGRDS	S EQU	VALEN	ITS (N	UMBER	OF L	ANES	AT LA	ANE W	IDTH)				
			1@ 8'			1@ 9'			1@ 10	'		1 @ 11	·	1	@ 12 <sup>1</sup>		2	@ 12'	
RADIUS (FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
15000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
10000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
7000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
5000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
4000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
3000	2.1	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
2500	2.1	22	100	3.8	23	100	2.8	100	100	0.0	100	100	0.0	100	100	0.0	100	100	0.0
2250	2.2	22	100	3.9	23	100	2.9	96	100	0.0	96	100	0.0	96	100	0.0	96	100	0.0
2000	2.4	21	100	4.0	23	100	3.0	24	100	2.0	88	100	0.0	88	100	0.0	88	100	0.0
1750	2.7	21	100	4.0	23	100	3.0	24	100	2.0	78	100	0.0	78	100	0.0	78	100	0.0
1500	3.1	21	100	4.1	23	100	3.1	24	100	2.0	68	100	0.0	68	100	0.0	68	100	0.0
1300	3.5	21	100	4.3	23	100	3.3	24	100	2.3	60	100	0.0	60	100	0.0	60	100	0.0
1150	3.8	21	100	4.4	23	100	3.4	24	100	2.4	56	100	0.0	56	100	0.0	67	120	0.0
1000	4.2	21	100	4.5	22	100	3.5	24	100	2.5	50	100	0.0	50	100	0.0	60	120	0.0
900	4.6	21	100	4.6	22	100	3.6	24	100	2.6	46	100	0.0	46	100	0.0	64	140	0.0
800	4.9	21	100	4.7	22	100	3.7	24	100	2.7	43	100	0.0	43	100	0.0	60	140	0.0
750	5.2	21	100	4.8	22	100	3.8	24	100	2.8	41	100	0.0	41	100	0.0	57	140	0.0
700	5.4	21	100	4.9	22	100	3.9	23	100	2.9	39	100	0.0	39	100	0.0	63	160	0.0
650	5.6	20	100	5.0	22	100	4.0	23	100	3.0	29	120	2.0	45	120	0.0	60	160	2.0
600	5.9	20	100	5.1	22	100	4.1	28	120	3.1	29	120	2.0	43	120	0.0	46	180	2.2
550	6.1	20	100	5.2	26	120	4.2	28	120	3.2	29	120	2.2	42	120	0.0	45	180	2.4
500	6.4	24	120	5.4	26	120	4.4	27	120	3.4	29	120	2.4	40	120	0.0	50	200	2.8
475	6.6	24	120	5.5	26	120	4.5	27	120	3.5	33	140	2.5	39	120	0.0	50	200	3.0
450	6.8	24	120	5.5	26	120	4.5	27	120	3.5	33	140	2.5	44	140	0.0	50	200	3.0
425	7.0	24	120	5.7	25	120	4.7	32	140	3.7	33	140	2.7	42	140	0.0	54	220	3.4
400	7.1	24	120	5.8	30	140	4.8	31	140	3.8	33	140	2.8	42	140	0.0	54	220	3.6
375	7.3	24	120	5.9	29	140	4.9	31	140	3.9	33	140	2.9	41	140	0.0	54	220	3.8
350	7.5	27	140	6.0	29	140	5.0	31	140	4.0	33	140	3.0	39	160	2.0	54	220	4.0
325	7.7	27	140	6.2	29	140	5.2	30	140	4.2	37	160	3.2	39	160	2.2	58	240	4.4
300	7.9	27	140	6.4	29	140	5.4	35	160	4.4	37	160	3.4	39	160	2.4	58	240	4.8
280	8.0	27	140	6.6	33	160	5.6	35	160	4.6	37	160	3.6	38	160	2.6	57	240	5.2
265	8.0	26	140	6.7	32	160	5.7	35	160	4.7	36	160	3.7	38	160	2.7	57	240	5.4
<b>⊕</b> 250	8.0	26	140	6.9	32	160	5.9	34	160	4.9	36	160	3.9	43	180	2.9	61	260	5.8

NOTE:

Lt, Lr & w VALUES IN FEET.

DECION VELOCIT	V 75	1405	TII 40		WID T			WID 7			\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		ГТ	WID T			T	F11 70	
DESIGN VELOCIT	Y=35	WID	TH=18			H=20			H=22			H=24			H=48	FI	MID	ΓH=72	F I
				IGR	DS EQ	UIVALE	ENTS	(NUMBI	ER OF	LANE	S AT	LANE	WIDTH	)					
			1@9	1		1@ 10	1		1@ 1	1'		@ 12'			2 @ 1	2'		3 @ 1	2'
RADIUS (FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
15000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
10000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
7000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
5000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
4000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
3000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
2500	2.5	28	120	2.9	101	120	0.0	101	120	0.0	101	120	0.0	101	120	0.0	101	120	0.0
2250	2.8	27	120	3.0	29	120	2.0	90	120	0.0	90	120	0.0	90	120	0.0	90	120	0.0
2000	3.0	27	120	3.1	29	120	2.0	84	120	0.0	84	120	0.0	84	120	0.0	84	120	0.0
1750	3.4	27	120	3.2	29	120	2.2	75	120	0.0	75	120	0.0	75	120	0.0	87	140	0.0
1500	3.8	27	120	3.3	29	120	2.3	67	120	0.0	67	120	0.0	67	120	0.0	89	160	0.0
1300	4.3	27	120	3.4	29	120	2.4	59	120	0.0	59	120	0.0	69	140	0.0	88	180	0.0
1150	4.7	27	120	3.5	28	120	2.5	54	120	0.0	54	120	0.0	63	140	0.0	81	180	0.0
1000	5.2	27	120	3.6	28	120	2.6	49	120	0.0	49	120	0.0	65	160	0.0	81	200	0.0
900	5.5	27	120	3.8	28	120	2.8	46	120	0.0	46	120	0.0	62	160	0.0	84	220	0.0
800	5.9	26	120	3.9	28	120	2.9	43	120	0.0	43	120	0.0	65	180	0.0	61	240	2.7
750	6.1	26	120	4.0	28	120	3.0	29	120	2.0	42	120	0.0	51	200	2.0	66	260	3.0
700	6.4	26	120	4.1	28	120	3.1	34	140	2.0	46	140	0.0	51	200	2.2	66	260	3.3
650	6.6	26	120	4.2	32	140	3.2	34	140	2.2	45	140	0.0	50	200	2.4	70	280	3.6
600	6.9	30	140	4.3	32	140	3.3	34	140	2.3	43	140	0.0	55	220	2.6	70	280	3.9
550	7.1	30	140	4.4	32	140	3.4	34	140	2.4	42	140	0.0	55	220	2.8	75	300	4.2
500	7.4	30	140	4.6	32	140	3.6	38	160	2.6	46	160	0.0	60	240	3.2	79	320	4.8
475	7.6	30	140	4.7	36	160	3.7	38	160	2.7	45	160	0.0	59	240	3.4	79	320	5.1
450	7.7	30	140	4.8	36	160	3.8	38	160	2.8	44	160	0.0	59	240	3.6	79	320	5.4
425	7.8	34	160	4.9	36	160	3.9	38	160	2.9	44	160	0.0	64	260	3.8	83	340	5.7
400	7.9	33	160	5.0	35	160	4.0	37	160	3.0	44	180	2.0	63	260	4.0	83	340	6.0
375	8.0	33	160	5.2	35	160	4.2	37	160	3.2	44	180	2.2	63	260	4.4	82	340	6.6
350 ₩	8.0	3.3	160	5.3	35	160	4.3	42	180	3.3	44	180	2.3	63	260	4.6	82	340	6.9

Lt, Lr, & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

DESIGN F	FACTORS	5 F(	OR A	A DE	SIGN	√ SF	PEED	OF	40	MF	РН (	RUR	AL)	USII	NG E	== 8	3% N	1AX.	
DESIGN VELOCIT	Y=40	WID	TH=18	FT	WID	TH=20	FT	WIDT	H=22	FT	WIDT	ΓH=24	FT	WIDTI	H=48	FT	WIDT	H=72	FT
				IGRI	DS EQ	UIVALE	ENTS (	NUMBE	R OF	LANE	S AT	LANE	WIDTH	1)					
			1@ 9	9'		1 @ 10	)'		1 @ 11	ı		1@ 1:	2'		2 @ 1:	2'		3 @ 12	2'
RADIUS(FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
15000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
10000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
7000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
5000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
4000	2.1	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0	120	120	0.0
3000	2.6	97	120	0.0	97	120	0.0	97	120	0.0	97	120	0.0	97	120	0.0	97	120	0.0
2500	3.1	27	120	3.0	29	120	2.0	82	120	0.0	82	120	0.0	82	120	0.0	95	140	0.0
2250	3.4	27	120	3.1	29	120	2.0	75	120	0.0	75	120	0.0	75	120	0.0	99	160	0.0
2000	3.7	27	120	3.2	29	120	2.2	69	120	0.0	69	120	0.0	69	120	0.0	91	160	0.0
1750	4.1	27	120	3.3	29	120	2.3	62	120	0.0	62	120	0.0	72	140	0.0	93	180	0.0
1500	4.6	27	120	3.4	29	120	2.4	55	120	0.0	55	120	0.0	74	160	0.0	92	200	0.0
1300	5.1	27	120	3.5	28	120	2.5	50	120	0.0	50	120	0.0	66	160	0.0	91	220	0.0
1150	5.5	27	120	3.7	28	120	2.7	45	120	0.0	45	120	0.0	68	180	0.0	90	240	0.0
1000	6.0	27	120	3.8	28	120	2.8	42	120	0.0	49	140	0.0	70	200	0.0	91	270	0.0
900	6.4	31	140	3.9	33	140	2.9	46	140	0.0	46	140	0.0	66	200	0.0	92	280	0.0
800	6.8	30	140	4.1	32	140	3.1	39	160	2.0	50	160	0.0	61	240	2.2	76	300	3.3
750	7.0	30	140	4.2	32	140	3.2	39	160	2.2	48	160	0.0	60	240	2.4	80	340	3.6
700	7.3	34	160	4.3	37	160	3.3	39	160	2.3	47	160	0.0	60	240	2.6	80	340	3.9
650	7.5	34	160	4.4	36	160	3.4	38	160	2.4	45	160	0.0	65	270	2.8	85	340	4.2
600	7.7	34	160	4.5	36	160	3.5	43	180	2.5	44	160	0.0	65	270	3.0	84	340	4.5
550	7.9	34	160	4.6	41	180	3.6	43	180	2.6	48	180	0.0	69	280	3.2	89	360	4.8
500	8.0	34	160	4.8	40	180	3.8	42	180	2.8	48	180	0.0	69	280	3.6	88	360	5.4
475	8.0	34	160	4.9	40	180	3.9	42	180	2.9	48	180	0.0	69	280	3.8	88	360	5.7
₩ 465	8.0	33	160	5.0	40	180	4.0	42	180	3.0	44	180	2.0	68	280	4.0	88	360	6.0

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

MINIMUM ALLOWABLE RADIUS

REV. 1/07 801.34

DESIGN	FACTO	RS I	OR	Α [	DESI	GN	SPE	ED (	OF 4	15 N	лРН	(RU	RAL	) US	ING	E=	8% N	ЛАХ.	
DESIGN VELOCIT	Y=45	WIDTI	H=18 F	Т	WIDT	H=20	FT	WIDT	H=22	FT	WIDT	ΓH=24	FT	WIDTH	1=48 F	Т	WIDTH	=72 F	Т
				IGF	RDS E	QUIV AL	ENTS.	(NUME	BER OF	LANE	ES AT	LANE	WIDTH	1)					
		1@ 9'			1 @ 10'			1 @ 11'			1 @ 12'			2 @ 12'			3	1	
RADIUS (FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0
15000	2.1	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0
10000	2.1	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0
7000	2.1	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0
5000	2.1	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0	140	140	0.0
4000	2.5	118	140	0.0	118	140	0.0	118	140	0.0	118	140	0.0	118	140	0.0	118	140	0.0
3000	3.2	92	140	0.0	92	140	0.0	92	140	0.0	92	140	0.0	92	140	0.0	105	160	0.0
2500	3.7	32	140	3.1	34	140	2.0	80	140	0.0	80	140	0.0	80	140	0.0	103	180	0.0
2250	4.0	32	140	3.2	34	140	2.2	74	140	0.0	74	140	0.0	74	140	0.0	95	180	0.0
2000	4.4	32	140	3.3	33	140	2.3	67	140	0.0	67	140	0.0	77	160	0.0	96	200	0.0
1750	4.9	31	140	3.4	33	140	2.4	60	140	0.0	60	140	0.0	78	180	0.0	95	220	0.0
1500	5.4	31	140	3.5	33	140	2.5	55	140	0.0	55	140	0.0	70	180	0.0	94	240	0.0
1300	6.0	31	140	3.7	33	140	2.7	49	140	0.0	49	140	0.0	70	200	0.0	98	280	0.0
1150	6.4	31	140	3.8	33	140	2.8	46	140	0.0	53	160	0.0	73	220	0.0	99	300	0.0
1000	6.9	35	160	4.0	37	160	3.0	39	160	2.0	49	160	0.0	74	240	0.0	98	320	0.0
900	7.3	35	160	4.1	37	160	3.1	44	180	2.0	52	160	0.0	75	260	0.0	98	340	0.0
800	7.6	34	160	4.3	41	180	3.3	43	180	2.3	50	180	0.0	70	280	2.6	90	360	3.9
750	7.8	39	180	4.3	41	180	3.3	43	180	2.3	49	180	0.0	70	280	2.6	95	380	3.9
700	7.9	38	180	4.4	41	180	3.4	43	180	2.4	48	180	0.0	70	280	2.8	95	380	4.2
650	8.0	38	180	4.6	41	180	3.6	47	200	2.6	48	180	0.0	74	300	3.2	94	380	4.8
₩ 602	8.0	38	180	4.7	40	180	3.7	47	200	2.7	48	180	0.0	74	300	3.4	99	400	5.1

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

DESIGN	FACTOR:	S F(	DR A	A DE	SIGN	N SF	PEEL	) OF	- 5C	) MF	Н (	RUR.	AL)	USIN	GΕ	= 8;	⁄. М <i>А</i>	٩X.	
DESIGN VELOCIT	Y=50	WIDT	H=18 F	Т	WIDT	H=20 F	T	WIDT	H=22	FT	WIDT	H=24	FT	WIDTH=48 FT			WIDTH	Т	
				IGF	RDS E	QUIVAL	ENTS	(NUME	BER OF	LANE	S AT	LANE	WIDTH	1)					
		1@ 9'			1 @ 10'			1 @ 11'			1 @ 12'			2 @ 12'			3	1	
RADIUS (FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0
15000	2.1	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0
10000	2.1	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0
7000	2.1	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0	160	160	0.0
5000	2.4	140	160	0.0	140	160	0.0	140	160	0.0	140	160	0.0	140	160	0.0	140	160	0.0
4000	2.9	116	160	0.0	116	160	0.0	116	160	0.0	116	160	0.0	116	160	0.0	116	160	0.0
3000	3.7	91	160	0.0	91	160	0.0	91	160	0.0	91	160	0.0	91	160	0.0	103	180	0.0
2500	4.3	36	160	3.2	38	160	2.2	79	160	0.0	79	160	0.0	79	160	0.0	108	220	0.0
2250	4.7	36	160	3.3	38	160	2.3	72	160	0.0	72	160	0.0	81	180	0.0	108	240	0.0
2000	5.1	36	160	3.4	38	160	2.4	66	160	0.0	66	160	0.0	83	200	0.0	108	260	0.0
1750	5.6	36	160	3.5	38	160	2.5	60	160	0.0	60	160	0.0	83	220	0.0	105	280	0.0
1500	6.2	35	160	3.7	38	160	2.7	55	160	0.0	55	160	0.0	82	240	0.0	102	300	0.0
1300	6.7	35	160	3.8	37	160	2.8	51	160	0.0	57	180	0.0	82	260	0.0	107	340	0.0
1150	7.2	35	160	3.9	42	180	2.9	47	160	0.0	53	180	0.0	76	260	0.0	105	360	0.0
1000	7.6	39	180	4.1	41	180	3.1	48	200	2.0	56	200	0.0	78	280	0.0	105	380	0.0
900	7.9	39	180	4.3	46	200	3.3	48	200	2.3	54	200	0.0	80	300	0.0	102	380	0.0
800	8.0	38	180	4.4	45	200	3.4	48	200	2.4	53	200	0.0	80	320	2.8	105	420	4.2
₩ 760	8.0	38	180	4.5	45	200	3.5	48	200	2.5	53	200	0.0	80	320	3.0	104	420	4.5

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

DESIGN 1	FACTORS	FOR	ΑΙ	DESI	GN	SPE	ED (	OF 5	55 N	1PH	(RL	JRAL	) US	ING	E=	8%	МАХ.		
DESIGN VELOC	ITY=55	WID.	TH=18	FT	WIE	)TH=20	) FT	WID.	TH=22	FT	WIDTH=24 FT			WID.	TH=48	FT	WIDT	H=72	FT
		IGRDS EQUIVALENTS (NUMBER OF LANES AT LANE WIDTH)																	
			1@ 9'		1 @ 10'			1 @ 11'			1 @ 12'			2 @ 12'			3 @ 12'		
RADIUS (FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0
15000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0
10000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0
7000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0
5000	2.8	135	180	0.0	135	180	0.0	135	180	0.0	135	180	0.0	135	180	0.0	135	180	0.0
4000	3.4	112	180	0.0	112	180	0.0	112	180	0.0	112	180	0.0	112	180	0.0	112	180	0.0
3000	4.4	86	180	0.0	86	180	0.0	86	180	0.0	86	180	0.0	86	180	0.0	115	240	0.0
2500	5.0	40	180	3.3	43	180	2.3	76	180	0.0	76	180	0.0	84	200	0.0	110	260	0.0
2250	5.4	40	180	3.4	43	180	2.4	70	180	0.0	70	180	0.0	86	220	0.0	109	280	0.0
2000	5.9	40	180	3.5	42	180	2.5	65	180	0.0	65	180	0.0	86	240	0.0	114	320	0.0
1750	6.4	40	180	3.6	42	180	2.6	60	180	0.0	60	180	0.0	86	260	0.0	112	340	0.0
1500	7.0	40	180	3.8	42	180	2.8	54	180	0.0	54	180	0.0	84	280	0.0	108	360	0.0
1300	7.5	39	180	4.0	46	200	3.0	49	200	2.0	56	200	0.0	84	300	0.0	112	400	0.0
1150	7.8	43	200	4.1	46	200	3.1	48	200	2.0	54	200	0.0	81	300	0.0	108	400	0.0
1000	8.0	43	200	4.3	46	200	3.3	53	220	2.3	58	220	0.0	84	320	0.0	111	420	0.0
₩ 964	8.0	43	200	4.3	46	200	3.3	53	220	2.3	58	220	0.0	84	320	0.0	111	420	3.9

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

TC-5

DESIGN FACTORS FOR A DESIGN SPEED OF 60 MPH (RURAL) USING E= 8% MAX.

DESIGN VELOCITY=60		WIDT	WIDTH=18 FT			WIDTH=20 FT			WIDTH=22 FT			WIDTH=24 FT			WIDTH=48 FT			WIDTH=72 FT		
				IGF	RDS EC	QUIV ALI	ENTS	(NUMB	ER OF	LANE	S AT	LANE	WIDTH	1)						
			1 @ 9'			1 @ 10'			1 @ 11'			1 @ 12'			2 @ 12'			3 @ 12'		
RADIUS(FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	
20000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	
15000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	
10000	2.1	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	180	180	0.0	
7000	2.4	158	180	0.0	158	180	0.0	158	180	0.0	158	180	0.0	158	180	0.0	158	180	0.0	
5000	3.3	115	180	0.0	115	180	0.0	115	180	0.0	115	180	0.0	115	180	0.0	115	180	0.0	
4000	4.0	95	180	0.0	95	180	0.0	95	180	0.0	95	180	0.0	95	180	0.0	116	220	0.0	
3000	5.0	76	180	0.0	76	180	0.0	76	180	0.0	76	180	0.0	84	200	0.0	118	280	0.0	
2500	5.8	40	180	3.4	43	180	2.4	66	180	0.0	66	180	0.0	87	240	0.0	116	320	0.0	
2250	6.2	40	180	3.5	42	180	2.5	61	180	0.0	61	180	0.0	89	260	0.0	116	340	0.0	
2000	6.7	40	180	3.6	42	180	2.6	57	180	0.0	57	180	0.0	88	280	0.0	113	360	0.0	
1750	7.2	40	180	3.8	47	200	2.8	53	180	0.0	59	200	0.0	88	300	0.0	117	400	0.0	
1500	7.7	44	200	3.9	46	200	2.9	55	200	0.0	60	220	0.0	88	320	0.0	115	420	0.0	
1300	8.0	43	200	4.1	50	220	3.1	58	220	2.0	58	220	0.0	84	320	0.0	116	440	0.0	
<b>⊕</b> 1204	8.0	43	200	4.2	50	220	3.2	58	220	2.2	58	220	0.0	84	320	0.0	116	440	0.0	

NOTE:

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

## DESIGN FACTORS FOR A DESIGN SPEED OF 65 MPH (RURAL) USING E= 8% MAX.

DESIGN VELOCITY=65		WIDT	WIDTH=18 FT			H=20	FT	WIDT	H=22	FT	WIDT	H=24	FT	WIDTH=48 FT			WIDTH	- <sub>T</sub>	
				IGRE	S EQI	JIVALE	NTS (	NUMBE	R OF	LANES	AT L	ANE V	VIDTH)						
			1@ 9'			1 @ 10'			1 @ 11'			1 @ 12'			2 @ 12'			3 @ 12'	
RADIUS(FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0
15000	2.1	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0
10000	2.1	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0	200	200	0.0
7000	2.7	156	200	0.0	156	200	0.0	156	200	0.0	156	200	0.0	156	200	0.0	156	200	0.0
5000	3.7	114	200	0.0	114	200	0.0	114	200	0.0	114	200	0.0	114	200	0.0	125	220	0.0
4000	4.4	96	200	0.0	96	200	0.0	96	200	0.0	96	200	0.0	96	200	0.0	125	260	0.0
3000	5.6	75	200	0.0	75	200	0.0	75	200	0.0	75	200	0.0	98	260	0.0	128	340	0.0
2500	6.5	44	200	3.5	47	200	2.5	65	200	0.0	65	200	0.0	97	300	0.0	130	400	0.0
2250	6.9	44	200	3.6	47	200	2.6	61	200	0.0	67	220	0.0	98	320	0.0	128	420	0.0
2000	7.4	44	200	3.7	51	220	2.7	57	200	0.0	63	220	0.0	97	340	0.0	125	440	0.0
1750	7.8	48	220	3.9	51	220	2.9	60	220	0.0	65	240	0.0	97	360	0.0	124	460	0.0
1500	8.0	48	220	4.1	55	240	3.1	58	240	2.0	63	240	0.0	95	360	0.0	126	480	0.0
<b>⊕</b> 1488	8.0	48	220	4.1	55	240	3.1	58	240	2.0	63	240	0.0	95	360	0.0	126	480	0.0

NOTE:

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

DESIGN	DESIGN FACTORS FOR A DESIGN SPEED OF 70 MPH (RURAL) USING E= 8% MAX.																		
DESIGN VELOCI	DESIGN VELOCITY=70 WIDTH=18 FT			WIDTH=20 FT			WIDTH=22 FT		WIDTH=24 FT		WIDTH=48 FT		WIDTH=72 FT		Т				
				IGF	DS EQUIVALENTS (NUMBER OF LANES AT LANE WIDTH)														
			1@ 9'			1 @ 10'			1 @ 11'			1 @ 12'		2	@ 12	1	3 @ 12'		
RADIUS (FT)	E(%)	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w	Lt	Lr	w
20000	2.1	220	220	0.0	220	220	0.0	220	220	0.0	220	220	0.0	220	220	0.0	220	220	0.0
15000	2.1	220	220	0.0	220	220	0.0	220	220	0.0	220	220	0.0	220	220	0.0	220	220	0.0
10000	2.2	210	220	0.0	210	220	0.0	210	220	0.0	210	220	0.0	210	220	0.0	210	220	0.0
7000	3.0	154	220	0.0	154	220	0.0	154	220	0.0	154	220	0.0	154	220	0.0	154	220	0.0
5000	4.1	113	220	0.0	113	220	0.0	113	220	0.0	113	220	0.0	113	220	0.0	134	260	0.0
4000	5.0	93	220	0.0	93	220	0.0	93	220	0.0	93	220	0.0	101	240	0.0	126	300	0.0
3000	6.3	74	220	0.0	74	220	0.0	74	220	0.0	74	220	0.0	100	300	0.0	127	380	0.0
2500	7.2	49	220	3.6	52	220	2.6	65	220	0.0	65	220	0.0	100	340	0.0	129	440	0.0
2250	7.6	48	220	3.7	51	220	2.7	61	220	0.0	67	240	0.0	100	360	0.0	128	460	0.0
2000	8.0	48	220	3.9	56	240	2.9	58	220	0.0	63	240	0.0	95	360	0.0	126	480	0.0
₩ 1821	8.0	45	220	4.0	55	240	3.0	58	240	2.0	63	240	0.0	95	360	0.0	126	480	0.0

NOTE:

Lt, Lr & w VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY IGRDS.

MINIMUM ALLOWABLE RADIUS

#### STANDARD SYMBOLS

LOCATION  ALIGNMENT ON WHICH THE PROPOSED RIGHT-OF-WAY AND CONSTRUCTION IS BASED.  STANDARD PAVEMENT
NCAPPROXIMATE MAXIMUM SAFE SPEED IN MILES PER HOUR WITH NO SUPERELEVATION. FACTORS APPLY ONLT TO URBAN LOW SPEED CONDITIONS.
Lr LENGTH OF TRANSITION CURVE MEASURED ALONG BASELINE. WHERE NO TRANSITION CURVE IS APPLIED Lr IS LENGTH OF SUPERELEVATION RUNOFF SECTION.  W OR PW WIDTH OF STANDARD PAVEMENT.  ZT DISTANCE FROM TRANSITIONED BASELINE TO EDGES OF TRANSITIONED PAVEMENT WIDENING.  E RATE OF SUPERELEVATION.  F SAFE SIDE FRICTION FACTOR.  S AMOUNT OF SUPERELEVATION TO BE APPLIED TO THE BASELINE GRADE TO OBTAIN THE ELEVATIONS OF THE EDGES OF TRANSITIONED PAVEMENT.  C DIFFERENCE IN ELEVATION BETWEEN BASELINE (CENTER) AND EDGE OF PAVEMENT FOR STANDARD PAVEMENT CROWN.  Lt STANDARD PAVEMENT CROWN TRANSITION OR TANGENT RUNOUT SECTION.  CP CHORD POINT (1/10 INCREMENTS OF TRANSITION CURVE).  NPC NORMAL PAVEMENT CROWN.

ALL DISTANCES (HORIZONTAL AND VERTICAL) ARE MEASURED IN FEET.

SPECIFICATION REFERENCE TRANSITION CURVES FOR RURAL AND URBAN HIGHWAYS AND STREET CONDITIONS

REV. 1/07

### URBAN CONDITION

URBAN CONDITIONS APPLY TO URBAN <u>STREET</u> SYSTEMS AND ANY OTHER ROAD WITH PRESENT OR FUTURE URBAN <u>STREET</u> OPERATING CONDITIONS.

THESE TABLES CONTAIN THE MINIMUM SUPERELEVATION RATES AND TRANSITION LENGTHS FOR STANDARD URBAN PAVEMENT WIDTHS THROUGH A RANGE OF DESIGN VELOCITIES CONSIDERED MOST LIKELY TO BE USED IN URBAN ROAD DESIGN.

DEFINITIONS FOR THE STANDARD SYMBOLS USED THROUGHOUT THESE TABLES ARE FOUND ON SHEET 802.01.

A TABLE FOR "LOW SPEED URBAN" DESIGNS IS ON SHEET 802.24 WITH A RANGE OF STANDARD PAVEMENT WIDTHS (W), SUPERELEVATION RUNOFF (Lr), AND RADII OF CURVE WHEN SUPERELEVATED BY AN AMOUNT EQUAL TO THE NORMAL CROWN AND THE APPROXIMATE MAXIMUM SAFE SPEEDS (DV) AFFORDED THEREBY. VALUES IN THIS TABLE CAN BE USED ON STREETS WITH OPERATING SPEEDS LESS THAN OR EQUAL TO 45 MPH. ALSO SHOWN ARE THE APPROXIMATE MAXIMUM SAFE SPEEDS (NC) WITH NO SUPERELEVATION. VALUES FOR (NC) CAN BE USED ON URBAN ARTERIAL, COLLECTOR, AND LOCAL STREETS.

FOR MINIMUM DESIGN FACTORS FOR VARIOUS DESIGN SPEEDS FOR URBAN CONDITIONS SEE SHEETS 802.25 THRU 802.33

WHEN URBAN CONDITIONS APPLY THERE <u>WILL</u> BE NO BASELINE TRANSITION OR PAVEMENT WIDENING. THE LENGTH OF SUPERELEVATION RUNOFF (Lr) DETERMINES THE LENGTH OF SUPERELEVATION TRANSITION THROUGH WHICH THE OUTER EDGE OF PAVEMENT IS RAISED ABOVE THE BASELINE GRADE TO A MAXIMUM OF E ( $\frac{W}{2}$ ). SEE SHEET 802.07 FOR A GRAPHICAL ILLUSTRATION OF THE APPLICATION OF THIS CORRECTION.

FOR CURVE RADII NOT LISTED IN TABLES REFER TO SHEET 802.22 TO CALCULATE SUPERELEVATION RUNOFF (Lr).

Lr SHOULD BE SHOWN ON THE PLANS FOR ALL CURVES.

E SHOULD BE SHOWN ON THE PLANS FOR ALL CURVES WITH URBAN STREET CONDITIONS.

FOR GRAPHICAL ILLUSTRATION OF DESIGN SUPERELEVATION RATES FOR URBAN CONDITIONS SEE SHEET 802.19.

FOR ADDITIONAL GENERAL INSTRUCTIONS (BOTH URBAN AND RURAL) SEE SHEET 802.04.

EXPLANATION OF TABLES AND INSTRUCTIONS FOR USE URBAN CONDITION

REV. 1/07 802.02

### RURAL CONDITION

RURAL CONDITIONS APPLY TO INTERSTATE, ARTERIAL, PRIMARY AND SECONDARY SYSTEMS OR TO ANY OTHER ROAD WITH RURAL TYPE DESIGN AND OPERATING CONDITIONS.

THESE TABLES CONTAIN THE MINIMUM ALLOWABLE SUPERELEVATION, TRANSITION LENGTHS, AND WIDENING CORRECTIONS FOR STANDARD RURAL PAVEMENT WIDTHS THROUGH A RANGE OF DESIGN VELOCITIES CONSIDERED MOST LIKELY TO BE USED IN RURAL HIGHWAY DESIGN.

DEFINITIONS FOR THE STANDARD SYMBOLS USED THROUGHOUT THESE TABLES ARE FOUND ON SHEET 802.01.

FOR MINIMUM DESIGN FACTORS FOR VARIOUS DESIGN SPEEDS FOR RURAL CONDITIONS SEE SHEETS 802.34 THRU 802.44.

ON CURVES WITH GREATER THAN 2865 FT RADIUS, THERE WILL BE NO SPIRAL TRANSITION OR PAVEMENT WIDENING. PAVEMENT WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE RATE SHOWN IN THE TABLES. SEE SHEET 802.06 FOR A GRAPHICAL ILLUSTRATION OF THE APPLICATION OF THIS CORRECTION.

ON CURVES WITH PAVEMENT WIDTHS OF 24'OR WIDER AND A RADIUS OF 882 FT. OR GREATER, THERE WILL BE NO SPIRAL TRANSITION OR PAVEMENT WIDENING. PAVEMENT WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE RATE SHOWN IN THESE TABLES.

FOR CURVE RADII NOT LISTED IN TABLES, REFER TO SHEET 802.22 TO CALCULATE SUPERELEVATION RUNOFF LENGTH (Lr) AND PAVEMENT WIDENING (w).

Lr AND E SHOULD BE SHOWN ON THE PLANS FOR ALL CURVES ..

FOR GRAPHICAL ILLUSTRATION OF DESIGN SUPERELEVATION RATES FOR RURAL CONDITIONS SEE SHEET 802.20.

FOR ADDITIONAL GENERAL INSTRUCTIONS (BOTH URBAN AND RURAL) SEE SHEET 802.04.

SEE SHEET 802.05 FOR A GRAPHICAL ILLUSTRATION OF SPIRAL TRANSITIONS.

# EXPLANATION OF TABLES AND INSTRUCTIONS FOR USE RURAL CONDITION

### GENERAL CONDITION

ALL ORIGINAL CROSS SECTIONS SHALL BE TAKEN FROM THE BASELINE AT STATIONS, PLUS FIFTIES, AND UNUSUAL BREAKS IN THE GROUND AS ON TANGENT ALIGNMENT.

WHERE A PART OR ALL OF A SUPERELEVATION TRANSITION CURVE FALLS ON A VERTICAL CURVE, ELEVATIONS ON THE VERTICAL CURVE SHOULD BE COMPUTED FOR THE POSITIONS GIVEN ON SHEET 802.16 FOR CROWN TRANSITIONS, SHEET 802.17 FOR URBAN PROJECTS AND SHEET 802.18 FOR RURAL PROJECTS. THESE ELEVATIONS AND PLUSES SHOULD BE SHOWN ON THE PLANS FOR THE CONVENIENCE OF THE SURVEY PARTY IN STAKING OUT THE PROJECT. THROUGHOUT THESE SECTIONS OF THE GRADE, ELEVATIONS AT EVEN STATIONS AND PLUS FIFTIES SHOULD BE OMITTED.

SLOPE STAKES SHOULD BE SET AT THE POSITIONS ON THE TRANSITION GIVEN ON SHEETS 802.16, 802.17 AND 802.18 AND GROUND CROSS SECTIONS TAKEN AT THESE POSITIONS OMITTING THE STATIONS AND PLUS FIFTIES THROUGHOUT THE TRANSITION. IF UNUSUAL BREAKS IN THE GROUND OCCUR, ADDITIONAL SECTIONS SHOULD, OF COURSE, BE TAKEN. ADDITIONAL SECTIONS SHOULD ALSO BE TAKEN WHERE LOCATION IS THROUGH ROCK CUT IN ANTICIPATION OF UNUSUAL BREAKAGE WHICH MAY OCCUR DURING CONSTRUCTION.

AFTER ROUGH GRADING HAS BEEN DONE, FINE GRADING (BLUE TOP) AND FORM STAKES SHOULD BE SET AT THE POSITIONS GIVEN ON SHEET 802.16 FOR CROWN TRANSITIONS, SHEET 802.17 FOR URBAN PROJECTS OR AS GIVEN ON SHEET 802.18 FOR RURAL PROJECTS.

FINAL CROSS SECTIONS SHOULD, OF COURSE, BE TAKEN AT THOSE POSITIONS AT WHICH THE SLOPE STAKE SECTIONS WERE TAKEN. WHERE UNUSUAL BREAKAGE IN ROCK OCCURS, AND THIS WAS NOT ANTICIPATED, ADDITIONAL FINAL SECTIONS SHOULD BE TAKEN AND ORIGINAL GROUND SECTIONS INTERPOLATED.

BASELINE STAKES SHOULD BE SET AT ALL P.C.'S, P.T.'S, T.S.'S, S.T.'S, S.C.'S, AND C.S.'S IN STAKING OUT ALIGNMENT BUT SLOPE STAKES NEED NOT BE SET NOR CROSS SECTIONS TAKEN AT P.C.'S OR P.T.'S EXCEPT WHERE CALLED FOR IN THE ACCOMPANYING TABLES. THE TRANSITION WILL TAKE ITS FORM FROM THE POSITIONS GIVEN ON SHEETS 802.17 AND 802.18.

THE RIGHT OF WAY SHALL, IN ALL CASES, BE REFERENCED FROM THE BASELINE.

THE DESIGNER SHOULD EXERCISE CAUTION IN THE USE OF COMPOUND AND REVERSE CURVES UNLESS TOPOGRAPHICAL OR RIGHT OF WAY RESTRICTIONS MAKE THEIR USE APPROPIATE. THE USE OF BROKEN-BACK CURVES SHOULD BE AVOIDED EXCEPT WHERE VERY UNUSUAL TOPOGRAPHICAL OR RIGHT OF WAY CONDITIONS MAKE OTHER ALTERNATIVES IMPRACTICAL. THE USE OF BROKEN-BACK CURVES MAY REQUIRE A DESIGN EXCEPTION FROM THE STATE LOCATION AND DESIGN ENGINEER. SEE SHEETS 802.11 THRU 802.14 FOR GENERAL INFORMATION ON COMPOUND, REVERSE AND BROKEN-BACK CURVE INFORMATION. REFER TO APPENDIX A OF THE ROAD DESIGN MANUAL FOR SPECIFIC COMPOUND AND REVERSE CURVE DESIGN INFORMATION.

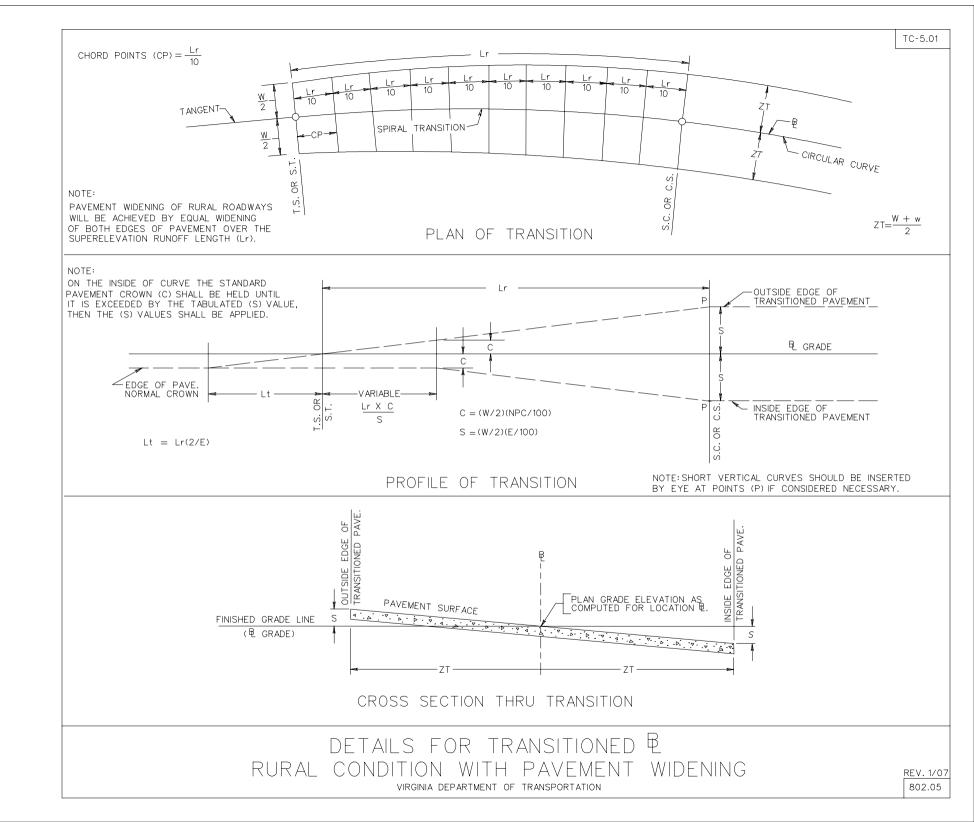
A DESIGN EXCEPTION IS NOT REQUIRED WHEN USING VALUES FROM SHEETS 802.24 THRU 802.44 SINCE THESE TABLES WERE DERIVED WITHIN AASHTO GUIDELINES.

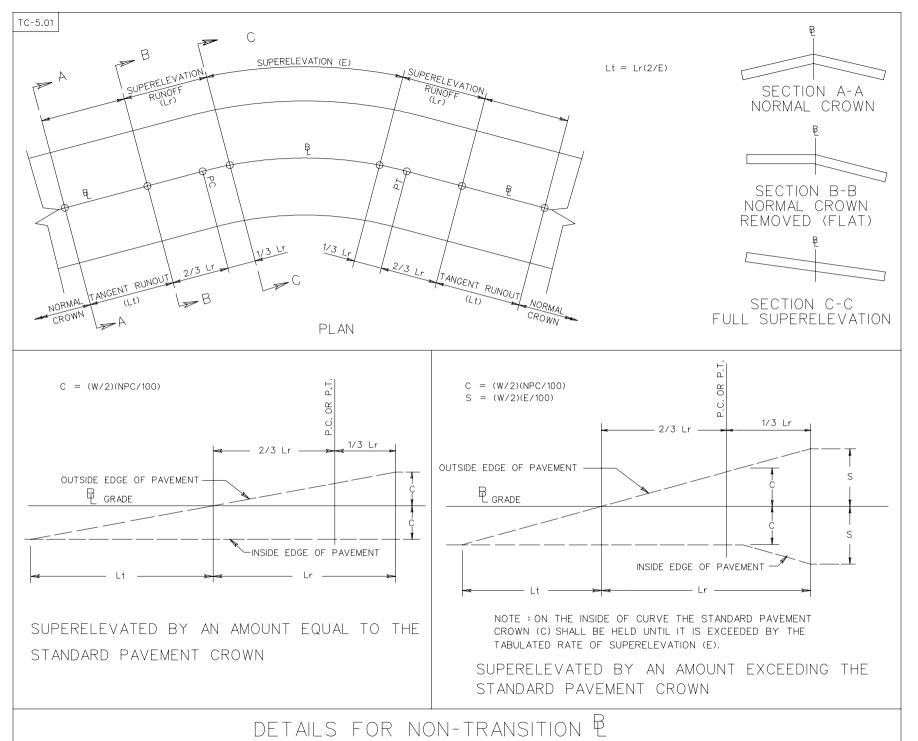
REFER TO CHAPTER 4 OF AASHTO'S <u>A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS</u> FOR INFORMATION ON THE USE OF 18' PAVEMENT WIDTHS (9' LANE WIDTHS).

ALL TANGENT RUNOUT SECTION (Lt) VALUES AND SUPERELEVATION RUNOFF LENGTHS (Lr) LISTED IN THE TABLES HAVE BEEN ROUNDED UP TO THE NEAREST FOOT. ALL Lt VALUES ARE BASED ON A 2% CROWN.

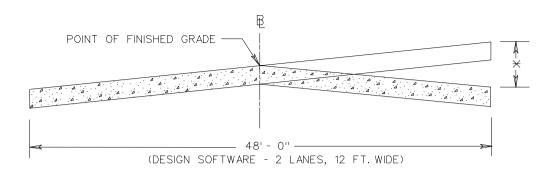
EXPLANATION OF TABLES AND INSTRUCTIONS FOR USE GENERAL CONDITION

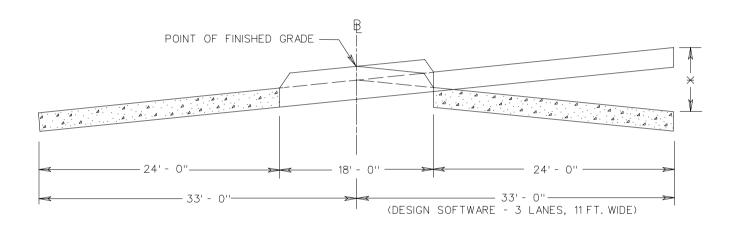
REV. 1/07 802.04





REV. 1/07 URBAN CONDITIONS AND RURAL CONDITIONS WITHOUT PAVEMENT WIDENING
802.06 VIRGINIA DEPARTMENT OF TRANSPORTATION

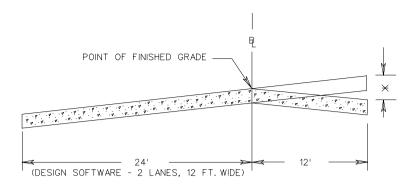




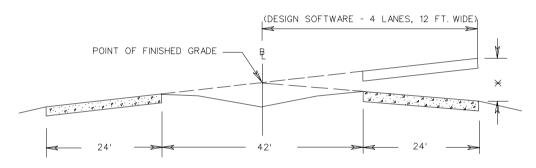
\* THE ELEVATION DIFFERENTIAL BETWEEN NORMAL CROWN AND MAXIMUM SUPERELEVATION, RELATIVE TO THE BASELINE PROFILE.

ADDITIONAL INFORMATION MAY BE OBTAINED FROM A POLICY ON GEOMETRIC DESIGN OF HIGHWAYS AND STREETS (AASHTO) BOOK, CHAPTER III - ELEMENTS OF DESIGN (SUPERELEVATION RUNOFF).

ON STANDARD TC-5.01ULS, TC-5.01U , AND TC-5.01R (WITHOUT PAVEMENT WIDENING) SUPERELEVATED CURVES, POSITION THE SUPERELEVATION RUNOFF SECTION (Lr) TWO THIRDS (2/3) ON THE TANGENT AND ONE THIRD (1/3) INTO THE CURVE. STATIONS AND ELEVATIONS FOR THESE TRANSITIONS WILL NEED TO BE COMPUTED FOR ALL CHORD POINTS AND SHOWN ON THE PROFILES.



THE PAVEMENT WIDTHS SHOWN IN THE STANDARD TC-5.01 TABLES ON SHEET 802.25 THROUGH 802.44 REPRESENT TWICE THE DISTANCE FROM THE CROWNLINE TO THE EDGE OF PAVEMENT ON THE HIGH SIDE.

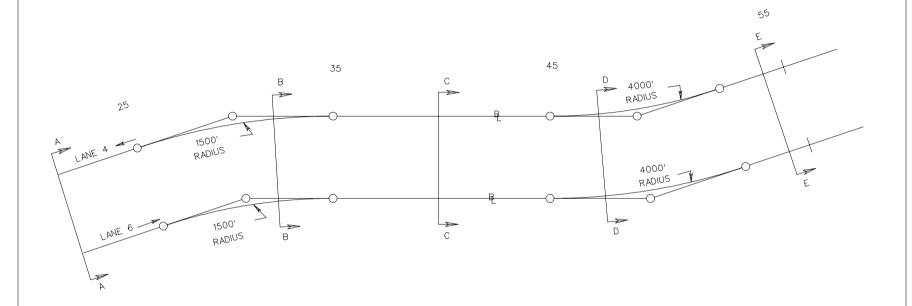


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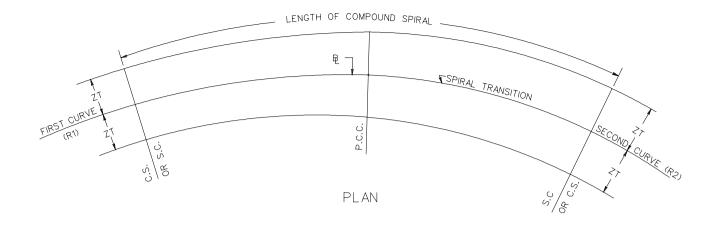
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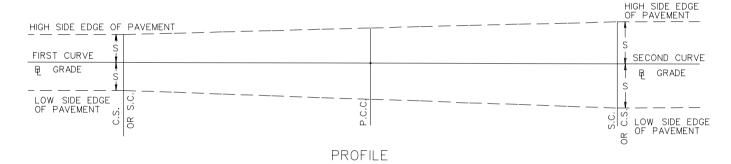
PROJECTS IN WHICH LANES MAY BE ADDED IN THE FUTURE IN THE MEDIAN AREA SHOULD BE DESIGNED WITH THE CONSTRUCTION BASELINE AND POINT OF FINISHED GRADE LOCATED IN THE MIDDLE OF THE MEDIAN. SUPERELEVATION IS TO BE ROTATED FROM THIS BASELINE POINT. THIS WILL PREVENT UNEVEN PAVEMENT PROBLEMS (WHEN ADDITIONAL LANES ARE ADDED IN THE MEDIAN AREA) SUCH AS CROSSOVER GRADES AS WELL AS THE NEED FOR RETAINING WALLS, MEDIAN BARRIERS AND SPECIAL DESIGN DRAINAGE STRUCTURES. ADDITIONAL RIGHT OF WAY OR EASEMENTS, IN MOST SITUATIONS, WILL NOT BE REQUIRED.

TC-5.01



EXAMPLE FOR FOUR LANE ROADWAYS



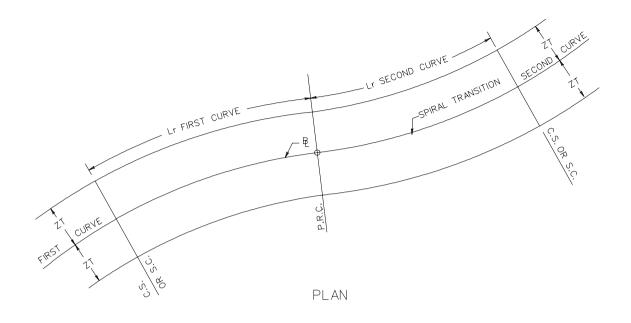


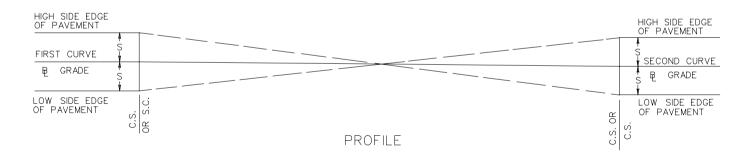
#### NOTE:

- 1. FOR COMPOUND CURVES ON OPEN ROADWAYS, THE RATIO OF FLATTER RADIUS (R1) TO THE SHARPER RADIUS (R2) SHALL NOT EXCEED 1.5:1. WHERE PRACTICAL, A DESIRABLE MAXIMUM RATIO OF 1.75:1 SHOULD BE USED.
- 2. FOR COMPOUND CURVES ON RAMPS AND AT INTERSECTIONS, THE RATIO OF THE FLATTER RADIUS (R1) TO THE SHARPER RADIUS (R2) SHALL NOT EXCEED 2:1.
- 3. COMPUTE STRAIGHT LINE WIDENING AND SUPERELEVATION TRANSITION FROM MAXIMUM OF FIRST CURVE TO MAXIMUM OF SECOND CURVE.
- 4. REFER TO CHAPTER 3 OF THE AASHTO GREEN BOOK FOR ADDITIONAL COMPOUND CURVE DESIGN INFORMATION.

SPECIFICATION REFERENCE METHOD OF APPLYING TC-5.01 ON COMPOUND CURVES RURAL CONDITIONS WITH PAVEMENT WIDENING

TC-5.01





#### NOTE:

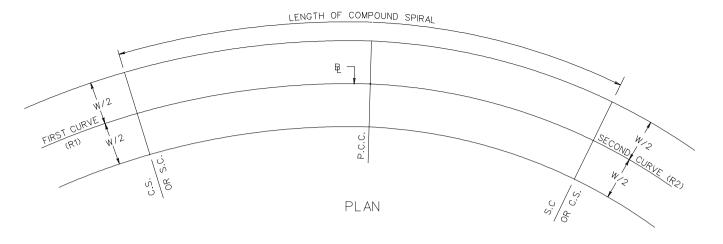
- 1. COMPUTE STRAIGHT LINE WIDENING AND SUPERELEVATION TRANSITION FROM MAXIMUM OF FIRST CURVE TO MAXIMUM OF SECOND CURVE.
- 2. REFER TO CHAPTER 3 OF THE AASHTO'S <u>A POLICY ON THE GEOMETRIC DESIGN OF HIGHWAYS AND STREETS FOR ADDITIONAL REVERSE CURVE DESIGN INFORMATION.</u>

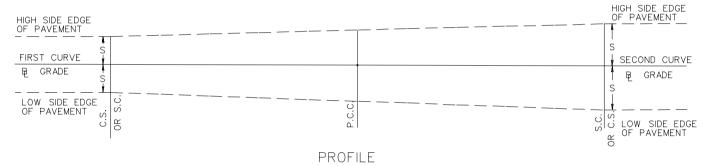
METHOD OF APPLYING TC-5.01 ON REVERSE CURVES RURAL CONDITIONS WITH PAVEMENT WIDENING

SPECIFICATION REFERENCE

REV. 1/07 802.12





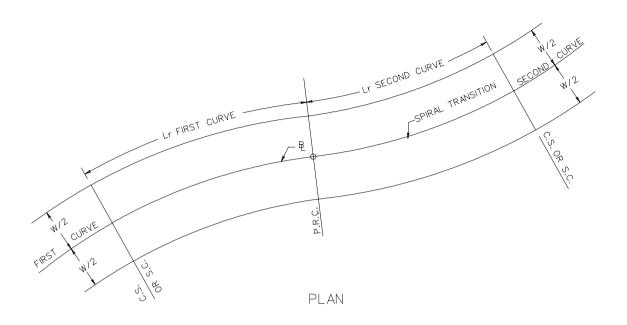


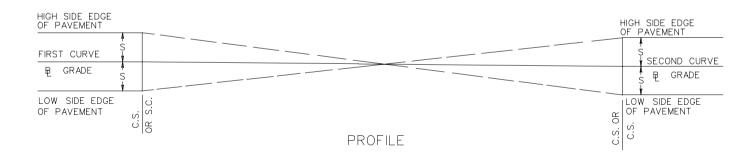
#### NOTE:

- 1. FOR COMPOUND CURVES ON OPEN ROADWAYS, THE RATIO OF FLATTER RADIUS (R1) TO THE SHARPER RADIUS (R2) SHALL NOT EXCEED 1.5:1. WHERE PRACTICAL, A DESIRABLE MAXIMUM RATIO OF 1.75:1 SHOULD BE USED.
- 2. FOR COMPOUND CURVES ON RAMPS AND AT INTERSECTIONS, THE RATIO OF THE FLATTER RADIUS (R1) TO THE SHARPER RADIUS (R2) SHALL NOT EXCEED 2:1.
- 3. COMPUTE SUPERELEVATION TRANSITION FROM MAXIMUM OF FIRST CURVE TO MAXIMUM OF SECOND CURVE. LENGTH OF COMPOUND SPIRAL COMPUTED PER PAGE 802.22.
- 4. REFER TO CHAPTER 3 OF THE AASHTO GREEN BOOK FOR ADDITIONAL COMPOUND CURVE DESIGN INFORMATION.

SPECIFICATION REFERENCE METHOD OF APPLYING TC-5.01 ON COMPOUND CURVES URBAN CONDITIONS & RURAL CONDITIONS WITHOUT PAVEMENT WIDENING







#### NOTE:

- COMPUTE SUPERELEVATION TRANSITION FROM MAXIMUM OF FIRST CURVE TO MAXIMUM OF SECOND CURVE, LENGTH OF SUPERELEVATION RUNOFF (Lr) COMPUTED PER PAGE 802.22.
- 2. REFER TO CHAPTER 3 OF THE AASHTO'S <u>A POLICY ON THE GEOMETRIC DESIGN OF HIGHWAYS AND STREETS</u>
  FOR ADDITIONAL REVERSE CURVE DESIGN INFORMATION.

METHOD OF APPLYING TC-5.01 ON REVERSE CURVES
URBAN CONDITIONS & RURAL CONDITIONS WITHOUT PAVEMENT WIDENING

SPECIFICATION REFERENCE

REV. 1/07

### TRANSITION TABLE

LENGTH OF TANGENT RUNOUT (Lt)	START/END OF SUPERELEVATION RUNOFF	START/END (	DISTANCE IN FEET DF SUPERELEVATION	FROM RUNOFF SECTION (L	NORMAL CROWN	
(20)	(Lr)	1	2	3	4	
220	0	44	88	132	176	220
200	0	40	80	120	140	200
180	0	36	72	108	144	180
160	0	32	64	96	128	160
140	0	28	56	84	112	140
120	0	24	48	72	96	120
100	0	20	40	60	80	100
90	0	18	36	54	72	90
80	0	16	32	48	64	80
60	0	15	30	45		60
40	0	20				40

#### NOTE:

TABLE LISTS POSTIONS ON TRANSITIONS AT WHICH SLOPE STAKES SHOULD BE SET, CONSTRUCTION AND FINAL CROSS-SECTIONS TAKEN, FINE GRADING STAKES (BLUE TOP) SET, AND FORM STAKES SET (CONCRETE PAVEMENT ONLY).

CROWN TRANSITION / TANGENT RUNOUT (Lt) TABLE

# URBAN CONDITIONS RURAL CONDITIONS WITHOUT PAVEMENT WIDENING

FOR USE WITH FLEXIBLE AND CONCRETE PAVEMENT (Lr POSITIONED 2/3 ±ON TANGENT, 1/3 ±ON CURVE)

LENGTH OF SUPERELEVATION RUNOFF	END/ BEGIN TANGENT RUNOUT		DISTANCE IN FEET FROM P.C. OR P.T. ON TANGENT					P.C. OR P.T.		ANCE IN FEET F		FULL SUPER ELEVATION (E)
(Lr)	(Lt)	1	2	3	4	5	6		7	8	9	
480	320	272	224	176	128	80	32	STAKE	16	64	112	160
460	307	261	215	169	123	77	31	STAKE	15	61	107	153
440	293	249	205	161	117	73	29	STAKE	15	59	103	147
420	280	238	196	154	112	70	28	STAKE	14	56	98	140
400	267	227	187	147	107	67	27	STAKE	13	53	93	133
380	253	215	177	139	101	63	25	STAKE	13	51	89	127
360	240	204	168	132	96	60	24	STAKE	12	48	84	120
340	227	193	159	125	91	57	23	STAKE	11	45	79	113
320	213	181	149	117	85	53	21	STAKE	11	43	75	107
300	200	170	140	110	80	50	20	STAKE	10	40	70	100
280	187	159	131	103	75	47	19	STAKE	9	37	65	93
260	173	147 ×	121	95 X	69	43 ×	17	STAKE *	9	35 ×	61	87
240	160	136 ×	112	88 ×	64	40 ×	16	STAKE *	8	32 X	56	80
220	147	125 X	103	81 ×	59	37 X	15	STAKE *	7	29 ×	51	73
200	133	113 ×	93	73 ×	53	33 ×	13	STAKE X	7	27 ×	47	67
180	120	102 ×	84	66 ×	48	30 ×	12	STAKE *	6	24 X	42	60
160	107	91 <sup>Ж</sup>	75	59 X	43	27 X	11	STAKE *	5	21 <sup>Ж</sup>	37	53

#### NOTE :

TABLE GIVING POSITIONS ON CURVES AT WHICH SLOPE STAKES SHOULD BE SET, CONSTRUCTION AND FINAL CROSS-SECTIONS TAKEN, FINE GRADING STAKES (BLUE TOP) SET, AND FORM STAKES SET (CONCRETE PAVEMENT ONLY).

\* DENOTES ADDITIONAL STAKING POSITIONS FOR USE WITH CONCRETE PAVEMENT ONLY.

TABLE I

### RURAL CONDITIONS WITH PAVEMENT WIDENING

FOR USE WITH FLEXIBLE AND CONCRETE PAVEMENT

LENGTH OF SUPERELEVATION RUNOFF (Lr)	T.S. OR S.T.		DISTANCE IN FEET FROM T.S. OR S.T.  ALONG SPIRAL TRANSITION								S.C. OR C.S.
RONOLL (EL)		1	2	3	4	5	6	7	8	9	
480	0	48	96	144	192	240	288	336	384	432	480
460	0	46	92	138	184	230	276	322	368	414	460
440	0	44	88	132	176	220	264	308	352	396	440
420	0	42	84	126	168	210	252	294	336	378	420
400	0	40	80	120	160	200	240	280	320	360	400
380	0	38	76	114	152	190	228	266	304	342	380
360	0	36	72	108	144	180	216	252	288	324	360
340	0	34	68	102	136	170	204	238	272	306	340
320	0	32	64	96	128	160	192	224	256	288	320
300	0	30	60	90	120	150	180	210	240	270	300
280	0	28	56	84	112	140	168	196	224	252	280
260	0	26 X	52	78 X	104	130 ×	156	182 X	208	234 X	260
240	0	24 X	48	72 X	96	120 X	144	168 X	192	216 X	240
220	0	22 Ж	44	66 X	88	110 *	132	154 *	176	198 X	220
200	0	20 Ж	40	60 X	80	100 ×	120	140 X	160	180 X	200
180	0	18 X	36	54 X	72	90 X	108	126 X	144	162 X	180
160	0	16 X	32	48 X	64	80 X	96	112 *	128	144 X	160

#### NOTE :

TABLE GIVING POSITIONS ON TRANSITION CURVES AT WHICH SLOPE STAKES SHOULD BE SET, CONSTRUCTION AND FINAL CROSS-SECTIONS TAKEN, FINE GRADING STAKES (BLUE TOP) SET, AND FORM STAKES SET (CONCRETE PAVEMENT ONLY).

\* DENOTES ADDITIONAL STAKING POSITIONS FOR USE WITH CONCRETE PAVEMENT ONLY.

TABLE 2

#### LEGEND

- C- RATE OF CHANGE OF SIDE FRICTION (f) IN FT./SEC.
- e- SUPERELEVATION RATE.
- f- FRICTION FACTOR.
- Lr- LENGTH OF SUPERELEVATION RUNOFF SECTION.
- Lt- LENGTH OF TANGENT RUNOUT SECTION.
- R- RADIUS OF CURVE.
- DV- DESIGN VELOCITY UTILIZING SUPERELEVATION.
- NC- MAXIMUM VELOCITY WITH NO SUPERELEVATION (NORMAL CROWN).

#### URBAN LOW SPEED DESIGN TABLE

DV/NC (MPH)	MAX. f	С	MIN. Lr (FEET)		
45	0.161	2.75	125		
40	0.178	3.00	115		
35	0.197	3.25	100		
30	0.221	3.50	90		
25	0.252	3.75	80		
20	0.300	4.00	75		

FRICTION FACTORS (f) FOR ODD VELOCITIES NOT LISTED SHOULD BE DERIVED BY INTERPOLATION.

FOR Lr LENGTHS FOR INTERMEDIATE VELOCITIES NOT LISTED IN TABLE USE THE Lr FOR NEAREST VELOCITY IN TABLE.

#### GENERAL DESIGN CONSIDERATIONS

- WHEN "URBAN LOW SPEED" DESIGNS UTILIZE SUPERELEVATION, THEY WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE NORMAL CROWN (TYPICALLY 2.0%) AND THE APPROXIMATE MAXIMUM SAFE SPEED (DV) AFFORDED THEREBY.
- 2. WHEN "URBAN LOW SPEED" DESIGNS UTILIZE NO SUPERELEVATION, THE APPROXIMATE MAXIMUM SAFE SPEED (NC) IS CALCULATED USING A NEGATIVE NORMAL CROWN (TYPICALLY -2.0 %).
- 3. WHEN THE CURVE IS SUPERELEVATED, THE Lr IS APPLIED IN THE SAME MANNER AS IN URBAN CONDITIONS WITH THE TANGENT RUNOUT (Lt) BEING EQUAL TO THE Lr VALUE. THE TANGENT RUNOUT (Lt) IS ALWAYS ACHIEVED OUTSIDE OF THE SUPERELEVATION RUNOFF SECTION(Lr).
- 4. PLEASE NOTE THAT THE RADIUS VALUES LISTED ON PAGE 802.24 HAVE BEEN ROUNDED UP TO THE NEAREST FOOT.

EXAMPLES

DV = 21 mph

e = +2.0 %

 $f = MAX f \pm INTERPOLATED DIFFERENCE BETWEEN LISTED FRICTION FACTORS$ 

f = 0.300-[1/5(0.300-0.252)]=0.2904 (ROUND TO 0.29)

Lr = 47.2 f DV/C

Ir = 47.2(0.29)(21)/4=71.862 FT.

71.862 <90 THEREFORE Lr=90 FT.

Rmin. =  $DV^2/15(e+f)$ 

Rmin. = (21) / 15(0.02 + 0.29) = 94.83870968 FT.

NC = 37 mph

e = -2.0 %

f = MAX f = INTERPOLATED DIFFERENCE BETWEEN LISTED FRICTION FACTORS

f = 0.197-[2/5(0.197-0.178)]=0.1894 (ROUND TO 0.189)

Rmin. = NC  $^{2}/15(-e + f)$ 

Rmin. =  $(37)^2 / 15(-0.02 + 0.189) = 540.0394477$  FT.

	UF	RBAN LOW	SPEED DE	ESIGN TAB	LE	
DV/NC (MPH)	45	40	35	30	25	20
MAX. f	0.150	0.160	0.180	0.200	0.230	0.270

FRICTION FACTORS (f) FOR ODD VELOCITIES NOT LISTED SHOULD BE DERIVED BY INTERPOLATION.

#### LEGEND

- e- SUPERELEVATION RATE.
- f- FRICTION FACTOR.
- Lr- LENGTH OF SUPERELEVATION RUNOFF SECTION.
- Lt- LENGTH OF TANGENT RUNOUT SECTION.
- R- RADIUS OF CURVE.
- DV- DESIGN VELOCITY UTILIZING SUPERELEVATION.
- NC- MAXIMUM VELOCITY WITH NO SUPERELEVATION (NORMAL CROWN).

#### GENERAL DESIGN CONSIDERATIONS

- 1. WHEN "URBAN LOW SPEED" DESIGNS UTILIZE SUPERELEVATION, THEY WILL BE SUPERELEVATED BY AN AMOUNT EQUAL TO THE NORMAL CROWN (TYPICALLY 2.0%) AND THE APPROXIMATE MAXIMUM SAFE SPEED (DV) AFFORDED THEREBY.
- 2. WHEN "URBAN LOW SPEED DESIGN" WITH NO SUPERELEVATION, THE APPROXIMATE MAXIMUM SAFE SPEED (NC) IS CALCULATED USING A NEGATIVE NORMAL CROWN (TYPICALLY -2.0 %).
- 3. WHEN THE CURVE IS SUPERELEVATED, THE Lr IS APPLIED IN THE SAME MANNER AS IN URBAN CONDITIONS WITH THE TANGENT RUNOUT (Lt) BEING EQUAL TO THE Lr VALUE. THE TANGENT RUNOUT (Lt) IS ALWAYS ACHIEVED OUTSIDE OF THE SUPERELEVATION RUNOFF (Lr).
- 4. PLEASE NOTE THAT THE RADIUS VALUES LISTED ON PAGE 802.24A HAVE BEEN ROUNDED UP TO THE NEAREST FOOT.

#### EXAMPLES

 $DV = 21 \, mph$ 

e = +2.0 %

f = MAX f ± INTERPOLATED DIFFERENCE BETWEEN LISTED FRICTION FACTORS f = MAX f ± INTERPOLATED DIFFERENCE BETWEEN LISTED FRICTION FACTORS

f = 0.270 - [1/5(0.270 - 0.230)] = 0.262

Rmin = DV  $^{2}/15(e+f)$ 

Rmin. =  $(21)^2/15(0.02 + 0.262) = 104.2553191$  FT.

NC = 37 mph

e = -2.0 %

f = 0.18-[2/5(0.18-0.16)]=0.172

Rmin. = NC 2/15(-e + f)

Rmin. =  $(37)^2/15(-0.02 + 0.172)=600.4385965$  FT.

#### CURVE WIDENING TABLES

#### SU DESIGN VEHICLE

COMPONENT	SIZE
OVERALL WIDTH	(u) 8.0 ft
WHEELBASE (	L) 20 ft
FRONT OVERHAN	G (A) 4 ft

#### LATERAL CLEARANCE

LANE WIDTH	CLEARANCE (C)
9 ft	1.5 ft
10 ft	2 ft
11 ft	2.5 ft
12 ft	3 ft
16 ft	5 ft

#### ADJUSTMENT FACTORS

NUMBER OF LANES ROTATED n <sub>1</sub>	ADJUSTMENT FACTOR (bw)
1	1.00
1.5	0.8333
2	0.75
2.5	0.70
3	0.6667
3.5	0.6425

#### RELATIVE GRADIENTS

DESIGN SPEED VD MPH	MAXIMUM RELATIVE GRADIENT (rg)	MIN. TRANSITION LENGTH IN FEET RURAL CONDITIONS WITH PAVEMENT WIDENING AND REVERSE CURVES FOR ALL CONDITIONS  (2 SECOND RULE)
20	0.74	59
25	0.70	74
30	0.66	88
35	0.62	103
40	0.58	117
45	0.54	132
50	0.50	147
55	0.47	161
60	0.45	176
65	0.43	191
70	0.40	205

### A - FRONT OVERHANG OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

bw - ADJUSTMENT FACTOR FROM TABLE.

 LATERAL CLEARANCE OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

E - SUPERELEVATION RATE FROM APPROPRIATE TABLE.

F<sub>A</sub> - CALCULATED WIDTH OF OVERHANG FOR DESIGN VEHICLE.

L - WHEELBASE OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

Lr - LENGTH OF SUPERELEVATION RUNOFF SECTION.

#### **DEFINITIONS**

Lt - LENGTH OF TANGENT RUNOUT SECTION

M - MULTIPLE LANE FACTOR.

N - NUMBER OF LANES.

 $\rm n_1$ - NUMBER OF LANES ROTATED (FROM TABLES).

Pw - PAVEMENT WIDTH.

R - RADIUS OF CURVE.

rg - RELATIVE GRADIENT FROM APPROPRIATE TABLE.

U - CALCULATED TRACK WIDTH OF DESIGN VEHICLE.

J - TRACK WIDTH OF DESIGN VEHICLE FROM APPROPRIATE TABLE.

 $V_{\mathsf{D}}$  - DESIGN VELOCITY.

w - CALCULATED WIDENING.

W - PAVEMENT WIDTH

W<sub>C</sub> - CALCULATED TOTAL CURVE WIDTH.

Wn - WIDTH OF LANE.

Z - CALCULATED EXTRA WIDTH ALLOWANCE.

#### GENERAL DESIGN CONSIDERATIONS

- WHERE PAVEMENT WIDENING IS REQUIRED, THE APPROPRIATE WIDENING IS ADDED TO THE LANE WIDTH WHEN CALCULATING THE SUPERELEVATION RUNOFF LENGTH (Lr).
- 2. THE COMPUTED SUPERELEVATION RUNOFF LENGTH (Lr) IS ROUNDED UP TO THE NEAREST FOOT.
- 3. WHEN THE SUPERELEVATION RUNOFF LENGTH (Lr) IS CALCULATED, IT MUST BE COMPARED WITH THE MINIMUM VALUE LISTED IN THE APPROPRIATE COLUMN ON THE RELATIVE GRADIENT TABLE.
- 4. TANGENT RUNOUT (Lt) IS ALWAYS ACHIEVED OUTSIDE OF THE SUPERELEVATION RUNOFF SECTION (Lr).
- 5. NO PAVEMENT WIDENING IS REQUIRED FOR URBAN ROADWAYS.
- NO PAVEMENT WIDENING IS REQUIRED FOR RURAL ROADWAYS WITH A CURVE RADIUS GREATER THAN 2865 FEET.

- 7. NO PAVEMENT WIDENING IS REQUIRED FOR RURAL ROADWAYS WITH 12 FOOT WIDE LANES AND A CURVE RADIUS GREATER THAN 881 FEET.
- 8. PAVEMENT WIDENING IS APPLIED ONLY WHEN CALCULATED WIDENING (w) IS EQUAL TO OR GREATER THAN 2 FEET.
- 9. WHEN CALCULATING WIDENING (W) FOR MULTI-LANE RURAL ROADWAYS, WIDENING IS FIRST CALCULATED USING THE SINGLE LANE WIDTH FOR "W".
- 10. AN ALTERNATE METHOD FOR MULTI-LANE UNDIVIDED PAVEMENTS (48'). THE Lr IS 1.5 TIMES (M-1.5) THE CORRESPONDING LENGTH FOR TWO LANE HIGHWAYS; AND FOR SIX LANE UNDIVIDED PAVEMENTS (72'), THE Lr IS TWO TIMES (M-2) THE CORRESPONDING LENGTH FOR TWO LANE HIGHWAYS.
- 11. CALCULATED WIDENING IS ROUNDED UP TO THE NEAREST 0.1 FOOT.
- 12. CURVES WITH SPIRAL CURVE TRANSITIONS MUST HAVE A MINIMUM SUPERELEVATION RUNOFF LENGTH (Lr) EQUAL TO 2 SECONDS OF TRAVEL TIME AT THE ROADWAY'S DESIGN SPEED AS NOTED IN THE RELATIVE GRADIENT TABLE.

NO WIDENING REQUIRED FORMULAS USED TO CALCULATE SUPERELEVATION RUNOFF (Lr) AND WIDENING (W)

 $Lr = b_w(W_n E/rg)$ 

Lr = M(WE/rg) (ALT. MULTI-LANE)

Lr = m[E(W + w/N)/rg] (ALT. MULTI-LANE)

WIDENING REQUIRED

 $Lr = b_w[E n_1(W_n + w/N)/rg]$ 

 $U = u + R - \sqrt{R^2 - L^2}$ 

 $F_A = \sqrt{R^2 + A(2L + A)} - R$ 

 $Z = (V_D / \sqrt{R})$ 

 $W = W_C - 2W_n$ 

 $W_C = N(U + C) + F_A + Z$ 

FOR SOLVED PROBLEMS USING THIS METHODOLOGY, SEE THE EXAMPLES ON PAGE 802.23

METHODOLOGIES FOR CALCULATING TC-5.01 VALUES

REV. 1/07 802.22

# RURAL EXAMPLE 20 FT PAVEMENT WIDTH (DESIGN SOFTWARE - 1 LANE AT 10 FT)

$$U = U + R - \sqrt{R^2 - L^2}$$

$$U = 8.0 + 1000 - \sqrt{(1000)^2 - (20)^2}$$

$$U = 8.20002$$

$$F_A = \sqrt{R^2 + A(2L + A)} - R$$

$$F_A = \sqrt{(1000)^2 + 4E(2(20) + 4]} - 1000$$

$$F_A = .087996$$

$$Z = (V_D / \sqrt{R})$$
  
 $Z = (50 / \sqrt{1000})$   
 $Z = 1.58$ 

$$W_{C} = N (U + C) + F_{A} + Z$$
  
 $W_{C} = 2(8.20002 + 2) + 0.087996 + 1.58$   
 $W_{C} = 22.0680$ 

$$W = W_C - 2W_n = 22.0680 - 2(10) = 2.1$$

(R<2865 & w>2 THEREFORE WIDENING IS REQUIRED)   
 
$$Lr = E n_1 (W_n + w/2) / rg ] b_w$$
  
 $Lr = [7.6(1)(10 + 2.1/2) / 0.50] 1$   
 $Lr = 7.6 (11.05)/0.50$   
 $Lr = 167.96$ 

### RURAL EXAMPLE

72 FT PAVEMENT WIDTH (DESIGN SOFTWARE - 3 LANES AT 12 FT)

$$U = u + R - \sqrt{R^2 - L^2}$$

$$U = 8.0 + 500 - \sqrt{(500)^2 - (20)^2}$$

$$U = 8.4002$$

$$F_{A} = \sqrt{R^{2} + A (2L + A)} - R$$

$$F_{A} = \sqrt{(500)^{2} + 4[2(20) + 4]} - 500$$

$$F_{A} = .1760$$

$$Z = (V_D / \sqrt{R})$$
  
 $Z = (40 / \sqrt{500})$   
 $Z = 1.7885$ 

$$W_C = 2 (U + C) + F_A + Z$$
  
 $W_C = 2(8.4002 + 3.0) + .1760 + 1.7885$   
 $W_C = 24.7651$ 

$$w = W_C - 2W_p = 24.7651 - 2(12) = 0.7651(0.8)$$

FOR 72' PAVEMENT WIDTH 
$$w = 3(0.8) = 2.4$$

$$Lr = [E \ n_1(W_n + w/3)/ \ rg] b_w$$
  
 $Lr = [8 \ (3) \ (12 +2.4/3)/ \ 0.58] \ 0.6667$ 

$$Lr = (307.2/0.58) 0.6667$$
  
 $Lr = 353.1211$ 

Lr = 353.1034

$$Lr = MEE(W_n + w/N)/rg$$
]  
 $Lr = 2 [8(12 + 4.5/3) / 0.58]$   
 $Lr = 2 (102.4/0.58)$ 

#### URBAN EXAMPLES

24 FT PAVEMENT WIDTH (DESIGN SOFTWARE - 1 LANE AT 12 FT)

$$Lr = (W_n n, E/rg) b_w$$
  
 $Lr = [12(1)(4)/0.58] 1.00$   
 $Lr = (48/.058)$   
 $Lr = 82.7586$ 

66 FT PAVEMENT WIDTH (DESIGN SOFTWARE - 3 LANES AT 11 FT)

$$V_D = 40 \text{ MPH}$$
 R = 600 FT  
 $W_n = 11 \text{ FT}$  rg = 0.58  
F = 4.0 (4% PFR PAGE 802.29)

$$\begin{array}{lll} Lr &= b_{\text{w}} \; (W_n \; n_1 \; E/rg) \\ Lr &= 0.6667 \; [11(3)(4)/ \; 0.58] \\ Lr &= 0.6667 \; (132/0.58) \\ Lr &= 151.7317 \end{array}$$

#### MINIMUM RADII AND SUPERELEVATION RUNOFF SECTION (Lr) LENGTHS FOR 2% SUPERELEVATION

					Lr (FEET)
RADIUS	E	F	DV		PAVEMENT WIDTH (W)
(FEET)	(%)		(MPH)	W <u>&lt;</u> 72 FT.	W > 72 FT
>738	2.0	.163	45	126	
539	2.0	.178	40	113	NOTE:
377	2.0	.197	35	101	FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE LY VALUES DEVELOPED
249	2.0	.221	30	90	BY THE DESIGN SOFTWARE.
154	2.0	.252	25	80	
84	2.0	.300	20	75	

# MINIMUM RADIIFOR DESIGNS UTILIZING NORMAL PAVEMENT CROWN

RADIUS (FEET)	F	NC (MPH)
> 945	.163	45
676	.178	40
462	.197	35
299	.221	30
180	.252	25
96	.300	20

#### MINIMUM RADII AND SUPERELEVATION RUNOFF SECTION LENGTHS (Lr) FOR +2% SUPERELEVATION

				LENG	GTH OF	SUPEREL	EVATION	RUNOF	F (Lr) IN	I FEET
RADIUS	E	f	DV		РА	VEMENT	WIDTH	(W)		
(FEET)	(%)	'	(MPH)	24' (1@12')	36' (1.5@12')	48' (2@12')	60' (3@10')	66' (3@11')	72' (3@12')	W > 72'
> 795	2.0	0.150	45	45	56	67	75	82	90	*
593	2.0	0.160	40	42	52	63	70	77	84	×
408	2.0	0.180	35	39	49	59	65	72	78	×
273	2.0	0.200	30	37	46	55	61	67	74	×
167	2.0	0.230	25	35	43	52	58	64	69	×
92	2.0	0.270	20	33	41	49	55	60	66	*

<sup>\*</sup> FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

MINIMUM RADII FOR DESIGNS

UTILIZING -2% SUPERELEVATION NORMAL PAVEMENT CROWN

RADIUS (FEET)	f	NC (MPH)
> 1039	.150	45
762	.160	40
510	.180	35
333	.200	30
198	.230	25
107	.270	20

## DESIGN FACTORS FOR A DESIGN SPEED OF 20 MPH (URBAN) USING E= 4% MAX.

				TOITE	7 (1 1 7 )	201146	<i>,</i>	1 7 1	/1/ \/\.				
					PAVE	MENT V	VIDTH						
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)		DESIGN	SOFTV	VARE E	QUIVALE	ENTS (N	IUMBER	OF LAN	IES AT	LANE \	WIDTH)	
		1 @	12'	1.5 @	⊉ 12'	2 @	12'	3 @	10'	3 C	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
1400	NC	0	0	0	0	0	0	0	0	0	0	0	0
961	2.0	33	33	41	41	49	49	55	55	60	60	65	65
884	2.1	33	35	41	43	49	52	55	57	60	63	65	69
810	2.2	33	36	41	45	49	54	55	60	60	66	65	72
735	2.3	33	38	41	47	49	56	55	63	60	69	65	75
653	2.4	33	39	41	49	49	59	55	65	60	72	65	78
578	2.5	33	41	41	51	49	61	55	68	60	75	65	82
516	2.6	33	43	41	53	49	64	55	71	60	78	65	85
464	2.7	33	44	41	55	49	66	55	73	60	81	65	88
421	2.8	33	46	41	57	49	69	55	76	60	84	65	91
383	2.9	33	48	41	59	49	71	55	79	60	87	65	95
351	3.0	33	49	41	61	49	73	55	82	60	90	65	98
322	3.1	33	51	41	63	49	76	55	84	60	93	65	101
296	3.2	33	52	41	65	49	78	55	87	60	96	65	104
273	3.3	33	54	41	67	49	81	55	90	60	99	65	108
252	3.4	33	56	41	69	49	83	55	92	60	102	65	111
232	3.5	33	57	41	71	49	86	55	95	60	105	65	114
214	3.6	33	59	41	73	49	88	55	98	60	108	65	117
196	3.7	33	60	41	75	49	90	55	100	60	110	65	120
179	3.8	33	62	41	77	49	93	55	103	60	113	65	124
160	3.9	33	64	41	79	49	95	55	106	60	116	65	127
127	4.0	33	65	41	81	49	98	55	109	60	119	65	130
	-	-	-		•					•	-		-

#### NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

SPECIFICATION REFERENCE TRANSITION CURVES - URBAN 20 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

TC-5.01 DESIGN FACTORS FOR A DESIGN SPEED OF 25 MPH (URBAN) USING F= 4% MAX.													
					PAVE	MENT W	/IDTH						
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)	DE	ESIGN S	SOFTWA	RE EQL	JIVALEN	TS (NU	MBER O	F LANE:	S AT L	ANE WI	DTH)	
		1@	12'	1.5 @	12'	2 @	12'	3 @	10'	3 ❷	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
2500	NC	0	0	0	0	0	0	0	0	0	0	0	0
1407	2.0	35	35	43	43	52	52	58	58	63	63	69	69
1299	2.1	35	36	43	45	52	54	58	60	63	66	69	72
1195	2.2	35	38	43	48	52	57	58	63	63	70	69	76
1094	2.3	35	40	43	50	52	60	58	66	63	73	69	79
990	2.4	35	42	43	52	52	62	58	69	63	76	69	83
883	2.5	35	43	43	54	52	65	58	72	63	79	69	86
793	2.6	35	45	43	56	52	67	58	75	63	82	69	90
718	2.7	35	47	43	58	52	70	58	78	63	85	69	93
654	2.8	35	48	43	60	52	72	58	80	63	88	69	96
598	2.9	35	50	43	63	52	75	58	83	63	92	69	100
548	3.0	35	52	43	65	52	78	58	86	63	95	69	103
505	3.1	35	54	43	67	52	80	58	89	63	98	69	107
466	3.2	35	55	43	69	52	83	58	92	63	101	69	110
430	3.3	35	57	43	71	52	85	58	95	63	104	69	114
397	3.4	35	59	43	73	52	88	58	98	63	107	69	117
367	3.5	35	60	43	75	52	90	58	100	63	110	69	120
339	3.6	35	62	43	78	52	93	58	103	63	114	69	124
311	3.7	35	64	43	80	52	96	58	106	63	117	69	127
284	3.8	35	66	43	82	52	98	58	109	63	120	69	131
255	3.9	35	67	43	84	52	101	58	112	63	123	69	134
204	4.0	35	69	43	86	52	103	58	115	63	126	69	138

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

## DESIGN FACTORS FOR A DESIGN SPEED OF 30 MPH (URBAN) USING E= 4% MAX.

				TOND	/ \  \  / \	001110	<i>/</i> _	17. 1	VI/ \/\•				
					PAVE	MENT V	VIDTH						
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)		ESIGN	SOFTW	ARE EQ	UIVALEN	NTS (NL	JMBER (	OF LANE	ES AT I	_ANE W	IDTH)	
		1@	12'	1.5 @	2 12'	2 @	12'	3 @	10'	3 ₪	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
3000	NC	0	0	0	0	0	0	0	0	0	0	0	0
1940	2.0	37	37	46	46	55	55	61	61	67	67	73	73
1795	2.1	37	39	46	48	55	58	61	64	67	70	73	77
1658	2.2	37	40	46	50	55	60	61	67	67	74	73	80
1525	2.3	37	42	46	53	55	63	61	70	67	77	73	84
1393	2.4	37	44	46	55	55	66	61	73	67	80	73	88
1255	2.5	37	46	46	57	55	69	61	76	67	84	73	91
1134	2.6	37	48	46	60	55	71	61	79	67	87	73	95
1030	2.7	37	50	46	62	55	74	61	82	67	90	73	99
941	2.8	37	51	46	64	55	77	61	85	67	94	73	102
863	2.9	37	53	46	66	55	80	61	88	67	97	73	106
794	3.0	37	55	46	69	55	82	61	91	67	100	73	110
732	3.1	37	57	46	71	55	85	61	94	67	104	73	113
677	3.2	37	59	46	73	55	88	61	97	67	107	73	117
627	3.3	37	60	46	75	55	90	61	100	67	110	73	120
580	3.4	37	62	46	78	55	93	61	104	67	114	73	124
537	3.5	37	64	46	80	55	96	61	107	67	117	73	128
496	3.6	37	66	46	82	55	99	61	110	67	120	73	131
457	3.7	37	68	46	85	55	101	61	113	67	124	73	135
417	3.8	37	70	46	87	55	104	61	116	67	127	73	139
375	3.9	37	71	46	89	55	107	61	119	67	130	73	142
300	4.0	37	73	46	91	55	110	61	122	67	134	73	146
	•	•	•	•	•	•	•	•	•	•	•	•	•

#### NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

TRANSITION CURVES - URBAN 30 MPH DESIGN SPEED

TC-5.01	DESI	GN F	ACT	ORS (URB					EED (	OF 3	5 MF	PH	
				UKB				4/, 1	MAX.				
					PAVEI	MENT W	/IDTH						
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)	D	ESIGN	SOFTWA	ARE EQ	UIVALEN	ITS (NL	IMBER (	OF LANE	S AT L	ANE W	DTH)	
		1 @	12'	1.5 @	12'	2 @	12'	3 @	10'	3 ⊚	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	CR	Lr
4000	NC	0	0	0	0	0	0	0	0	0	0	0	0
2561	2.0	39	39	49	49	59	59	65	65	71	71	78	78
2374	2.1	39	41	49	51	59	61	65	68	71	75	78	82
2199			49	54	59	64	65	71	71	79	78	86	
2031	2.3	39	45	49	56	59	67	65	75	71	82	78	90
1866	2.4	39	47	49	59	59	70	65	78	71	86	78	93
1697	2.5	39	49	49	61	59	73	65	81	71	89	78	97
1538	2.6	39	51	49	63	59	76	65	84	71	93	78	101
1403	2.7	39	53	49	66	59	79	65	88	71	96	78	105
1285	2.8	39	55	49	68	59	82	65	91	71	100	78	109
1182	2.9	39	57	49	71	59	85	65	94	71	103	78	113
1090	3.0	39	59	49	73	59	88	65	97	71	107	78	117
1008	3.1	39	60	49	75	59	90	65	100	71	110	78	120
933	3.2	39	62	49	78	59	93	65	104	71	114	78	124
865	3.3	39	64	49	80	59	96	65	107	71	118	78	128
802	3.4	39	66	49	83	59	99	65	110	71	121	78	132
743	3.5	39	68	49	85	59	102	65	113	71	125	78	136
688	3.6	39	70	49	88	59	105	65	117	71	128	78	140
634	3.7	39	72	49	90	59	108	65	120	71	132	78	144
580	3.8	39	74	49	92	59	111	65	123	71	135	78	148
522	3.9	39	76	49	95	59	114	65	126	71	139	78	151
420	4.0	39	78	49	97	59	117	65	130	71	142	78	155

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

TRANSITION CURVES - URBAN 35 MPH DESIGN SPEED

SPECIFICATION REFERENCE

REV. 1/07 802.28

## DESIGN FACTORS FOR A DESIGN SPEED OF 40 MPH (URBAN) USING E= 4% MAX.

				TOND	AIV) (	731110		+/· I	/////				
					PAVE	MENT V	VIDTH						
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)	DESI	GN SOF	TWARE	EQUIV/	ALENTS	(NUMB	ER OF	LANES	AT LAN	E WIDTH	1)	
		1 @	12'	1.5 @	12'	2 @	12'	3 @	10'	3 ⊚	11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
5000	NC	0	0	0	0	0	0	0	0	0	0	0	0
3273	2.0	42	42	52	52	63	63	69	69	76	76	83	83
3039	2.1	42	44	52	55	63	66	69	73	76	80	83	87
2820	2.2	42	46	52	57	63	69	69	76	76	84	83	92
2612	2.3	42	48	52	60	63	72	69	80	76	88	83	96
2411	2.4	42	50	52	63	63	75	69	83	76	92	83	100
2209	2.5	42	52	52	65	63	78	69	87	76	95	83	104
2010	2.6	42	54	52	68	63	81	69	90	76	99	83	108
1839	2.7	42	56	52	70	63	84	69	94	76	103	83	112
1689	2.8	42	58	52	73	63	87	69	97	76	107	83	116
1557	2.9	42	60	52	75	63	90	69	100	76	110	83	120
1439	3.0	42	63	52	78	63	94	69	104	76	114	83	125
1332	3.1	42	65	52	81	63	97	69	107	76	118	83	129
1236	3.2	42	67	52	83	63	100	69	111	76	122	83	133
1148	3.3	42	69	52	86	63	103	69	114	76	126	83	137
1066	3.4	42	71	52	88	63	106	69	118	76	129	83	141
989	3.5	42	73	52	91	63	109	69	121	76	133	83	145
916	3.6	42	75	52	94	63	112	69	125	76	137	83	149
845	3.7	42	77	52	96	63	115	69	128	76	141	83	154
774	3.8	42	79	52	99	63	118	69	132	76	145	83	158
698	3.9	42	81	52	101	63	122	69	135	76	148	83	162
563	4.0	42	83	52	104	63	125	69	138	76	152	83	166

#### NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

TC-5.01

# DESIGN FACTORS FOR A DESIGN SPEED OF 45 MPH (URBAN) USING E= 4% MAX.

			PAVEMENT WIDTH 24 FT   36 FT   48 FT   60 FT   66 FT   72 FT										
RADIUS	E	24	- T	36 F	Т	48 F	Т	60 F	Т	66 F	Т	72 F	Т
(FEET)	(%)			DESIGN	SOFTWA	ARE EQU	JIVALENT	S (NUMI	BER OF	LANES	AT LAN	E WIDTH	1)
		1@	12'	1.5 @	⊉ 12'	2 @	! 12'	3 @	10'	3 @	11'	3 ⊚	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
6000	NC	0	0	0	0	0	0	0	0	0	0	0	0
4076	2.0	45	45	56	56	67	67	75	75	82	82	89	89
3790	2.1	45	47	56	59	67	70	75	78	82	86	89	94
3523	2.2	45	49	56	62	67	74	75	82	82	90	89	98
3271	2.3	45	52	56	64	67	77	75	86	82	94	89	103
3029	2.4	45	54	56	67	67	80	75	89	82	98	89	107
2790	2.5	45	56	56	70	67	84	75	93	82	102	89	112
2552	2.6	45	58	56	73	67	87	75	97	82	106	89	116
2341	2.7	45	60	56	75	67	90	75	100	82	110	89	120
2155	2.8	45	63	56	78	67	94	75	104	82	115	89	125
1990	2.9	45	65	56	81	67	97	75	108	82	119	89	129
1843	3.0	45	67	56	84	67	100	75	112	82	123	89	134
1710	3.1	45	69	56	87	67	104	75	115	82	127	89	138
1589	3.2	45	72	56	89	67	107	75	119	82	131	89	143
1477	3.3	45	74	56	92	67	110	75	123	82	135	89	147
1374	3.4	45	76	56	95	67	114	75	126	82	139	89	152
1276	3.5	45	78	56	98	67	117	75	130	82	143	89	156
1184	3.6	45	80	56	100	67	120	75	134	82	147	89	160
1093	3.7	45	83	56	103	67	124	75	138	82	151	89	165
1003	3.8	45	85	56	106	67	127	75	141	82	155	89	169
905	3.9	45	87	56	109	67	130	75	145	82	159	89	174
730	4.0	45	89	56	112	67	134	75	149	82	163	89	178

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

TRANSITION CURVES - URBAN 45 MPH DESIGN SPEED

# DESIGN FACTORS FOR A DESIGN SPEED OF 50 MPH (URBAN) USING E= 4 % MAX.

							PAVE	MENT	WIDTH				
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FT	72	FT
(FEET)	(%)	DE	SIGN	SOFTW	ARE EC	UIVALE	NTS (N	UMBER	OF LA	NES A	T LANE	WIDT	<del> </del> )
		1@	12'	1.5 @	⊉ 12'	2 @	12'	3 @	10'	3 @	2 11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
8000	NC	0	0	0	0	0	0	0	0	0	0	0	0
4792	2.0	48	48	60	60	72	72	80	80	88	88	96	96
4629	2.1	48	51	60	63	72	76	80	84	88	93	96	101
4310	2.2	48	53	60	66	72	80	80	88	88	97	96	106
4010	2.3	48	56	60	69	72	83	80	92	88	102	96	111
3723	2.4	48	58	60	72	72	87	80	96	88	106	96	116
3444	2.5	48	60	60	75	72	90	80	100	88	110	96	120
3166	2.6	48	63	60	78	72	94	80	104	88	115	96	125
2911	2.7	48	65	60	81	72	98	80	108	88	119	96	130
2686	2.8	48	68	60	84	72	101	80	112	88	124	96	135
2486	2.9	48	70	60	87	72	105	80	116	88	128	96	140
2306	3.0	48	72	60	90	72	108	80	120	88	132	96	144
2143	3.1	48	75	60	93	72	112	80	124	88	137	96	149
1994	3.2	48	77	60	96	72	116	80	128	88	141	96	154
1857	3.3	48	80	60	99	72	119	80	132	88	146	96	159
1729	3.4	48	82	60	102	72	123	80	136	88	150	96	164
1608	3.5	48	84	60	105	72	126	80	140	88	154	96	168
1493	3.6	48	87	60	108	72	130	80	14 4	88	159	96	173
1381	3.7	48	89	60	111	72	134	80	148	88	163	96	178
1268	3.8	48	92	60	114	72	137	80	152	88	168	96	183
1146	3.9	48	94	60	117	72	141	80	156	88	172	96	188
929	4.0	48	96	60	120	72	144	80	160	88	176	96	192

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt AND Lr VALUES.

TC-5.01

## DESIGN FACTORS FOR A DESIGN SPEED OF 55 MPH (URBAN) USING E= 4% MAX.

			PAVEMENT WIDTH  4 FT											
RADIUS	E	24	FT	36 F	Т	48 F	Т	60 F	Т	66 F	Т	72 F	Т	
(FEET)	(%)		DE	SIGN SO	FTWARE	EQUIVA	LENTS (	NUMBER	OF LA	NES AT	LANE W	/IDTH)		
		1@	12'	1.5 @	⊉ 12'	2 @	! 12'	3 @	10'	3 €	11'	3 @	12'	
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	
10000	NC	0	0	0	0	0	0	0	0	0	0	0	0	
5995	2.0	52	52	64	64	77	77	86	86	94	94	103	103	
5592	2.1	52	54	64	68	77	81	86	90	94	99	103	108	
5218	2.2	52	57	64	71	77	85	86	94	94	103	103	113	
4869	2.3	52	59	64	74	77	89	86	98	94	108	103	118	
4538	2.4	52	62	64	77	77	92	86	103	94	113	103	123	
4220	2.5	52	64	64	80	77	96	86	107	94	118	103	128	
3909	2.6	52	67	64	83	77	100	86	111	94	122	103	133	
3610	2.7	52	69	64	87	77	104	86	115	94	127	103	138	
3343	2.8	52	72	64	90	77	108	86	120	94	132	103	143	
3104	2.9	52	75	64	93	77	112	86	124	94	136	103	149	
2888	3.0	52	77	64	96	77	115	86	128	94	141	103	154	
2691	3.1	52	80	64	99	77	119	86	132	94	146	103	159	
2510	3.2	52	82	64	103	77	123	86	137	94	150	103	164	
2343	3.3	52	85	64	106	77	127	86	141	94	155	103	169	
2186	3.4	52	87	64	109	77	131	86	145	94	160	103	174	
2037	3.5	52	90	64	112	77	135	86	149	94	164	103	179	
1895	3.6	52	92	64	115	77	138	86	154	94	169	103	184	
1756	3.7	52	95	64	119	77	142	86	158	94	174	103	189	
1615	3.8	52	98	64	122	77	146	86	162	94	178	103	195	
1462	3.9	52	100	64	125	77	150	86	166	94	183	103	200	
1190	4.0	52	103	64	128	77	154	86	171	94	188	103	205	

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

## DESIGN FACTORS FOR A DESIGN SPEED OF 60 MPH (URBAN) USING E= 4 % MAX.

					F	PAVEME	NT WID	TH					
RADIUS	E	24	FT	36	FT	48	FT	60	FT	66	FΤ	72	FT
(FEET)	(%)	D	ESIGN	SOFTW	VARE E	QUIVALI	ENTS (N	NUMBEF	R OF L	ANES .	AT LAN	IE WIDT	TH)
		1 @	12'	1.5	⊉ 12'	2 @	! 12'	3 @	10'	3 @	2 11'	3 @	12'
		Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr	Lt	Lr
10000	NC	0	0	0	0	0	0	0	0	0	0	0	0
7131	2.0	54	54	67	67	80	80	89	89	98	98	107	107
6663	2.1	54	56	67	70	80	84	89	94	98	103	107	112
6232	2.2	54	59	67	74	80	88	89	98	98	108	107	118
5829	2.3	54	62	67	77	80	92	89	103	98	113	107	123
5451	2.4	54	64	67	80	80	96	89	107	98	118	107	128
5092	2.5	54	67	67	84	80	100	89	112	98	123	107	134
4746	2.6	54	70	67	87	80	104	89	116	98	128	107	139
4408	2.7	54	72	67	90	80	108	89	120	98	132	107	144
4098	2.8	54	75	67	94	80	112	89	125	98	137	107	150
3818	2.9	54	78	67	97	80	116	89	129	98	142	107	155
3563	3.0	54	80	67	100	80	120	89	134	98	147	107	160
3330	3.1	54	83	67	104	80	124	89	138	98	152	107	166
3114	3.2	54	86	67	107	80	128	89	143	98	157	107	171
2913	3.3	54	88	67	110	80	132	89	147	98	162	107	176
2724	3.4	54	91	67	114	80	136	89	152	98	167	107	182
2544	3.5	54	94	67	117	80	140	89	156	98	172	107	187
2372	3.6	54	96	67	120	80	144	89	160	98	176	107	192
2202	3.7	54	99	67	124	80	148	89	165	98	181	107	198
2030	3.8	54	102	67	127	80	152	89	169	98	186	107	203
1842	3.9	54	104	67	130	80	156	89	174	98	191	107	208
1505	4.0	54	107	67	134	80	160	89	178	98	196	107	214

NOTE:

Lt AND Lr VALUES IN FEET.

FOR PAVEMENT WIDTHS GREATER THAN 72 FEET USE Lr VALUES DEVELOPED BY THE DESIGN SOFTWARE.

LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, AND Lr VALUES.

=20 RADIUS(FT) E(X) 1800 NC 1213 2.0 1148 2.1 1090 2.2 1036 2.3 987 2.4 941 2.5 899 2.6 860 2.7 824 2.8 790 2.9			DESIGN	S		FT   WIDTH=22 FT EQUIVALENTS (NUMBER	WIDTH=ZZ ENTS (NUME	1=22 F   (NUMBER	ᅴ뇽	WIDTH	WIDTH=24 FT ANES AT LANE	WIDTH)	WIDTH=48 (H)	=48 FT	Z	INTERCHANGE	ANGE RAMPS	L L
		1@ 9'					-	@ 11 <sub>-</sub>		1			~	@ 12'	16	FT	18	FT
	) Lt	Lr	w	Lt	Lr	w	Lt	Lr	W	Lt	Lr	M w	Lt L	Lr w	Lt	Lr	Lt	Lr
		0 65	0.0	0 %	0 %	0.0	0 0 2.	0 %	0.0	0 2.3.3	0 0	0.0		0.0 0.0	0 65	0 62	0 4	0 4
	-	59	2.1	28	29	0.0	30		0.0	33	-		49 5	$\vdash$		40	41	43
	$\perp$	59	2.1	28	30	0.0	30		0.0	33	36 (		_	54 0.0	39	42	14	45
	4	200	7.7	87 00	22	0.0	202		0.0	55	+	+	+	+	-	4 4	4 -	4 0
	+	59	2.2	28	34	0.0	30	+	0.0	33	+	0.0	64	+	3.9	2 4 6	+ 4	5 7
		59		28	36	0.0	30	39	0.0	33		-	$\vdash$	$\vdash$		20	41	53
	$\Box$	59	2.3	28	37	0.0	30		0.0	33	H			$\vdash$		52	41	22
	_	59	2.3	28	38	0.0	30	42	0.0	33	_	+	+	69 0.0	_	54	4 ,	57
	$\perp$	29		87 8	04	0.0	30	+	0.0	55	+	+	+	+	+	200	4 4	50
	+	200	4.7	0 00	14	0.0	200	4 7 7	0.0	33	64 6	0.0	+	76 0.0	-	200	4 4	0 2
	+	29		28	4 4	0.0	30		0.0	33		+	+	+		61	14	65
		59	2.5	28	45	0.0	30		0.0	33			8 64			63	41	67
	$\Box$	59	2.6	28	46	0.0	30	51	0.0	33		0.0		-		65	41	69
	_	59	2.6	28	8 4	0.0	30		0.0	33	+	+	+	+	+	67	4 ;	7
	+	29	7.7	87.8	94 0	0.0	30	+	0.0	55	+	+	8 0	+	+	69	4 4	7.5
	+	000	7.7	07 00	200	0.00	200	+	0.0	22	+	0.0	+	+	200	77	- <del>-</del> -	0 7
	+	59	2.0	28	53	0.0	30	7,00	0.0	33	64	+		+	+	75	4	/ 6/
	┝	59	2.9	28	55	0.0	30		0.0	33		-		$\vdash$		77	14	2
		59	2.9	28	56	0.0	30		0.0	33		0.				79	41	83
	Н	09	3.0	30	63	2.0	30	63	0.0	33	Н	0.0		Н		80	41	82
	+	62	3.0	30	64	2.0	30		0.0	333	0/2	0 (	10 64	105 0.0	39	82	4 ,	8/2
	+	50	5.0	30	99	2.0	202		0.0	33	+	+	+	+	+	40	4 4	0 0
	+	20	 	205	200	7.7	30	+	2.0	33	+	+	+	112 0.0	30	8 8	4 4	92
	29 29	89	3.2	31	71	2.2	30 20	02	0.0	33	2/2	0.0	49	115 0.0		8 6	4	96
	$\vdash$	70	3.3	31	73	2.3	30		0.0	33	+	+	+	+	$\sqcup$	92	41	86
	_	71	3.3	31	74	2.3	30		0.0	33	80	_	49	120 0.0	_	94	14	100
	+	73	4.5	31	76	4.7	30		0.0	33	+	+	+	+	+	96	14 6	102
	+	76	) K	2 5	0 0	5.7	200	0 0	0.0	2 6	+	0.0	+	+	7 0	9 5	4	106
	+	7 8	3.6	3 5	8 8	2.6	300	+	0.0	33	+	+	+	129 0.0	+	101	14	108
	_	80		31	83	2.7	30		0.0	33	$\vdash$	0.	$\vdash$	$\vdash$	Ľ	103	41	110
	Н	82	3.8	31	85	2.8	30		0.0	33	Н	0	Н	Н	39	105	41	112
	$\dashv$	83	3.9	32	87	2.9	30	$\dashv$	0.0	33	$\dashv$	4	$\dashv$	+	4	107	41	114
	+	82	0.0	32	83	2.9	30	+	0.0	33	+	+	+	+	4	109	4 1	116
	+	ò	5 4	32	9.3	0.7	5.5	0.0	2.0	22	+	0.0	54	27 2.0	60 60	113	4	120
	+	6	4.2	32	95	3.2	33	+	2.7	33	86	+	+	+	$\perp$	115	14	122
	_	92	4.3	32	97	3.3	34		2.3	33	$\vdash$	╀	╀	╁	-	117	41	124
	Н	94	4.4	32	66	3.4	34	Н	2.4	Н	Н	0.	Н	$\vdash$	39	119	41	126
	+	96		333	101	3.5	34	+	2.5	+	103	0	+	173 3.0	1	120	4	128
	+	100	5.4	5.5	202	2 7	4 6	100	2.0	22	+	0.0	56	181 7.4	60 60	124	4	132
	+	102	8.4	333	107	80.00	34	+	2 0	333	+		+	+	1	126	14	134
	$\vdash$	104		33	109	3.9	34		2.9	33	$\vdash$	0	+	+	<u> </u>	128	41	136
	$\vdash$	106	5.0	33	111	4.0	34	115	3.0	36				$\vdash$		130	41	138
	$\Box$	108	5.1	33	113	4.1	35		3.1	36	122	2.1	$\dashv$	$\vdash$		132	41	140
	$\rightarrow$	110	5.2	33	115	4.2	35	+	3.2	36	4	7	+	202 4.4	4	134	4	142
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	+	119	2.8	34	124	0 4	35	+	2 6	37	+	+	+	+-		141	14	150
	+	12.2	5.9	34	127	6.4	36	+	3.0	37	-	0 0	+	+	+	143	41	152
	$\vdash$	124	6.1	34	129	5.1	36	135	5.7	37	}	·-	+	233 6.2	39	145	41	154
	$\vdash$	127	6.3	35	132	5.3	36	+	4.3		ļ.,	3		9		147	41	156
	$\sqcup$	130	6.5	35	135	5.5	36		4.5	Н	145	5.5	64 2	246 7.0	39	149	41	158
	Н	133	6.8	35	138	5.8	37	Н	4.8	38	149	Н	Н	7		151	41	160
		139	7.6	36	144	6.6	38				155 4			6		153	41	162

20 MPH DESIGN SPEED

CATION ENCE

CORRESPONDING

THE MINIMUM ALLOWABLE RADIUS FOR

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IN FEET. LISTED RADIUS

REV. 1/07 802.34

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EQUIVALENTS		>	0.0	0.0	0.0	0.0		0.0	0.0		0 0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.0	2.1	2.2	2.2	2.4	2.4	2.5	2.6	2.7	8.0	D 0	3.0	3.2	3.2	3.3	3.5	3.6	ν.ν	0.4	1.4	δ. 4. δ. 8.	] 2   
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<u>≻</u> -⊑		) E(;;)		2.1	2.2	2.3	7.1	2.6	2.7	2.0	2.3	3.1	3.2	3.3	3.5	3.6	\S.\	0,0	6.4	4.1	4.3	4.4	4.5	4.7	8.4	5.0	5.1	5.2	5.4	5.5	5.7	5.8	6.0	6.1	6.2	6.4	0.0	6.7	0.0	7.0	7.1		<u></u>	- 1	-		00	
VELOCITY =25	7-	RADIUS(FT	2500	1664	1579	1502	1366	1306	1250	1140	1104	1061	1021	983	948	882	852	795	769	744	969	674	652	612	592	555	537	519	485	468	437	423	396	383	371	347	326	315	295	286	276	258	248	229	219	209	171	NOTE:
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VIRGINIA DEPARTMENT OF TRANSPORTATION

S-5.0			0 4	υ 4 ω	250	52	54	57	59	10	59	89	70	72	2 1	79	25	84	98	2000	93	95	97	99	104	106	5 108	113	112	117	120	124	126	129	131	135	138	140	142	14.7	149	151	153	158	160	162	165	169	171	174	176	2 2
RAMPS	00	Ļ	0 4	45	45	45	45	45	45	ر 4 د م	45	45	45	45	45	45	45	45	45	45 77	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45 7.	45	45	45	45	45
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INTER	16 F	t	0,	0 4 4	43	43	43	43	43	5 4 6	0 4 4 0 10	43	43	43	4 د د د	2 4 4 2 4 2	43	43	43	4 د د د	43	43	43	43	43	43	5 7	0 4 6	43	43	43	2 4 8 7 8	43	43	43	2 4 4	2 4 4	43	43	5 4 4 5 4 3 4	43	43	54 2	0 4 0 4 0 4	43	43	2 4 4 2 4 4	5 4 6 7	43	43	43	454
T.		*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0		0.0	0.0	0.0	0:0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	0.0		0.0		2.4	2.6	7.8	J.0
WIDTH=48 F	@ 12.			+	+				7.1		/ 08	+	$\Box$	88 8	+	96	Н	$\dashv$	+	10/		Н	+	-	126	+	+	137	+	$\vdash$	+	+	153	H	+	161	+	$\vdash$	+	178	180	183	186	+	$\vdash$	+	+	224	228	233	+	$\dashv$
WIDT	2	=	0 4	22	55	55	55	55	55	22	55	55	55	55	55	55	55	55	55	22	55	55	55	55	55	55	+	+	-	Н	+	+	Н	$\vdash$	+	20	+	$\vdash$	+	55		Н	+	+	Н	+	+	+	09	H	+	+
		>	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	_ 
1=24 AT		-	+	+					84 0	+	+	+	57 (	-	+		$\vdash$	+	+	+	75	Н	+	+	84 (	+	+	99	+	H	76	+	102	$\vdash$	+	1108	+	$\vdash$	115	+	$\vdash$	122 (	+	128		+	133	+	+	140	+	-
WIDTH=24	7 -	Lt	0 1	77	37	37	37	37	37	7 2 7	37	37	37	37	2/2	37	37	37	37	2/	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37	37		37	37			37	37	37		37	
	5	>	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.7	2.2	м.	+	D.
WIDTH=22 FT	NOMBE @ 11	۲		75	+			42 (			/ 4 / 6 / 6		H			29 (				605		Н	+	74 (	+		+	282	+	H	68	+	Н	Н	+	99	+	H	+	109	$\vdash$	Н	+	117	Н	$\dashv$	122 (	+	-	Н	145	
		ť	0 7	34	34	34	34	34	34	+	+	+			42 24		34	-	+		+		34	34	34	+	+	34			34	+	34	34	+	34	+	Н	+	34	34	34	+	34		+	34	37	37	Н	38	_
WIDTH=20 FT WIDT	- V	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	2.0	2.0	2.1	1.7			5.3	4. 4	2.5			2.7	2.8	2.8	0.0	2.7	5.2		3.4	5.5
WIDTH=20 FT	10. ©		0 7	+	+				40	+	0 4 4	+	$\vdash$	+	+	54	Н	$\dashv$	+	09	+	Н	+	+	70 (	+	+	2 9	+		+	+	94		+	101	+	$\vdash$	70	111	113 2	Н	+	121		+	127	32	34	136	+	141
WIDTH	- N	Н	0 7	2 5		_			. 121	+	2 15		+		2 2		31	H	12,1	+	31	Н	31	21	31		72 7	2 12			31	+			+	45	+	Н	+	+	35	. 55	-	35	H	+	35 1	+	+	36 1	+	36
		>	0.0	0.0	0.0	0.0	0.5	0.5	2.0	- 1	-   -	2.1	2.2	2.2	7.7	2.3	5.3		2.4	4.7	+ 40	2.5	2.5	9 9	2.6		2.7	7.7	ω.	∞.	2.9	20.0	2.0	3.0	-	- 6	1	H	4	4.0	Ľ		4	1		4	8.9 0.7		4.2	F. 3	+	Ω
9	9 6	Н		+	+				88	+	+	+	+		-	-	Н	-	+	+	+	$\vdash$	$\dashv$	+	88	+	+	+	+	H	+	+	$\vdash$	Н	93	+	+	$\vdash$	+	106		Н	+	+	Н	+	+	+	<u> </u>	131 4	+	$\dashv$
WIDTH=	1	H	+	+	+				89	+			57 8						+		43	Н	-	+	39 8		-	36			+	+		$\vdash$	$\perp$	+	+	Н	-	33			+	+	Н	+	+	+		35	+	$\dashv$
		E(;;)			1				2.6	_	_	1				3.5	Ľ	_	`	n c	0.1-	4.2	4	1	4.6		ω ς	D C	5.1		4	1				1	1			6.5			1	1.		7.2	1	1.	9		4	_
DESIGN	-30=	î	$^{+}$		$\dagger$				T										+															П	$^{\dagger}$							П	1		Н						t	1
<u>9</u>		RADIUS(F	3500	24(	216	205	196	<u>(</u> 2	371	7 / 1	157	151	145	741	155	125	121	117	113		102	66	96	93	877	8	82	77	75	72	200	99	64	62	09	200	54	53	51	4 0 0	46	45	44	4 4 1	40	38	36	348	33	320	30	707

TRANSITION CURVES - RURAL 30 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

SPECIFICATION REFERENCE

1		RADIU\$	=35			_		5					- 1			į		-						
		RADIUS 50: 31:			- 1			1 0 10			100 1		_	0		2	0	-	( א	0				18 FT
N. C.   0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	N. C. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	31,	3(FT) E();	$\perp$	۲	*		۲	*	Lt	L		LT	r	>	Lt	۲	*		-			$\vdash$	Lt
Name	Name	70	OC OC	_	0 5	0.0	_	0 22	0.0	0 22	0 5		0 2	0 2	0.0	0	0	0.0	0 0	0 0	0	_	0	0 9
		28	36 2.3	+	31	0.0	33	34	0.0	36	38		39	6 14	0.0	29	61	0.0	78	82		+	0 00	0 00
2.2         3.0 <td>2.2. 50, 9.3. 0.2. 0.2. 0.2. 0.2. 0.2. 0.2. 0.2. 0</td> <td>28,</td> <td>35 2.2</td> <td><math>\vdash</math></td> <td>32</td> <td>0.0</td> <td>33</td> <td>36</td> <td>0.0</td> <td>36</td> <td>40</td> <td></td> <td>39</td> <td>43</td> <td>0.0</td> <td>59</td> <td>64</td> <td>0.0</td> <td>78</td> <td>98</td> <td>0</td> <td><math>\Box</math></td> <td>0.5</td> <td>φ.</td>	2.2. 50, 9.3. 0.2. 0.2. 0.2. 0.2. 0.2. 0.2. 0.2. 0	28,	35 2.2	$\vdash$	32	0.0	33	36	0.0	36	40		39	43	0.0	59	64	0.0	78	98	0	$\Box$	0.5	φ.
2.6         5.0 <td>2.6</td> <td>28.</td> <td>35 2.2</td> <td><math>\perp</math></td> <td>32</td> <td>0.0</td> <td>33</td> <td>38</td> <td>0.0</td> <td>36</td> <td>40</td> <td></td> <td>39</td> <td>43</td> <td>0.0</td> <td>23</td> <td>64</td> <td>0.0</td> <td>78</td> <td>98</td> <td>0 0</td> <td>_</td> <td>000</td> <td>φ φ</td>	2.6	28.	35 2.2	$\perp$	32	0.0	33	38	0.0	36	40		39	43	0.0	23	64	0.0	78	98	0 0	_	000	φ φ
	2.5 6 8.3 10.3 2.0 3.4 4. 0 10.0 5 6 4.7 10.0 3 6 4.9 10.0 19.0 4.9 10.0 19.0 19.0 19.0 19.0 19.0 19.0 19	25	73 2.4	+	35	0.0	33	39	0.0	36	43		33	47	0.0	59	70	0.0	78	93	0	$\perp$	55	0 00
2.0.         2.0. <th< td=""><td>2.2. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.</td><td>24,</td><td>57 2.5</td><td></td><td>103</td><td>2.0</td><td>33</td><td>41</td><td>0.0</td><td>36</td><td>45</td><td></td><td>39</td><td>49</td><td>0.0</td><td>59</td><td>73</td><td>0.0</td><td>78</td><td>97</td><td>0 (</td><td></td><td>27</td><td>9 8</td></th<>	2.2. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.	24,	57 2.5		103	2.0	33	41	0.0	36	45		39	49	0.0	59	73	0.0	78	97	0 (		27	9 8
2.8         74         0.0         2.0         0.0         99         0.0         0.0         99         0.0         0.0         99         85         0.0         78         1.0         0.0         99         85         0.0         0.0         99         85         0.0         78         1.0         0.0         99         85         0.0         78         1.0         0.0         99         0.0         78         1.0         0.0         99         0.0         78         1.0         0.0         99         0.0         78         1.0         0.0         99         0.0         78         1.0         0.0         99         0.0         78         1.0         0.0         99         0.0         0.0         99         0.0         0.0         99         0.0         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0         99         0.0	2.8         4.0         0.0         3.8         5.0         0.0         9.8         0.0         7.8         1.0         0.0         0.0         9.8         0.0         0.0         7.8         1.0         0.0 <td>23.</td> <td>50 2.6</td> <td>_</td> <td>103</td> <td>2.0</td> <td>33</td> <td>44</td> <td>0.0</td> <td>36</td> <td>4 4 8 4 7</td> <td></td> <td>39</td> <td>53</td> <td>0.0</td> <td>29</td> <td>79</td> <td>0.0</td> <td>78</td> <td>101</td> <td>00</td> <td></td> <td>59 , 61 ,</td> <td>φ φ</td>	23.	50 2.6	_	103	2.0	33	44	0.0	36	4 4 8 4 7		39	53	0.0	29	79	0.0	78	101	00		59 , 61 ,	φ φ
3.0         1.0         3.0 <td>2.0 97 0.0 12. 13. 14. 10. 10. 156 13. 0. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 10. 19. 10. 10. 10. 19. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10</td> <td>216</td> <td>3.5</td> <td><math>\vdash</math></td> <td>103</td> <td>2.0</td> <td>33</td> <td>46</td> <td>0.0</td> <td>36</td> <td>50</td> <td>0.0</td> <td>39</td> <td>55</td> <td>0.0</td> <td>59</td> <td>82</td> <td>0.0</td> <td>78</td> <td>109</td> <td>0</td> <td></td> <td>64</td> <td>_ ω</td>	2.0 97 0.0 12. 13. 14. 10. 10. 156 13. 0. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 19. 19. 10. 0. 10. 10. 19. 10. 10. 10. 19. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10	216	3.5	$\vdash$	103	2.0	33	46	0.0	36	50	0.0	39	55	0.0	59	82	0.0	78	109	0		64	_ ω
3.1         6.7         6.0         6.7         6.0 <td>  Name   Name  </td> <td>20.</td> <td>73 2.5</td> <td><math>\vdash</math></td> <td>103</td> <td>2.1</td> <td>33</td> <td>47</td> <td>0.0</td> <td>36</td> <td>52</td> <td>0.0</td> <td>39</td> <td>57</td> <td>0.0</td> <td>59</td> <td>85</td> <td>0.0</td> <td>78</td> <td>113</td> <td>0.0</td> <td>46</td> <td>, 99</td> <td><u>∞</u> (</td>	Name	20.	73 2.5	$\vdash$	103	2.1	33	47	0.0	36	52	0.0	39	57	0.0	59	85	0.0	78	113	0.0	46	, 99	<u>∞</u> (
3.2         6.6         1.3         2.7         1.5 <td>  1</td> <td>195</td> <td>3.(</td> <td>+</td> <td>103</td> <td>2.1</td> <td>33</td> <td>4 0</td> <td>0.0</td> <td>36</td> <td>54</td> <td>0.0</td> <td>39</td> <td>29</td> <td>0.0</td> <td>20</td> <td>88</td> <td>0.0</td> <td>ω/ α/</td> <td>130</td> <td>0.0</td> <td>46</td> <td>89</td> <td>φ o</td>	1	195	3.(	+	103	2.1	33	4 0	0.0	36	54	0.0	39	29	0.0	20	88	0.0	ω/ α/	130	0.0	46	89	φ o
3.3         6.1         0.1         2.2         3.3         6.4         0.0         3.9         6.0         0.0         78         1.28         0.0         3.9         6.0         0.0         5.9         1.0         7.0         7.0         7.0         3.0         6.0         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         78         1.2         0.0         2.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0         1.2         0.0         3.0 <th< td=""><td>3.3</td><td>187</td><td>7 3.2</td><td>+</td><td>103</td><td>2.1</td><td>33</td><td>52</td><td>0.0</td><td>36</td><td>57</td><td>0.0</td><td>39</td><td>62</td><td>0.0</td><td>59</td><td>93</td><td>0.0</td><td>78</td><td>124</td><td>-</td><td>46 +</td><td>2 12</td><td>0 00</td></th<>	3.3	187	7 3.2	+	103	2.1	33	52	0.0	36	57	0.0	39	62	0.0	59	93	0.0	78	124	-	46 +	2 12	0 00
3.4         61         61         62	3.4         10.3         2.4.         3.9         10.3         2.4.         3.9         10.0         2.9.         10.0         10	17.5	30 3.	$\vdash$	103	2.2	33	54	0.0	36	59		39	64		59	96	0.0	78	128		9 4 6	75 ,	00 0
3.6         3.6 <td>3.6         3.6<td>1/2</td><td>7,5</td><td>_</td><td>10.5</td><td>2.2</td><td>252</td><td>20 22</td><td>0.0</td><td>26</td><td>61</td><td></td><td>50 6</td><td>000</td><td></td><td>20 20</td><td>200</td><td>0.0</td><td>χ α</td><td>1357</td><td></td><td>9 4</td><td>+</td><td>x 0x</td></td>	3.6         3.6 <td>1/2</td> <td>7,5</td> <td>_</td> <td>10.5</td> <td>2.2</td> <td>252</td> <td>20 22</td> <td>0.0</td> <td>26</td> <td>61</td> <td></td> <td>50 6</td> <td>000</td> <td></td> <td>20 20</td> <td>200</td> <td>0.0</td> <td>χ α</td> <td>1357</td> <td></td> <td>9 4</td> <td>+</td> <td>x 0x</td>	1/2	7,5	_	10.5	2.2	252	20 22	0.0	26	61		50 6	000		20 20	200	0.0	χ α	1357		9 4	+	x 0x
3.7         68         10.2         2.3         3.5         60         0.0         39         7.6         0.0         9.0         7.6         9.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         7.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.6         0.0         39         1.0         0.0         39         8         0.0         39         1.0         39         1.0         39         8         0.0         39         1.0         0.0         39         8         0.0         39         1.0         0.0         39         8         0.0         39         1.0         0.0         39 </td <td>3.7         6.8         10.3         2.3         6.8         0.0         3.9         7.2         0.0         9.9         1.0         9.9         1.0         1.0         9.0         1.0         9.0         1.0         9.0<td>9</td><td>3.6</td><td>+</td><td>103</td><td>2.2</td><td>33</td><td>20</td><td>0.0</td><td>36</td><td>50</td><td></td><td>39</td><td>70</td><td></td><td>20</td><td>105</td><td>0.0</td><td>2 × ×</td><td>140</td><td>+</td><td>-</td><td>6/8</td><td>φ φ</td></td>	3.7         6.8         10.3         2.3         6.8         0.0         3.9         7.2         0.0         9.9         1.0         9.9         1.0         1.0         9.0         1.0         9.0         1.0         9.0 <td>9</td> <td>3.6</td> <td>+</td> <td>103</td> <td>2.2</td> <td>33</td> <td>20</td> <td>0.0</td> <td>36</td> <td>50</td> <td></td> <td>39</td> <td>70</td> <td></td> <td>20</td> <td>105</td> <td>0.0</td> <td>2 × ×</td> <td>140</td> <td>+</td> <td>-</td> <td>6/8</td> <td>φ φ</td>	9	3.6	+	103	2.2	33	20	0.0	36	50		39	70		20	105	0.0	2 × ×	140	+	-	6/8	φ φ
3.8         5.6         10.3         2.3         2.5         10.3         2.3         2.5         10.3         2.3         2.5         10.3         2.3         2.5         10.3         2.3         2.5         10.3         2.3         2.5         10.3         2.5         1.0         0.0         3.9         7.6         0.0         3.9         7.6         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         1.0         0.0         3.9         3.0         0.0         3.9         3.0         0.0         3.9         3.0         0.0         3.9         3.0         0.0         3.9         3.0         0.0         3.9         3.0         0.0         3.9         3.0         0.0         3.0         3.0         3.0	3.8         5.5         10.3         2.3         3.5         6.5         0.0         3.9         7.4         0.0         5.9         1.4         0.0         5.9         1.4         0.0         5.9         1.4         0.0         5.9         1.4         0.0         5.9         1.4         0.0         5.9         1.4         0.0         7.8         1.0         0.0         4.4         4.0         5.0         1.0         2.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         9.0         0.0         5.9         1.0         0.0         5.9         1.0         0.0         5.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0 <td>152</td> <td>3.7</td> <td><math>\vdash</math></td> <td>103</td> <td>2.3</td> <td>33</td> <td>09</td> <td>0.0</td> <td>36</td> <td>99</td> <td></td> <td>39</td> <td>72</td> <td>0.0</td> <td>59</td> <td>108</td> <td>0.0</td> <td>78</td> <td>144</td> <td></td> <td><math>\mathbf{H}</math></td> <td>4</td> <td>48</td>	152	3.7	$\vdash$	103	2.3	33	09	0.0	36	99		39	72	0.0	59	108	0.0	78	144		$\mathbf{H}$	4	48
4.0         5.0 <td>4.1 5 103 2.2.3 3.2 6.2 0.0 36 77 0.0 39 87 0.0 59 177 0.0 78 150 0.0 46 4.4 4.4 4.7 103 2.4 33 6.5 0.0 36 77 0.0 39 88 0.0 39 170 0.0 78 159 0.0 46 4.4 4.4 4.4 103 2.4 33 6.5 0.0 36 77 0.0 39 88 0.0 39 170 0.0 78 159 0.0 46 4.4 4.4 4.4 103 2.4 33 6.5 0.0 36 77 0.0 39 88 0.0 39 128 0.0 78 170 0.0 46 4.4 4.4 4.4 103 2.4 33 70 0.0 36 87 70 0.0 39 88 0.0 39 128 0.0 39 128 0.0 46 4.4 4.4 4.4 103 2.4 33 70 0.0 36 82 0.0 39 88 0.0 39 128 0.0 39 128 0.0 46 6.4 120 0.0 38 128 0.0 46 4.4 4.4 4.4 103 2.5 33 75 0.0 36 82 0.0 39 88 0.0 39 128 0.0 39 128 0.0 46 6.4 120 0.0 38 128 0.0 39 129 0.0 39 12</td> <td>24 5</td> <td>3.8</td> <td>-</td> <td>103</td> <td>2.3</td> <td>33</td> <td>62</td> <td>0.0</td> <td>36</td> <td>68</td> <td></td> <td>39</td> <td>74</td> <td></td> <td>59</td> <td>= = =</td> <td>0.0</td> <td>2 78</td> <td>148</td> <td></td> <td>+</td> <td>(O)</td> <td>∞ 0</td>	4.1 5 103 2.2.3 3.2 6.2 0.0 36 77 0.0 39 87 0.0 59 177 0.0 78 150 0.0 46 4.4 4.4 4.7 103 2.4 33 6.5 0.0 36 77 0.0 39 88 0.0 39 170 0.0 78 159 0.0 46 4.4 4.4 4.4 103 2.4 33 6.5 0.0 36 77 0.0 39 88 0.0 39 170 0.0 78 159 0.0 46 4.4 4.4 4.4 103 2.4 33 6.5 0.0 36 77 0.0 39 88 0.0 39 128 0.0 78 170 0.0 46 4.4 4.4 4.4 103 2.4 33 70 0.0 36 87 70 0.0 39 88 0.0 39 128 0.0 39 128 0.0 46 4.4 4.4 4.4 103 2.4 33 70 0.0 36 82 0.0 39 88 0.0 39 128 0.0 39 128 0.0 46 6.4 120 0.0 38 128 0.0 46 4.4 4.4 4.4 103 2.5 33 75 0.0 36 82 0.0 39 88 0.0 39 128 0.0 39 128 0.0 46 6.4 120 0.0 38 128 0.0 39 129 0.0 39 12	24 5	3.8	-	103	2.3	33	62	0.0	36	68		39	74		59	= = =	0.0	2 78	148		+	(O)	∞ 0
4.1         51         10.3         2.4         3.3         67         0.0         36         7.5         0.0         39         8.0         0.0         59         12.0         0.0         7.8         0.0         4.4         4.1         4.1         4.1         4.1         4.1         4.1         4.2         10.3         2.4         3.3         6.0         36         7.0         0.0         59         12.0         0.0         59	4-11 51 103 2-4 33 67 0.0 36 73 0.0 36 73 0.0 39 80 0.0 0.9 91 120 0.0 78 159 0.0 0.4 44.4 44. 103 2-4 33 68 0.0 0.3 67 75 0.0 39 84 0.0 59 122 0.0 78 173 0.0 0.4 44.4 44. 103 2-4 33 70 0.0 36 75 0.0 39 84 0.0 59 122 0.0 78 173 0.0 0.4 45.4 44 17 103 2-5 33 70 0.0 36 75 0.0 39 88 0.0 59 131 0.0 78 173 0.0 0.4 45.4 44 17 103 2-5 33 70 0.0 36 82 0.0 39 81 0.0 59 131 0.0 78 175 0.0 44.4 44.4 44 17 103 2-5 33 70 0.0 36 82 0.0 39 81 0.0 59 131 0.0 78 175 0.0 44.4 44.8 44 17 103 2-5 33 70 0.0 36 82 0.0 39 91 0.0 59 131 0.0 78 175 0.0 44.8 48 130 2.5 33 78 0.0 36 82 0.0 39 91 0.0 59 131 0.0 78 175 0.0 44.8 48 130 2.5 33 78 0.0 36 82 0.0 39 91 0.0 59 144 0.0 78 186 0.0 44.8 48 130 2.5 33 88 0.0 36 82 0.0 39 91 0.0 59 144 0.0 78 149 0.0 44.8 48 130 2.5 33 88 0.0 36 82 0.0 39 91 0.0 59 144 0.0 78 149 0.0 44.8 48 130 2.5 33 88 0.0 36 82 0.0 39 91 0.0 59 144 0.0 78 149 0.0 44 148 148 149 149 149 149 149 149 149 149 149 149	14	33 4.0	+	103	2.3	33	65	0.0	36	71		39	78		29	117	0.0	0 / 8/	155		-	+	0 4 0 0 0 0
4.2         50         0.0         2.4         3.5         0.0         3.9         8.2         0.0         5.9         1.2         0.0         3.9         8.2         0.0         5.9         1.2         0.0         7.0         7.0         4.2         4.0         0.0         3.9         8.6         0.0         5.9         1.2         0.0         7.0         7.0         4.0         4.0         4.0         9.0         0.0         5.0         1.0         7.0         7.0         7.0         9.0         0.0         5.0         1.0         7.0         7.0         7.0         7.0         9.0         0.0         5.0         1.0         7.0         7.0         7.0         9.0         0.0         5.0         1.0         7.0         7.0         9.0         0.0         5.0         1.0         7.0         9.0         0.0         5.0         1.0         9.0         0.0         5.0         1.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         1.0         9.0         0.0         5.0         1.0         9.0         0.0	4.2 50 103 2.4 33 68 0.0 36 77 0.0 39 8 77 0.0 59 82 0.0 59 125 0.0 78 163 0.0 44 4.4 4.4 103 2.4 33 77 0.0 0.0 36 77 0.0 39 84 0.0 0 59 125 0.0 78 163 0.0 0 44 4.4 4.4 103 2.4 33 77 0.0 0.0 36 70 0.0 39 84 0.0 0 59 125 0.0 78 170 0.0 44 4.4 4.4 103 2.4 33 77 0.0 0.0 36 84 0.0 39 84 0.0 59 125 0.0 78 170 0.0 44 4.4 4.4 103 2.2 33 775 0.0 36 84 0.0 39 84 0.0 59 134 0.0 79 181 0.0 0.0 44 4.4 103 2.2 33 775 0.0 36 84 0.0 39 93 0.0 59 140 0.0 79 181 0.0 0.0 44 4.4 103 2.2 33 775 0.0 36 84 0.0 39 93 0.0 59 140 0.0 79 181 0.0 0.0 44 4.5 103 2.2 33 775 0.0 36 84 0.0 39 93 0.0 59 140 0.0 79 181 0.0 0.0 46 5.2 10 0.0 36 84 0.0 39 0.0 0.0 59 140 0.0 79 181 0.0 0.0 46 5.2 10 0.0 36 84 0.0 39 0.0 0.0 59 140 0.0 59 140 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 36 89 0.0 0.0 39 0.0 0.0 59 140 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 36 89 0.0 0.0 39 0.0 0.0 59 140 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 36 89 0.0 0.0 39 0.0 0.0 59 140 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 36 99 0.0 0.0 59 140 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 59 140 0.0 0.0 59 140 0.0 0.0 0.0 46 5.2 10 0.0 0.0 46 5.2 10 0.0 0.0 59 140 0.	13,6	59 4.	$\vdash$	103	2.4	33	67	0.0	36	73		39	80		59	120	0.0	78	159			2	<u>∞</u>
4.7.         4.7. <th< td=""><td>4.5 4 7 102 2.5 33 7 7 10 0.0 36 87 0.0 39 88 0.0 59 134 0.0 78 171 0.0 46 46 47 103 2.5 33 7 7 10 0.0 36 80 0.0 39 88 0.0 59 134 0.0 78 171 0.0 0 46 46 47 103 2.5 33 7 7 10 0.0 36 80 0.0 39 93 0.0 59 134 0.0 78 175 0.0 46 46 47 103 2.5 33 7 7 0.0 36 80 0.0 39 93 0.0 59 134 0.0 78 180 0.0 46 47 48 43 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 200 0.0 46 51 103 2.6 33 80 0.0 36 90 0.0 39 103 0.0 59 143 0.0 36 143 0.0 46 51 103 2.6 33 80 0.0 36 90 0.0 39 103 0.0 59 143 0.0 36 144 0.0 36 1</td><td>13.</td><td>7 4.</td><td>_</td><td>103</td><td>2.4</td><td>33</td><td>68</td><td>0.0</td><td>36</td><td>75</td><td></td><td>39</td><td>82</td><td></td><td>20</td><td>122</td><td>0.0</td><td>78</td><td>163</td><td>+</td><td>+</td><td>95</td><td>φ o</td></th<>	4.5 4 7 102 2.5 33 7 7 10 0.0 36 87 0.0 39 88 0.0 59 134 0.0 78 171 0.0 46 46 47 103 2.5 33 7 7 10 0.0 36 80 0.0 39 88 0.0 59 134 0.0 78 171 0.0 0 46 46 47 103 2.5 33 7 7 10 0.0 36 80 0.0 39 93 0.0 59 134 0.0 78 175 0.0 46 46 47 103 2.5 33 7 7 0.0 36 80 0.0 39 93 0.0 59 134 0.0 78 180 0.0 46 47 48 43 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 180 0.0 46 51 103 2.6 33 80 0.0 36 80 0.0 39 93 0.0 59 143 0.0 78 200 0.0 46 51 103 2.6 33 80 0.0 36 90 0.0 39 103 0.0 59 143 0.0 36 143 0.0 46 51 103 2.6 33 80 0.0 36 90 0.0 39 103 0.0 59 143 0.0 36 144 0.0 36 1	13.	7 4.	_	103	2.4	33	68	0.0	36	75		39	82		20	122	0.0	78	163	+	+	95	φ o
4.5         4.6         10.3         2.5         3.3         7.3         0.0         3.6         8.0         0.0         39         11.0         0.0         19.0         11.0         0.0         19.0         11.0         0.0         19.0         11.0         0.0         19.0         11.0         0.0         19.0         10.0         19.0         11.0         0.0         19.0         10.0         19.0         10.0         19.0         10.0	4.5 46 103 2.5 33 73 0.0 36 80 0.0 39 88 0.0 59 131 0.0 76 176 179 0.0 44 4.8 4.3 103 2.5 33 78 0.0 36 84 0.0 39 91 0.0 59 137 0.0 78 182 0.0 0.4 46 4.8 4.3 103 2.5 33 76 0.0 36 84 0.0 39 91 0.0 59 137 0.0 78 182 0.0 0.4 46 4.8 4.3 103 2.5 33 76 0.0 36 89 0.0 39 91 0.0 59 144 0.0 78 182 0.0 0.4 46 5.0 42 103 2.5 33 80 0.0 36 89 0.0 39 91 0.0 59 144 0.0 78 182 0.0 0.4 46 5.1 4.1 103 2.5 33 84 0.0 36 89 0.0 39 10 0.0 59 144 0.0 78 182 0.0 0.4 46 5.2 40 103 2.2 33 84 0.0 36 89 0.0 39 10 0.0 59 151 0.0 78 120 0.0 46 5.2 40 103 2.2 33 88 0.0 36 89 0.0 39 10 0.0 59 151 0.0 78 120 0.0 46 5.2 40 103 2.2 33 89 0.0 36 91 0.0 39 10 0.0 59 151 0.0 78 120 0.0 46 5.2 34 103 2.2 33 89 0.0 36 91 0.0 39 10 0.0 59 151 0.0 78 120 0.0 46 5.2 34 103 2.2 33 89 0.0 36 10 0.0 36 10 0.0 59 110 0.0 59 151 0.0 46 5.2 35 103 2.2 33 91 0.0 36 100 0.0 39 113 0.0 59 160 0.0 78 121 0.0 46 5.2 35 103 2.2 33 91 0.0 36 100 0.0 39 113 0.0 59 160 0.0 78 121 0.0 46 5.2 35 103 2.2 33 91 0.0 36 100 0.0 39 113 0.0 59 160 0.0 78 121 0.0 46 5.2 35 103 2.2 33 91 0.0 36 100 0.0 39 113 0.0 59 160 0.0 78 121 0.0 46 5.2 35 103 2.2 33 91 0.0 36 100 0.0 39 113 0.0 59 180 0.0 78 121 0.0 46 5.2 35 103 2.2 33 91 0.0 36 10 0.0 39 114 0.0 59 180 0.0 78 121 0.0 46 5.2 35 103 3.2 35 113 2.3 36 113 0.0 39 114 0.0 59 180 0.0 78 121 0.0 46 5.2 35 113 3.3 37 122 2.3 56 113 0.0 39 114 0.0 59 189 0.0 78 121 0.0 46 5.2 35 113 3.3 37 122 2.3 56 113 0.0 39 144 0.0 59 120 0.0 59 120 0.0 46 5.2 35 113 3.3 37 123 2.3 56 113 0.0 39 144 0.0 59 121 0.0 78 121 0.0 46 5.2 35 113 3.3 37 123 2.3 56 130 0.0 39 144 0.0 59 121 0.0 78 121 0.0 44 5.2 35 133 3.3 44 0.0 36 134 0.0 39 144 0.0 59 121 0.0 49 121 0.0 46 5.2 35 133 3.3 37 123 2.3 56 130 0.0 39 144 0.0 59 121 0.0 49 121 0.0 49 5.2 35 133 3.4 37 123 2.3 56 130 0.0 39 144 0.0 59 121 0.0 49 121 0.0 49 5.2 36 133 3.4 37 123 2.3 56 130 0.0 39 144 0.0 59 121 0.0 59 121 0.0 49 5.2 36 133 3.4 37 133 2.5 58 130 0.0 39 144 0.0 59 121 0.0 59 121 0.0 49 5.2 36 133 3.4 37 132 2.3 51 13 0.0 39 144 0.0 59 121 0.0 59 121 0.0 49 5.2 36 138 3.8 37 1	12.	7,4 4.7	+	103	2.4	33	12	0.0	36	79		39	86	0.0	29	128	0.0	0 / 0	171		+	, 001	0 00
4.7. 44, 10.3 2.5 3.3 75 0.0 36 84 0.0 39 91 0.0 59 137 0.0 78 179 0.0 4.4 1.4 10.3 2.5 3.3 75 0.0 36 84 0.0 39 91 0.0 59 137 0.0 78 182 0.0 0.0 4.6 4.1 10.3 2.6 3.3 176 0.0 36 84 0.0 39 95 0.0 59 144 0.0 70 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 78 180 0.0 0.0 5.0 144 0.0 0.0 1.0 140 0.0 1.0 140 0.0 0.0 144 0.0 0.0 1.0 140 0.0 140 0.0	4.7. 44 103 2.5 33 75 0.0 36 84 0.0 39 91 0.0 0.0 59 144 0.0 78 182 0.0 44 4.7 44 103 2.5 33 75 0.0 36 84 0.0 39 91 0.0 0.0 59 144 0.0 78 182 0.0 44 4.7 44 103 2.5 33 76 0.0 36 84 0.0 39 91 0.0 59 143 0.0 78 182 0.0 44 4.5 4.3 103 2.5 33 76 0.0 36 84 0.0 39 91 0.0 59 143 0.0 78 189 0.0 44 4.5 4.3 103 2.5 33 80 0.0 36 89 0.0 39 91 0.0 59 143 0.0 78 189 0.0 44 4.5 5.1 4.3 103 2.5 33 80 0.0 36 89 0.0 39 91 0.0 59 143 0.0 78 189 0.0 44 4.5 5.1 4.3 103 2.5 33 80 0.0 36 89 0.0 39 91 0.0 59 143 0.0 78 189 0.0 44 4.5 5.1 4.1 103 2.5 33 84 0.0 36 89 0.0 39 103 0.0 59 144 0.0 78 120 0.0 44 5.2 4.3 103 2.7 33 88 0.0 36 89 0.0 39 103 0.0 59 144 0.0 78 120 0.0 44 5.2 4.3 103 2.7 33 88 0.0 36 89 0.0 39 103 0.0 59 144 0.0 78 120 0.0 44 5.2 4.3 103 2.8 33 91 0.0 36 90 0.0 39 103 0.0 59 144 0.0 78 120 0.0 44 5.2 4.3 103 2.8 33 91 0.0 36 90 0.0 39 110 0.0 59 144 0.0 78 120 0.0 44 5.2 4.3 103 2.8 33 91 0.0 36 90 0.0 39 111 0.0 59 142 0.0 78 120 0.0 44 5.2 5.2 31 103 2.8 33 91 0.0 36 103 0.0 39 111 0.0 59 142 0.0 78 120 0.0 44 5.2 5.2 31 103 2.9 33 94 0.0 36 103 0.0 39 112 0.0 59 142 0.0 36 103 0.0 59 142 0.0 39 142 0.0 59 142 0.0 39 142 0.0 59 142 0.0 34 5.2 5.2 31 103 2.3 34 1	121	17 4.5	Н	103	2.5	33	73	0.0	36	80	0.0	39	88	0.0	59	131	0.0	78	175			102	<u>∞</u>
4.8         4.3         103         2.6         3.7         8.0         3.6         8.6         0.0         3.9         9.3         0.0         5.9         4.0         0.0         5.0         4.0         4.0         5.0         5.0         4.0         5.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         4.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0         5.0         9.0         0.0 <td>4.8 43 103 2.5 3.5 78 0.0 3.6 87 0.0 39 93 0.0 59 143 0.0 0.0 78 186 0.0 46 45 173 0.3 2.6 3.3 80 0.0 3.6 87 0.0 39 95 0.0 59 143 0.0 0.0 78 180 0.0 46 45 1.0 3 0.2 2.6 3.3 80 0.0 3.6 87 0.0 39 95 0.0 59 143 0.0 78 180 0.0 46 55.4 40 103 2.2 3.3 84 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 40 103 2.2 3.3 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 100 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 113 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 113 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.9 33 94 0.0 3.6 103 0.0 39 113 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.9 33 94 0.0 3.6 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.</td> <td>116</td> <td>3. F</td> <td>+</td> <td>103</td> <td>2.5</td> <td>255</td> <td>75</td> <td>0.0</td> <td>36</td> <td>82</td> <td>0.0</td> <td>259</td> <td>8 2</td> <td>0.00</td> <td>700</td> <td>13.4</td> <td>0.0</td> <td>χ α</td> <td>17.9</td> <td>-</td> <td>+</td> <td>104</td> <td>φ σ</td>	4.8 43 103 2.5 3.5 78 0.0 3.6 87 0.0 39 93 0.0 59 143 0.0 0.0 78 186 0.0 46 45 173 0.3 2.6 3.3 80 0.0 3.6 87 0.0 39 95 0.0 59 143 0.0 0.0 78 180 0.0 46 45 1.0 3 0.2 2.6 3.3 80 0.0 3.6 87 0.0 39 95 0.0 59 143 0.0 78 180 0.0 46 55.4 40 103 2.2 3.3 84 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 40 103 2.2 3.3 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 89 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 100 0.0 59 143 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 100 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 113 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.7 33 88 0.0 3.6 96 0.0 39 113 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.9 33 94 0.0 3.6 103 0.0 39 113 0.0 59 140 0.0 78 180 0.0 46 55.4 39 103 2.9 33 94 0.0 3.6 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 103 0.0 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.0 59 140 0.0 78 129 0.0 46 55.4 39 113 0.0 59 140 0.	116	3. F	+	103	2.5	255	75	0.0	36	82	0.0	259	8 2	0.00	700	13.4	0.0	χ α	17.9	-	+	104	φ σ
5.0         4.3         1.0         2.6         3.3         8.0         0.0         3.6         8.0         0.0         3.6         8.0         0.0         3.6         8.0         0.0         3.6         8.0         0.0         3.6         8.0         0.0         3.6         8.0         0.0         3.6         8.0         0.0         3.6         9.0         0.0         3.6         1.0         0.0 <td>5.0         4.9         4.2         4.3         4.3         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         0.0         36         9.9         0.0         39         1.0         5.9         14.9         0.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.0         4.0         4.0         4.0         1.0         4.0</td> <td>10,</td> <td>3.4 4.8</td> <td>+</td> <td>103</td> <td>2.6</td> <td>33</td> <td>78</td> <td></td> <td>36</td> <td>86</td> <td>0.0</td> <td>39</td> <td>93</td> <td>0.0</td> <td>29</td> <td>140</td> <td>0.0</td> <td>78</td> <td>186</td> <td></td> <td>+ +</td> <td>109</td> <td>0 00</td>	5.0         4.9         4.2         4.3         4.3         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         4.9         0.0         36         9.9         0.0         39         1.0         5.9         14.9         0.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.9         1.0         4.0         4.0         4.0         4.0         1.0         4.0	10,	3.4 4.8	+	103	2.6	33	78		36	86	0.0	39	93	0.0	29	140	0.0	78	186		+ +	109	0 00
5.7         4.7         5.0         5.2         5.3         8.3         5.0         5.0         5.0         5.0         5.0         1.4         0.0         5.0         1.4         0.0         5.0         1.4         0.0         5.0         1.0         5.0         1.0         0.0         5.0         1.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         5.0         1.0         0.0         3.0         1.0         0.0         3.0         1.0         0.0         3.0         1.0         0.0         3.0         1.0         0.0         3.0         1.0         0.0         3.0         1.0         0.0         3.0         1.0 <td>5.7.         4.7.         6.7.         5.7.         <th< td=""><td>10(</td><td>55</td><td>_</td><td>103</td><td>2.6</td><td>33</td><td>8 2</td><td>0.0</td><td>36</td><td>87</td><td>0.0</td><td>39</td><td>95</td><td>0.0</td><td>59</td><td>143</td><td>0.0</td><td>8 2</td><td>190</td><td>0.0</td><td>46</td><td>11 7</td><td>φ α</td></th<></td>	5.7.         4.7.         6.7.         5.7. <th< td=""><td>10(</td><td>55</td><td>_</td><td>103</td><td>2.6</td><td>33</td><td>8 2</td><td>0.0</td><td>36</td><td>87</td><td>0.0</td><td>39</td><td>95</td><td>0.0</td><td>59</td><td>143</td><td>0.0</td><td>8 2</td><td>190</td><td>0.0</td><td>46</td><td>11 7</td><td>φ α</td></th<>	10(	55	_	103	2.6	33	8 2	0.0	36	87	0.0	39	95	0.0	59	143	0.0	8 2	190	0.0	46	11 7	φ α
5.2         40         103         2.7         35         84         0.0         36         93         0.0         39         101         0.0         59         151         0.0         78         200         0.0           5.4         39         103         2.7         33         88         0.0         36         96         0.0         39         103         0.0         59         157         0.0         78         20         0.0         50         160         0.0         78         20         0.0         90         0.0         59         160         0.0         78         20         0.0         90         0.0         59         160         0.0         78         100         0.0         59         160         0.0         39         100         0.0         59         160         0.0         78         100         0.0         39         111         0.0         59         160         0.0         39         111         0.0         59         160         0.0         78         100         0.0         39         111         0.0         59         160         0.0         78         20         0.0         50         100	5.2         4.0         10.3         2.7         3.5         84         0.0         36         93         0.0         39         10.0         59         15.0         78         20.0         34         6.0         36         93         0.0         39         103         0.0         78         11.0         78         20.0         34         46         50.0         36         96         0.0         39         10.0         59         150         0.0         78         21.0         0.0         46         56         50         46         50.0         46         56         50         78         21.0         0.0         46         56         50         78         21.0         0.0         46         50         46         0.0         46         50         60         78         10.0         50         160         0.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         40         60         40         60         80         90         90         90         90         90         90         90         90         90         90         90 <td>10(</td> <td>74 5.</td> <td>+</td> <td>103</td> <td>2.6</td> <td>33</td> <td>83</td> <td>0:0</td> <td>36</td> <td>91</td> <td>0.0</td> <td>39</td> <td>66</td> <td>0.0</td> <td>29</td> <td>149</td> <td>0.0</td> <td>78</td> <td>198</td> <td>0.0</td> <td>46</td> <td>15</td> <td>0 00</td>	10(	74 5.	+	103	2.6	33	83	0:0	36	91	0.0	39	66	0.0	29	149	0.0	78	198	0.0	46	15	0 00
5.4         39         10.2         10	5.4.         39         10.3         2.0         39         10.4         7.0         7.8         2.0         0.0         44           5.4.         39         10.3         2.0         39         10.3         0.0         39         10.3         0.0         50         10.3         0.0         36         0.0         39         10.0         30         10.3         0.0         39         10.0         30         10.3         0.0	97	5 5.2		103	2.7	33	84	0.0	36	93	0.0	39	101	0.0	59	151	0.0	78	202	0.0	46 1	18	· · ·
5.5         38         10.0         36         98         10.0         39         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         59         160         10.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         217         0.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0         78         10.0 <th< td=""><td>5.5         38         103         2.8         33         89         0.0         36         107         0.0         59         160         0.0         78         213         0.0         46           5.6         37         103         2.8         33         89         0.0         36         100         0.0         59         165         0.0         78         217         0.0         46           5.8         37         103         2.9         3.0         0.0         39         113         0.0         59         166         0.0         78         217         0.0         46           5.9         103         2.9         3.0         0.0         39         113         0.0         59         166         0.0         78         217         0.0         46           6.0         35         103         0.0         39         117         0.0         59         166         0.0         78         179         0.0         46           6.0         35         103         0.0         39         117         0.0         59         166         0.0         78         27         0.0         46</td><td>94</td><td>0 8 0 5</td><td>_</td><td>103</td><td>2.7</td><td>3,3</td><td>98</td><td>0.00</td><td>36</td><td>95</td><td>0.0</td><td>39</td><td>10.5</td><td>0.0</td><td>200</td><td>154</td><td>0.0</td><td>20 00</td><td>206</td><td>0.0</td><td>466</td><td>207.</td><td>φ oc</td></th<>	5.5         38         103         2.8         33         89         0.0         36         107         0.0         59         160         0.0         78         213         0.0         46           5.6         37         103         2.8         33         89         0.0         36         100         0.0         59         165         0.0         78         217         0.0         46           5.8         37         103         2.9         3.0         0.0         39         113         0.0         59         166         0.0         78         217         0.0         46           5.9         103         2.9         3.0         0.0         39         113         0.0         59         166         0.0         78         217         0.0         46           6.0         35         103         0.0         39         117         0.0         59         166         0.0         78         179         0.0         46           6.0         35         103         0.0         39         117         0.0         59         166         0.0         78         27         0.0         46	94	0 8 0 5	_	103	2.7	3,3	98	0.00	36	95	0.0	39	10.5	0.0	200	154	0.0	20 00	206	0.0	466	207.	φ oc
5.6         3.7         10.3         2.8         3.3         91         0.0         36         100         39         100         39         100         39         100         39         100         39         100         39         100         39         100         39         100         39         100         39         111         0.0         59         160         0.0         78         27         100         30         100         39         111         0.0         59         160         0.0         39         112         0.0         59         160         0.0         39         112         0.0         59         160         0.0         39         112         0.0         59         160         0.0         39         112         0.0         59         160         0.0         39         112         0.0         39         112         0.0         39         112         0.0         36         100         0.0         39         117         0.0         59         172         0.0         78         180         0.0         30         0.0         39         112         0.0         39         112         0.0         39         1	5.6         3.7         10.3         2.8         3.3         91         0.0         36         10.0         59         16.5         0.0         78         2.7         0.0         46           5.7         3.0         1.0         3.6         10.0         3.9         11.0         0.0         59         165         0.0         78         2.2         10.0         46           5.9         3.0         3.2         3.3         9.4         0.0         3.6         10.2         0.0         3.9         11.0         0.0         59         166         0.0         78         2.2         0.0         46           6.0         3.5         10.3         3.0         3.6         10.0         3.9         11.0         0.0         59         17.2         0.0         46           6.0         3.5         10.3         3.0         10.0         3.0         10.0         3.0         17.2         0.0         3.0         1.0         0.0         3.0         17.2         0.0         4.6           6.0         3.0         3.0         3.0         3.0         10.0         3.0         10.0         5.0         1.0         0.0         4.6	8	7 5.£	+	103	2.8	33	8	0:0	36	86	0.0	39	107	0.0	29	160	0.0	78	213	0.0	1 9	24	0 00
5.6         3.6         10.2         2.6         3.9         11.1         0.0         2.9         10.0         2.9         10.0         2.9         10.0         2.9         10.0         2.9         10.0         2.9         10.0         2.0         2.0         3.0         10.0         3.0         10.0         2.0         3.0         10.0         3.0         10.0         2.0         3.0         10.0         3.0         10.0         2.0         3.0         10.0         3.0 <td>5.7         37         103         2.8         3.9         3.9         10.0         3.9         11.0         0.0         3.9         160         0.0         78         2.2         0.0         46           5.9         35         103         2.9         3.3         94         0.0         36         102         0.0         39         113         0.0         59         172         0.0         78         2.2         0.0         46           6.0         35         103         2.0         3.0         107         0.0         59         172         0.0         78         2.2         0.0         46           6.0         3.0         3.0         3.0         100         3.0         100         0.0         59         172         0.0         78         2.4         0.0         46           6.0         3.0         3.0         3.0         3.0         100         3.0         100         3.0         100         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0</td> <td>86</td> <td>4 5.6</td> <td></td> <td>103</td> <td>2.8</td> <td>33</td> <td>91</td> <td>0.0</td> <td>36</td> <td>100</td> <td>0.0</td> <td>39</td> <td>109</td> <td>0.0</td> <td>59</td> <td>163</td> <td>0.0</td> <td>78</td> <td>217</td> <td>0.0</td> <td>10 11</td> <td>27 ,</td> <td>· · ·</td>	5.7         37         103         2.8         3.9         3.9         10.0         3.9         11.0         0.0         3.9         160         0.0         78         2.2         0.0         46           5.9         35         103         2.9         3.3         94         0.0         36         102         0.0         39         113         0.0         59         172         0.0         78         2.2         0.0         46           6.0         35         103         2.0         3.0         107         0.0         59         172         0.0         78         2.2         0.0         46           6.0         3.0         3.0         3.0         100         3.0         100         0.0         59         172         0.0         78         2.4         0.0         46           6.0         3.0         3.0         3.0         3.0         100         3.0         100         3.0         100         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0         4.0	86	4 5.6		103	2.8	33	91	0.0	36	100	0.0	39	109	0.0	59	163	0.0	78	217	0.0	10 11	27 ,	· · ·
6.0         35         103         2.9         33         96         0.0         36         105         39         115         0.0         59         175         0.0         78         239         0.0           6.0         35         103         3.0         36         107         2.0         36         107         0.0         39         117         0.0         59         175         0.0         78         233         0.0           6.1         35         104         3.0         36         109         2.0         39         120         0.0         59         182         0.0         78         240         0.0           6.3         35         108         3.1         36         115         2.1         36         110         0.0         39         120         0.0         59         182         0.0         78         244         0.0           6.6         35         112         2.0         36         124         0.0         39         124         0.0         59         182         0.0         78         248         0.0           6.6         35         112         0.0         39         126 <td>5.9         35         103         2.9         33         96         0.0         36         105         103         172         0.0         78         229         0.0         46           6.0         35         103         3.0         36         107         2.0         36         107         0.0         39         117         0.0         59         175         0.0         78         233         0.0         46           6.0         35         104         3.0         36         109         2.0         36         100         0.0         59         175         0.0         78         244         0.0         46           6.3         35         108         3.0         36         112         0.0         39         120         0.0         59         182         0.0         78         244         0.0         46           6.3         35         108         3.1         36         112         2.0         36         124         0.0         59         188         0.0         78         244         0.0         46           6.9         35         109         3.0         39         124         0.0</td> <td>χ 20   20</td> <td>2 0 0</td> <td>+</td> <td>103</td> <td>2.8</td> <td>33</td> <td>92</td> <td>0.0</td> <td>36</td> <td>103</td> <td>0.0</td> <td>39</td> <td>= 13</td> <td>0.0</td> <td>20</td> <td>169</td> <td>0.0</td> <td>2 × ×</td> <td>225</td> <td>0.0</td> <td>46 4</td> <td>31</td> <td>δ   œ</td>	5.9         35         103         2.9         33         96         0.0         36         105         103         172         0.0         78         229         0.0         46           6.0         35         103         3.0         36         107         2.0         36         107         0.0         39         117         0.0         59         175         0.0         78         233         0.0         46           6.0         35         104         3.0         36         109         2.0         36         100         0.0         59         175         0.0         78         244         0.0         46           6.3         35         108         3.0         36         112         0.0         39         120         0.0         59         182         0.0         78         244         0.0         46           6.3         35         108         3.1         36         112         2.0         36         124         0.0         59         188         0.0         78         244         0.0         46           6.9         35         109         3.0         39         124         0.0	χ 20   20	2 0 0	+	103	2.8	33	92	0.0	36	103	0.0	39	= 13	0.0	20	169	0.0	2 × ×	225	0.0	46 4	31	δ   œ
6.0         35         103         3.0         36         107         2.0         36         107         0.0         39         117         0.0         59         175         0.0         78         233         0.0           6.1         35         104         3.0         36         109         0.0         39         119         0.0         59         182         0.0         78         244         0.0           6.2         35         108         3.1         36         112         0.0         39         120         0.0         59         182         0.0         78         244         0.0           6.5         35         108         3.1         36         112         0.0         39         126         0.0         59         186         0.0         78         244         0.0           6.5         35         112         3.2         36         116         0.0         39         126         0.0         59         186         0.0         78         249         0.0           6.6         35         112         0.0         39         126         0.0         59         189         0.0         78 </td <td>6.0         35         103         3.0         36         107         2.0         39         117         0.0         59         175         0.0         78         233         0.0         46           6.1         35         103         3.0         36         107         2.0         39         117         0.0         59         178         0.0         78         240         0.0         46           6.2         35         108         3.1         36         112         0.0         39         120         0.0         59         189         0.0         78         249         0.0         46           6.3         35         108         3.1         36         112         0.0         39         122         0.0         59         189         0.0         78         249         0.0         46           6.6         35         112         3.1         36         114         0.0         39         124         0.0         59         189         0.0         78         249         0.0         46           6.6         35         116         0.0         39         124         0.0         59         189</td> <td>7.8</td> <td>9 5.6</td> <td><math>\vdash</math></td> <td>103</td> <td>2.9</td> <td>33</td> <td>96</td> <td>0.0</td> <td>36</td> <td>105</td> <td>0.0</td> <td>39</td> <td>115</td> <td>0.0</td> <td>59</td> <td>172</td> <td>0.0</td> <td>78</td> <td>229</td> <td>0.0</td> <td>1-</td> <td>33</td> <td><u>∞</u></td>	6.0         35         103         3.0         36         107         2.0         39         117         0.0         59         175         0.0         78         233         0.0         46           6.1         35         103         3.0         36         107         2.0         39         117         0.0         59         178         0.0         78         240         0.0         46           6.2         35         108         3.1         36         112         0.0         39         120         0.0         59         189         0.0         78         249         0.0         46           6.3         35         108         3.1         36         112         0.0         39         122         0.0         59         189         0.0         78         249         0.0         46           6.6         35         112         3.1         36         114         0.0         39         124         0.0         59         189         0.0         78         249         0.0         46           6.6         35         116         0.0         39         124         0.0         59         189	7.8	9 5.6	$\vdash$	103	2.9	33	96	0.0	36	105	0.0	39	115	0.0	59	172	0.0	78	229	0.0	1-	33	<u>∞</u>
6.1         35         104         3.0         109         2.0         39         120         50         178         50         178         50         10         52         10         50	6.1         35         104         3.0         36         103         3.0         39         103         0.0         39         176         0.0         39         178         0.0         39         178         0.0         39         178         0.0         39         178         0.0         39         178         0.0         39         178         0.0         39         178         0.0         39         178         0.0         39         180         0.0         39         180         0.0         78         244         0.0         46           6.3         35         108         3.1         36         113         2.1         36         115         0.0         39         122         0.0         59         180         0.0         78         244         0.0         46           6.5         35         112         3.2         36         117         2.2         36         118         0.0         39         122         0.0         59         180         0.0         39         170         0.0         59         180         0.0         46           6.5         35         113         2.2         36         118<	76	6.6	-	103	3.0	36	107	2.0	36	107	0.0	39	117	0.0	59	175	0.0	78	233	0.0	1 46	36 ,	φ c
6.3         35         108         3.1         36         113         2.1         36         112         0.0         39         122         0.0         59         183         0.0         78         244         0.0           6.4         35         109         3.1         36         115         2.1         36         114         0.0         39         124         0.0         59         186         0.0         78         248         0.0           6.5         35         112         3.2         36         116         0.0         39         126         0.0         59         189         0.0         78         256         0.0           6.8         35         112         3.2         36         119         0.0         39         122         0.0         59         198         0.0         78         256         0.0           6.8         35         112         3.2         36         120         0.0         39         136         0.0         59         198         0.0         78         256         0.0           6.9         35         121         0.0         39         136         0.0         59 </td <td>6.3         35         108         3.1         36         113         2.1         36         112         0.0         39         122         0.0         59         183         0.0         78         244         0.0         46           6.4         35         109         3.1         36         115         2.1         36         114         0.0         39         124         0.0         59         186         0.0         78         248         0.0         46           6.6         35         112         3.2         36         117         2.2         36         118         0.0         59         189         0.0         78         256         0.0         46           6.6         35         113         3.2         37         120         2.2         36         120         0.0         39         136         0.0         38         136         0.0         38         136         0.0         38         136         0.0         38         136         0.0         38         46           6.8         35         116         0.0         39         136         0.0         38         136         0.0         38<td>72</td><td>2 6.2</td><td>_</td><td>105</td><td>3.0</td><td>36</td><td>110</td><td>2.0</td><td>36</td><td>110</td><td>0.0</td><td>39</td><td>120</td><td>0.0</td><td>29</td><td>180</td><td>0.0</td><td>0 / 8/</td><td>240</td><td>0.0</td><td>46 4</td><td>00 4 40 4</td><td>o ∞ •</td></td>	6.3         35         108         3.1         36         113         2.1         36         112         0.0         39         122         0.0         59         183         0.0         78         244         0.0         46           6.4         35         109         3.1         36         115         2.1         36         114         0.0         39         124         0.0         59         186         0.0         78         248         0.0         46           6.6         35         112         3.2         36         117         2.2         36         118         0.0         59         189         0.0         78         256         0.0         46           6.6         35         113         3.2         37         120         2.2         36         120         0.0         39         136         0.0         38         136         0.0         38         136         0.0         38         136         0.0         38         136         0.0         38         46           6.8         35         116         0.0         39         136         0.0         38         136         0.0         38 <td>72</td> <td>2 6.2</td> <td>_</td> <td>105</td> <td>3.0</td> <td>36</td> <td>110</td> <td>2.0</td> <td>36</td> <td>110</td> <td>0.0</td> <td>39</td> <td>120</td> <td>0.0</td> <td>29</td> <td>180</td> <td>0.0</td> <td>0 / 8/</td> <td>240</td> <td>0.0</td> <td>46 4</td> <td>00 4 40 4</td> <td>o ∞ •</td>	72	2 6.2	_	105	3.0	36	110	2.0	36	110	0.0	39	120	0.0	29	180	0.0	0 / 8/	240	0.0	46 4	00 4 40 4	o ∞ •
6.4         35         109         3.1         36         115         2.1         36         114         0.0         39         124         0.0         59         186         0.0         78         248         0.0           6.5         35         112         3.2         36         117         2.2         36         116         0.0         39         126         0.0         59         189         0.0         78         256         0.0           6.7         35         112         3.2         37         119         2.2         36         118         0.0         59         189         0.0         78         250         0.0           6.8         35         117         3.3         37         125         2.3         36         120         0.0         59         198         0.0         78         260         0.0           6.8         35         112         3.2         37         125         2.3         36         125         0.0         39         136         0.0         59         201         0.0         78         260         0.0           7.1         35         125         2.7         36 </td <td>6.4         35         109         3.1         36         115         2.1         36         114         0.0         39         124         0.0         59         186         0.0         78         248         0.0         46           6.5         35         112         3.2         36         117         2.2         36         116         0.0         39         126         0.0         59         189         0.0         78         256         0.0         46           6.6         35         112         3.2         37         122         36         119         0.0         39         136         0.0         59         189         0.0         46           6.7         35         117         3.2         37         122         36         120         0.0         39         136         0.0         59         189         0.0         39         46           6.9         35         117         3.2         37         125         2.3         36         120         0.0         39         136         0.0         78         264         0.0         46           6.0         35         121         0.0</td> <td>7/</td> <td>11 6.3</td> <td><math>\vdash</math></td> <td>108</td> <td>3.1</td> <td>36</td> <td>113</td> <td>2.1</td> <td>36</td> <td>112</td> <td>0.0</td> <td>39</td> <td>122</td> <td>0.0</td> <td>59</td> <td>183</td> <td>0.0</td> <td>78</td> <td>244</td> <td>0.0</td> <td>1-</td> <td>42</td> <td><u>∞</u></td>	6.4         35         109         3.1         36         115         2.1         36         114         0.0         39         124         0.0         59         186         0.0         78         248         0.0         46           6.5         35         112         3.2         36         117         2.2         36         116         0.0         39         126         0.0         59         189         0.0         78         256         0.0         46           6.6         35         112         3.2         37         122         36         119         0.0         39         136         0.0         59         189         0.0         46           6.7         35         117         3.2         37         122         36         120         0.0         39         136         0.0         59         189         0.0         39         46           6.9         35         117         3.2         37         125         2.3         36         120         0.0         39         136         0.0         78         264         0.0         46           6.0         35         121         0.0	7/	11 6.3	$\vdash$	108	3.1	36	113	2.1	36	112	0.0	39	122	0.0	59	183	0.0	78	244	0.0	1-	42	<u>∞</u>
6.0         3.5         112         3.2         3.0         117         2.2         3.6         118         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         128         0.0         3.9         138         0.0         5.9         109         0.0         3.9         138         0.0         5.9         100         0.0         3.9         138         0.0         5.9         100         0.0         3.9         138         0.0         5.9         100         0.0         0.0         0.0         2.0         0.0         0.0         0.0         0.0         0.0         0.0 <td>6.0         35         112         3.2         3.0         117         2.2         36         118         0.0         39         128         0.0         39         0.0         39         129         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         130         0.0         39         130         0.0         39         130         0.0         39         140         0.0         39         130         0.0         39         130         0.0         39         130         0.0         39         140         0.0         39         130         0.0         39         140         0.0         39         130         0.0         39         140         0.0         39         140         0.0         39         140         &lt;</td> <td>89</td> <td>0 6.4</td> <td>-</td> <td>109</td> <td>3.1</td> <td>36</td> <td>115</td> <td>2.1</td> <td>36</td> <td>417</td> <td>0.0</td> <td>39</td> <td>124</td> <td>0.0</td> <td>220</td> <td>186</td> <td>0.0</td> <td>2 0</td> <td>248</td> <td>0.0</td> <td>46</td> <td>5 1</td> <td>φ 0 0</td>	6.0         35         112         3.2         3.0         117         2.2         36         118         0.0         39         128         0.0         39         0.0         39         129         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         120         0.0         39         130         0.0         39         130         0.0         39         130         0.0         39         140         0.0         39         130         0.0         39         130         0.0         39         130         0.0         39         140         0.0         39         130         0.0         39         140         0.0         39         130         0.0         39         140         0.0         39         140         0.0         39         140         <	89	0 6.4	-	109	3.1	36	115	2.1	36	417	0.0	39	124	0.0	220	186	0.0	2 0	248	0.0	46	5 1	φ 0 0
6.7         35         115         3.2         36         120         2.2         36         119         0.0         39         130         0.0         59         195         0.0         78         260         0.0           6.8         35         117         3.3         37         123         2.3         36         121         0.0         39         132         0.0         59         198         0.0         78         264         0.0           7.0         35         121         3.4         37         122         3.4         37         120         0.0         39         134         0.0         59         201         0.0         78         264         0.0           7.1         35         123         3.4         37         127         2.4         36         128         0.0         39         140         0.0         59         204         0.0         78         271         0.0           7.2         35         122         3.6         136         0.0         39         140         0.0         59         204         0.0         78         271         0.0           7.4         35         132<	6.7         35         115         3.2         36         120         2.2         36         119         0.0         39         130         0.0         59         195         0.0         78         260         0.0         46           6.8         35         117         3.3         37         123         2.3         36         121         0.0         39         132         0.0         59         198         0.0         78         264         0.0         46           6.9         35         112         3.4         37         129         2.4         36         128         0.0         59         201         0.0         78         264         0.0         46           7.1         35         123         3.4         37         129         2.4         36         128         0.0         39         134         0.0         59         201         0.0         46           7.1         35         123         3.4         37         132         2.4         36         138         0.0         39         144         0.0         59         201         0.0         46           7.2         35         132	96	1 6.6	+	113	3.2	37	119	2.2	36	118	0.0	39	128	0.0	59	192	0.0	78	256	0.0	46 +	49	0 4 8
6.8         3.5         117         3.3         3.7         123         2.3         3.6         121         0.0         39         132         0.0         59         198         0.0         78         264         0.0           6.9         3.5         119         3.5         123         6.0         39         134         0.0         59         204         0.0         78         264         0.0           7.0         3.5         121         3.4         3.7         129         2.4         36         126         0.0         39         138         0.0         59         204         0.0         78         275         0.0           7.2         3.5         12.6         3.6         126         0.0         39         140         0.0         59         201         0.0         78         275         0.0           7.3         3.5         12.7         3.6         132         0.0         39         144         0.0         59         212         0.0         78         28         0.0           7.4         3.5         12.2         3.6         132         0.0         39         144         0.0         59	6.8         35         117         3.3         37         123         2.3         36         121         0.0         39         132         0.0         59         198         0.0         78         264         0.0         46           6.9         35         119         3.3         37         125         2.3         36         123         0.0         39         134         0.0         59         204         0.0         78         264         0.0         46           7.1         35         121         3.4         37         129         2.4         36         126         0.0         39         140         0.0         59         204         0.0         78         204         0.0         46           7.2         3.5         126         36         128         0.0         39         140         0.0         59         210         0.0         78         204         46           7.2         3.5         37         131         2.5         36         130         0.0         39         144         0.0         59         212         0.0         46           7.2         35         132         2.0 <td>62</td> <td>2 6.7</td> <td>Н</td> <td>115</td> <td>3.2</td> <td>36</td> <td>120</td> <td>2.2</td> <td>36</td> <td>119</td> <td>0.0</td> <td>39</td> <td>130</td> <td>0.0</td> <td>59</td> <td>195</td> <td>0.0</td> <td>78</td> <td>260</td> <td>0 (</td> <td>1 46</td> <td>51</td> <td>84</td>	62	2 6.7	Н	115	3.2	36	120	2.2	36	119	0.0	39	130	0.0	59	195	0.0	78	260	0 (	1 46	51	84
7.0         35         121         3.4         37         127         2.4         36         125         0.0         39         136         0.0         59         204         0.0         78         271         0.0           7.1         35         123         3.4         37         129         2.4         36         126         0.0         39         138         0.0         59         207         0.0         78         275         0.0           7.2         35         126         3.6         126         0.0         39         140         0.0         59         207         0.0         78         275         0.0           7.4         35         126         3.6         126         0.0         39         140         0.0         59         210         0.0         78         279         0.0           7.5         35         132         2.6         36         132         0.0         39         144         0.0         59         218         0.0         39         144         0.0         59         218         0.0         39         144         0.0         59         218         0.0         30         14	7.0         35         121         3.4         37         127         2.4         36         125         0.0         39         136         0.0         59         204         0.0         78         271         0.0         46           7.1         35         123         3.4         37         129         2.4         36         126         0.0         39         138         0.0         59         207         0.0         78         275         0.0         46           7.2         35         125         3.6         126         0.0         39         140         0.0         59         207         0.0         78         279         0.0         46           7.3         35         127         3.5         37         132         2.5         36         140         0.0         59         210         0.0         78         279         0.0         46           7.5         35         132         2.7         136         132         0.0         39         144         0.0         59         221         0.0         46           7.6         35         132         0.0         39         148         0.0 <td>58</td> <td>5 6.8</td> <td>_</td> <td>117</td> <td>3.3</td> <td>37</td> <td>123</td> <td>2.3</td> <td>36</td> <td>121</td> <td>0.0</td> <td>39</td> <td>132</td> <td>0.0</td> <td>29</td> <td>198</td> <td>0.0</td> <td>78</td> <td>264</td> <td>0</td> <td>46 1</td> <td>54</td> <td>8 4 8</td>	58	5 6.8	_	117	3.3	37	123	2.3	36	121	0.0	39	132	0.0	29	198	0.0	78	264	0	46 1	54	8 4 8
7.1         35         123         3.4         37         129         2.4         36         126         0.0         39         138         0.0         59         207         0.0         78         275         0.0           7.2         35         125         3.6         128         0.0         39         140         0.0         59         210         0.0         78         275         0.0           7.4         35         125         3.6         130         0.0         39         144         0.0         59         215         0.0         78         283         0.0           7.5         35         132         3.7         136         2.7         36         146         0.0         59         216         0.0         78         283         0.0           7.5         35         132         3.7         140         2.7         36         148         0.0         59         221         0.0         78         2.1         0.0         50         221         0.0         20         20         0.0         20         20         0.0         20         0.0         20         0.0         20         20         0.0<	7.1         35         123         3.4         37         129         2.4         36         126         0.0         39         138         0.0         59         207         0.0         78         275         0.0         46           7.2         35         125         3.5         37         131         2.5         36         128         0.0         39         140         0.0         59         210         0.0         78         279         0.0         46           7.4         3.5         137         135         2.6         36         130         0.0         39         144         0.0         59         215         0.0         46           7.5         3.5         137         136         2.7         36         134         0.0         39         148         0.0         59         218         0.0         46           7.5         3.5         137         3.5         134         0.0         39         148         0.0         59         221         0.0         46           7.7         3.6         132         0.0         39         148         0.0         59         224         0.0         83	56	7 7.0	$\vdash$	121	3.4	37	127	2.4	36	125	0.0	39	136	0.0	59	204	0.0	78	271	0	11 9+	28	84
7.2 35 125 3.5 37 131 2.5 36 128 0.0 39 140 0.0 59 210 0.0 76 279 0.0 0.0 74 2.7 0.0 0.0 59 142 0.0 59 210 0.0 78 2.8 0.0 0.0 0.0 39 142 0.0 59 210 0.0 78 287 0.0 0.0 0.0 35 127 3.5 129 3.6 3.7 135 2.6 36 130 0.0 39 142 0.0 59 215 0.0 78 287 0.0 0.0 0.0 35 132 3.7 37 138 2.7 36 135 0.0 39 146 0.0 59 218 0.0 83 308 2.1 0.0 12.	7.2 35 125 3.5 37 131 2.5 36 128 0.0 39 140 0.0 59 210 0.0 78 287 0.0 46 7.4 35 127 3.5 37 133 2.5 36 130 0.0 39 142 0.0 59 210 0.0 78 287 0.0 46 7.4 35 129 3.6 3.5 37 135 2.6 36 130 0.0 39 142 0.0 59 215 0.0 78 287 0.0 46 7.5 35 132 3.7 37 138 2.7 36 134 0.0 39 146 0.0 59 218 0.0 83 308 2.1 46 7.5 36 133 3.7 37 140 2.7 36 135 0.0 39 146 0.0 59 221 0.0 83 312 2.1 46 7.7 36 136 3.8 37 142 2.8 36 137 0.0 39 150 0.0 59 224 0.0 83 318 2.4 46 7.8 36 134 3.0 39 151 0.0 59 227 0.0 84 325 2.1 46 7.8 36 141 4.0 38 147 3.0 39 153 0.0 39 153 0.0 64 249 2.0 85 332 3.0 46 8.0 36 144 4.3 38 151 3.3 40 157 2.3 39 155 0.0 65 258 2.6 86 344 3.9 46 8.0 36 144 4.3 38 151 3.3 40 157 2.3 39 155 0.0 65 258 2.6 86 344 3.9 30 46 8.0 36 158 3.0 46 8.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 36 158 3.0 46 8.0 46 8.0 46 8.0 46 8.0 46	55		+	123	3.4	37	129	2.4	36	126	0.0	39	138	0.0	53	207	0.0	2 %	275	-	46	09	8 4
7.4         35         129         3.6         37         135         2.6         36         132         0.0         39         144         0.0         59         215         0.0         78         287         0.0           7.5         35         132         3.7         37         138         2.7         36         134         0.0         39         146         0.0         59         218         0.0         83         308         2.1           7.6         35         132         3.7         37         140         2.7         36         135         0.0         39         148         0.0         59         221         0.0         83         308         2.1           7.7         36         136         36         137         0.0         39         150         0.0         59         224         0.0         83         318         2.4           7.8         36         138         36         139         0.0         39         151         0.0         84         325         2.7           7.9         36         144         4.0         59         223         36         325         3.0         84 <td>7.4         35         129         3.6         37         135         2.6         36         132         0.0         39         144         0.0         59         215         0.0         78         287         0.0         46           7.5         35         132         3.7         37         138         2.7         36         134         0.0         39         146         0.0         59         218         0.0         83         308         2.1         46           7.6         35         133         3.7         37         140         2.7         36         135         0.0         39         148         0.0         59         221         0.0         83         312         2.1         46           7.7         36         136         0.0         39         148         0.0         59         221         0.0         83         312         2.1         46           7.8         36         136         137         0.0         39         150         0.0         59         227         0.0         83         318         2.4         46           7.8         36         144         4.0         38</td> <td>51</td> <td></td> <td>+</td> <td>127</td> <td>3.5</td> <td>37</td> <td>133</td> <td>2.5</td> <td>36</td> <td>130</td> <td>0.0</td> <td>39</td> <td>142</td> <td>0.0</td> <td>20</td> <td>212</td> <td>0.0</td> <td>0 / 8</td> <td>283</td> <td>+</td> <td>+</td> <td>165</td> <td>0 4 8</td>	7.4         35         129         3.6         37         135         2.6         36         132         0.0         39         144         0.0         59         215         0.0         78         287         0.0         46           7.5         35         132         3.7         37         138         2.7         36         134         0.0         39         146         0.0         59         218         0.0         83         308         2.1         46           7.6         35         133         3.7         37         140         2.7         36         135         0.0         39         148         0.0         59         221         0.0         83         312         2.1         46           7.7         36         136         0.0         39         148         0.0         59         221         0.0         83         312         2.1         46           7.8         36         136         137         0.0         39         150         0.0         59         227         0.0         83         318         2.4         46           7.8         36         144         4.0         38	51		+	127	3.5	37	133	2.5	36	130	0.0	39	142	0.0	20	212	0.0	0 / 8	283	+	+	165	0 4 8
7.5         35         132         3.7         13         2.7         36         134         0.0         39         146         0.0         59         218         0.0         83         308         2.1           7.6         35         133         3.7         37         140         2.7         36         135         0.0         59         148         0.0         59         221         0.0         83         312         2.1           7.7         36         136         3.8         145         2.8         36         130         0.0         59         224         0.0         83         318         2.4           7.8         36         148         0.0         59         127         0.0         83         318         2.4           7.8         36         148         0.0         59         127         0.0         83         318         2.4           7.9         36         141         4.0         38         147         3.0         153         153         0.0         64         249         2.0         85         332         3.0           8.0         36         144         4.3         38 </td <td>7.5 35 132 3.7 37 138 2.7 36 134 0.0 39 146 0.0 59 218 0.0 83 308 2.1 46 7.6 35 132 3.1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3</td> <td>46</td> <td></td> <td><math>\vdash</math></td> <td>129</td> <td>3.6</td> <td>37</td> <td>135</td> <td>2.6</td> <td>36</td> <td>132</td> <td>0.0</td> <td>39</td> <td>144</td> <td>0.0</td> <td>59</td> <td>215</td> <td>0.0</td> <td>78</td> <td>287</td> <td>0</td> <td>Н</td> <td>Н</td> <td>84</td>	7.5 35 132 3.7 37 138 2.7 36 134 0.0 39 146 0.0 59 218 0.0 83 308 2.1 46 7.6 35 132 3.1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	46		$\vdash$	129	3.6	37	135	2.6	36	132	0.0	39	144	0.0	59	215	0.0	78	287	0	Н	Н	84
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7.8     36     138     3.9     38     145     2.9     36     139     0.0     39     151     0.0     59     227     0.0     84     325     2.7       7.9     36     141     4.0     38     147     3.0     39     153     2.0     39     153     0.0     64     249     2.0     85     332     3.0       8.0     36     144     4.3     38     151     3.3     40     157     2.3     39     155     0.0     65     258     2.6     86     344     3.9	7.8 36 138 3.9 38 145 2.9 36 139 0.0 39 151 0.0 59 227 0.0 84 325 2.7 46 7.9 36 144 4.3 38 147 3.0 39 153 2.0 39 153 0.0 64 249 2.0 85 332 3.0 46 8.0 36 144 4.3 38 151 3.3 40 157 2.3 39 155 0.0 65 258 2.6 86 344 3.9 46 VALUES IN FEFT. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w	44		+	136	3.8	37	142	2.8	36	137	0.0	39	150	0.0	59	224	0.0	83	318	2.4	46	74	84
7.9 36 141 4.0 38 147 3.0 39 153 2.0 39 153 0.0 64 249 2.0 85 332 3.0 80 8.0 36 144 4.3 38 151 3.3 40 157 2.3 39 155 0.0 65 258 2.6 86 344 3.9	7.9 36 141 4.0 38 147 3.0 39 153 2.0 39 153 0.0 64 249 2.0 85 332 3.0 46 8.0 3.0 36 144 4.3 3.0 151 3.3 40 157 2.3 39 155 0.0 65 258 2.6 86 344 3.9 46 VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w	42		Н	138	3.	2	145	2.9	36	139		39	151		59	227	0.0	84	325		ì		∞
	VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w	35	×	+	141	4 4	+	147		39	153		39	153		64	4   W		85	332		`	179	8 4 8 8
	% w VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w	AT ON		1																				
8 w VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w		Lt, L	≥ ⊗	ALUES				RADIUS	$\overline{\circ}$			ALLOW	/ABLE	RADIU			CORR	ESPO	DING	Ľ,	-r, AND		VALUES.	

TRANSITION CURVES - RURAL 35 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

The STOCK A DESIGN SPEELD OF ACT MPH (RURAL) USING E= 87 MAX.    18   17   WURL-20 F  WU	1	RAMPS	F		0	52	57	09	65	67	70	2 5	75	78	80 %	85	88	90	Ç6 96	98	101	106	108	= = =	116	119	124	126	129	134	137	142	144	150	152	157	160	16.5	168	170	175	178	183	186	188	193	196	198	204	900
Maint-Registry   Main				_ t	0	52	52	52	5.5	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	r c
Maint-Registry   Main		RCHAN	1 × × × × × × × × × × × × × × × × × × ×	ـــــــــــــــــــــــــــــــــــــ	0	2 49	54	26	5 2	64	99	99	200	73	76	80	83	82	06	93	95	100	102	105	110	112	117	119	122	127	129	134	136	141	144	0 4 1 4 8 4 1	151	153	158	160	165	168	173	175	177	182	185	197	192	10,
NOTICE FOR A DESIGN SPEED OF ADMINIST FUND HAS FIND HAS	XAN	INTER	5	۲	0	64	49	49	y 4 0 4	64	49	64	94	49	64	9 4	49	64	64 4	49	49	64 6	49	49	64	64	94	49	64	49	49	94	49	949	64	y 4 0	49	49	49	49	94	49	9 4 9 4	49	64	49	49	49	64	5
Mathematical Region		FT			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.1	2
NATIONAL PROPERTY OF THE PROPERTY OF THE WORLD-S FT WOR			0	د  ر	0	83	92	96	104	108	112	112	120	125	129	137	141	145	154	158	162	170	174	178	187	191	199	203	207	216	220	228	232	240	245	249	257	261	269	274	282	286	290	298	303	311	315	319	346	7 2 2
Mainth-list F   Maint-20 F	5	WIDT	1	- 1	0	83	83	83	2 62						833	83 6	83	83	000	83	83	000	83	83	83	83	83	83	83	83	83	83	83	83	83	83 83	83	833	83.0	83	83	83	83	83	83	83	83	83	8 8	5
Mainth-18 FT   Mainth-20 FT   Mainth-22 FT   Mainth-24 FT   Mainth-18 FT   Mainth-20 FT   Mainth-22 FT   Mainth-22 FT   Mainth-24 FT   Mainth-18 FT   Mainth-22 FT   Mainth-22 FT   Mainth-24 FT   Main	USI	<u> </u>		>	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	C
Colone   C		184	WID!H	<u>-</u> -	+	+			+		$\vdash$	+	_	+	+	+	$\vdash$	+	+	+	$\rightarrow$		+	-	_	$\vdash$	_	$\vdash$	_	+	-	_	$\vdash$	+	$\vdash$	+	$\vdash$	_					_	$\perp$			$\vdash$	239	46	090
Column   C	KUR,			<b>ا</b>	$\vdash$	+	+		+		$\forall$	+	_	+	+	+	Н	+	+	+	+	+	$\forall$	+	2 6	$\vdash$	+	$\vdash$	+	+	+	+	2	2 12	M 1	2 12	M	W 4	2 2	2 2	2 12	W 1	2 2	2 2	2	2 12	2	53 2	53 2	2 4 2
Name			₹H	_	$\vdash$		_		_			_		$\vdash$	_		ш	+		$\vdash$	_	+	$\perp$	_		$\vdash$		Н	+	$\perp$	_		-		$\sqcup$	_	$\vdash$	_	$\perp$	_	+	-	_	+			Н		0	 
Name	MP	-24 F	ANES 12-	<u> </u>	+	+						+			-			5 6	0 [	+	_	+	+	_		$\vdash$	+	$\vdash$	+	+	-	7 4	$\vdash$	+	+	27 6	29 C	31 0	35 0	_	+	2	0 6	+	$\vdash$	_	0 89	00 00	34 0.	16.6
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Carron   C	SPE	DTH=	ALEN-	-		+		+	+		$\vdash$	+		+	+	_	$\vdash$	+	+		2/2	2 2	$\vdash$	+	+	$\vdash$	+	H	+		+	9 9	1219	-	$\vdash$	+	118	2 2	+	+	+	H)	13	13	13	41 4	4	4 7	150	10,1
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CAN   F ACTORS   FOR   North   18 FT   North		DTH=2	70° 10° 10°	,   _	0	35	38	40	4 4 4	45	47	47	24 00	52	54	57	59	61	64	99	89	7 7	73	75	78	80	83	85	8 8	8 6	92	94	97	100	102	106	107	105	124	126	130	132	136	136	141	145	148	150	155	150
CN   F ACTORS   F	N			Ļ	0	35	3	20 2	0 6.	0 60	2	2 2	J W	2	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	39	39	39	39	39	39	39	39	39	39	40	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
(GN FACTOR WITH- WITH- NC 0 0 10 2.1 32 33 2.2 32 32 2.3 32 33 2.4 32 33 2.5 32 32 2.7 32 32 2.8 84 117 3.0 64 117 3.1 76 117 3.2 64 117 3.3 65 117 4.4 54 117 3.5 65 117 4.5 52 117 4.6 51 117 5.7 44 117 5.6 44 117 5.7 45 117 6.0 39 117 6.1 39 117 6.2 38 117 7.3 64 117 7.4 65 117 7.5 5.8 41 117 7.6 6.9 37 122 6.8 37 122 6.9 37 122 6.9 37 122 6.9 37 122 6.0 37 122 6.0 37 122 6.0 37 122 6.1 37 122 6.2 38 133 7.1 130 7.2 37 122 6.3 37 122 7.1 37 139 7.2 38 139		[뉴   논	_الة		0.0	0.0	0.0	0.0	) ) ) (	0.0	0.0	2.0	2.0	2.0	2.1	2.1	2.1	2.2	2.2	2.2	2.2	ر. ک ج	2.3	2.3	2.4	2.4	2.5	2.5	2.5	2.6	2.6	2.5	2.7	2.7	2.8	2 2 2	2.9	2.9	3.0	3.0	3.1	3.1	3.2	3.3	3.3	3.4	3.5	3.5	3.7	5
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		M		Ļ	0	32	32	32	20 25	32	32	8	8 4	78	9/	71	69	67	64	62	9	0 KG	26	55	52	51	49	84	47	45	45	44	45	47	40	39	38	38	37	37	37	37	37	37	37	ς 38 8	38	38 2	38	0 10
		>	-	E(%)	NC S	2.1	2.2	2.3	2.5	2.6	2.7	2.7	2.9	3.0	3.1	3.3	3.4	3.5	3.7	3.8	6.5	4.1	4.2	6.4	4.5	4.6	4.8	4.9	5.0	5.2	5.3	5.5	5.6	5.8	5.9	0.0 6.1	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.3	7.5	7.6	7.7	7.9	cα
ニー・ロー・ロー・ロー・ロー・ロー・ロー・ロー・ロー・ロー・ロー・ロー・ロー・ロー	SIG	SIGN	-40		П				Т								П											П									П										П			Т

TRANSITION CURVES - RURAL 40 MPH DESIGN SPEED

REV. 1/07 802.38

VIRGINIA DEPARTMENT OF TRANSPORTATION

SPECIFICATION REFERENCE

	MPS	F	۲	0 4	200	64	67	7 2 2	75	78	- α 84 84	98 8	92	92	92	97	100	106	108	111	117	120	122	128	131	136	139	142	147	150	153	158	161	167	172	175	178	183	186	100	194	197	203	205	208	211	216	219	TC-5.01
	E RAMPS	_ ∞		0 4	56	56	56	200	56	56	56	56	56	56	56	56	56	56	56	56	56	99	56	56	56	200	56	56	26	56	56	56	56	56	26	56	56	56	56	0 2	56	56	0 2	56	95	56	26	56	8
	INTERCHANGE	¥ T	۲	0 2	56	58	63	99	72	4/	//	882	4004	87	780	92	95	000	103	105	3 =	113	116	121	124	97 20	132	134	\ 0 \ 0 \ 0	142	145	150	153	821	163	166	168	174	176	2 2	184	187	200	195	197	200	202	208	VALUES
MAX.	NTER	16		0 4	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	53	5.7	53	53	5,7	53	53	53	53	53	ງ ≽
<u>``</u>	F		>	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	r, AND
00	- 1	12.	$\mathbb{H}$	0 6	94	98 (	07	7 2	20	25 (	34	38 (	5 4	47 (	747	56 (	09	69	4	178			96	05 (	60	4 6	23 (	27 (	36 (	40	45	54 (	58 (	0 67	76 0	80	85	94 (	98	20 0	212	0 00	25	29 (	34	38	5 7 4	52 (	, Lt, L
G	WIDTH=72	2		0 8	6 6	30 00	62	2000	39	39	2000	200	39	39	39	39 1	39	30 2	39	39	39	39 1	39	39 2	39 2	2000	39 2	39 2	39 2	39 2	39 2	39 2	2 2 2	2 2	39 2	39 2	39	39 2	39 2	20 00	2000	39	200	39 3	39 3	39 3	39 3	39 3	ING E,
USING			>	0.0	j ο.	0 0	0 0	2 0	0.	0.0	5 0	0.0	5 O	0.	0 0	0.	0 0	0.00	0:	0.0	0.00	0.	0 0	0.00	0.0		0.	0 0		0.	0 0	0.	0, 0	0.0	j ο σ	0.	0 0	0.	0.0	5 0	0.00	0.0		0.	0.	0 0	) O	0.0	" QNOA!
AL) (	4=48 FT	WID I HJ		0 0	, 0	4 6	0 0	4 6	. 0	4 1	) (o	4 7		0	0 4	0	0 0	+ 1	0 09	0 6	140	0 4	00	0 4	$\vdash$	164		0 0/1	4 V	$\vdash$	184 0		194 0	0 0	207 0	10 0	4 7	220 0	24 0	7 0	34 0	27 0	5 4	0 / 1	000	1 0	260 0	0 40	CORRESPONDING
RURA		LANE W		+	, /	/ /	0 00	00 00	0 6	0 0	\ \ \	7 7	7 1	7	7 7	7 11	7 7	7	7 13	7 13	7 7	7 14	7 7	7 15	7 5	7 16	7 16	7 7	-  -	7 18	7 7	7 7	7 7	7 20	7 20.	7 2	7 2	7 22	7 22	7 6	2 2	7 2	7 7	2,7	7 25	7 25	7 26	7 26	THE O
			Lt	0 0	9	9 9	9 0	0 0	9 0	9 0	9 9	9 9	9 9	9 0	0 0	9 0	9 9	+	9 0	9 0	+	0	9 9	0	0	0 0	0	9 0		0	9 9	9 0	0 0	9 0	9 9	9 0	0 0	9 0	9 0		9	9 0		9	9 0	9 9	9 9	9 0	FOR 1
MPH	1-24 FT	ANE S 12'			0 0	0 0	0 0	0 0	0	0 0	0 0	0 0	0.0	0.	0 0	0.0	0 0	0 0	7 0.	0 0	0		o c	+	0 0	5 0	0	0.0		0	2 0	7 0	0 0	0.0	0 0	0	W 17	7	0 0	7 4	0 0	000	0 0	5	0.	0 0	4	0 0	RADIUS F
45	WIDTH=24	1 🖭	Н	0 4	t 4	4 3	10	Ω Ω	9 9	9	0 0	9 7		7	7 7	2 2	ω ω	ó 86		ο ο ο ο	5 6	96	98	9 10	105	109	11.	10 11	3 10	17	12 2	12	12 12	51 5	5 5	41	4 4	4	4 4	ο το 5 π	5 5	15 %	0 10	19	91 2	16	1 =	7 17	_
0F		M	Lt	0 5	4 4	4 4	4	4 4	4	4	4 4	4 4	4 4	4	4 4	45	0 0	† <del>4</del>	45	4 4	4	4 6	4	4 4	4	4 4	4	4	4 4	4	4 4	4	4 4	4	4 4	4	4 4	4	4	4 4	4	4	4 4	4	4	4	4 4	4	ALLOWABLE
	EZ FT	2   E		0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0		0.0	0.0	0.0	0.0	0.0	0.0	0.0		+	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0 0	000	0.0	0.0	0 0	0.0	0.0	I I
SPEEI	WIDTH=22		1 1 1	0 5	43	45	4	5.7	55	28	62	64	89	68	68	72	74	78/	80	82	86	88	8 8	94	96	2 2	102	104	100	110	113	17	13	123	127	129	131	135	137	141	14.3	145	140	151	153	155	159	161	MUMINIMUM I
NS.	<b>⊣</b>	*^IDD:	Ľ	0 5	4	4 4	4	4 4	4	4 :	4 4	4 2	1 4	4	4 4	4	4 5	1 4	41	4 4	4	4	4 5	4	4 2	4 4	4	4 4	4 4	4	4 4	4	14 4	14 2	1 4	41	4 4	4	4 4	4 4	4	4 4	4 4	4	4	4 4	1 4	4 4	_H H M
$\overline{S}$		O' PRE	>	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.1	2 2	2.2	2.2	2.3	2.4	2.5	<u>s</u>
A	WIDTH=20 F	10 10'		0 %	39	43	45	4 4 6 4	20	52	56	28	62	62	62	65	67	71	73	75	78/	80	82	86	88	g 6	93	95	66	100	102	106	108	112	115	117	119	123	125	141	143	146	040	153	155	157	162	165	RADIUS
9 8	<u>≥</u>		Ļ	0 0	388	38	38	20 00	38	38	2 82	38	388	38	3000	38	38	388	38	38	38	38	38	388	38	20 00	388	38	9 89	38	2000	388	38 88	38	38 20	38	2000	388	38	δ 7	4	42	4 4 2	42	42	42	42	42	LISTED F
S F	18 FT	ZE.	>	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.1	2.1	2.1	2.1	22	2.2	2.2	2.3	2.3	2.3	2.4	2.4	4.7	2.4	2.5	2.5	2.5	2.6	2.6	2.6	2.7	2.8	2.8	2, c 0, 0	2.9	2.9	2 2	3.0	2.1	٠ - -	3.2	3.2	3.3	0.0 4.0	3.5	ΩI I
ORS	WIDTH=	100	1 - 1	0 2	35	37	40	247	45	47	50	52	55	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	132	1357	137	139	14.7	146	148	150	155	158	FEET.
ACT	M		Lt	0 2	34	34	34	34	34	34	34	34	34	80	80	76	74	70	68	66	63	62	9	28	57	54	53	52	50	49	φ 4 α	47	46	44	43	42	42	40	40	90	40	40	04 04 04	40	40	04	4 04	40	JES IN
Z	>	_	E(%)	N C	2.1	2.2	2.4	2.5	2.7	2.8	3.0	3.1	3.3	3.3	3.3	3.5	3.6	3.8	3.9	4.0	4.2	4.3	4.4 4.4	6.4	4.7	δ. 4 0. 6	5.0	5.1	5.3	5.4	5.5	5.7	8 6	6.0	6.2	6.3	6.4	6.6	6.7	0 0	7.0	7.1	7.7	7.4	7.5	7.6	/: %:	7.9	VALUES
DESIGN	DESIGN	VELOCI -45	RADIUS(FT)	8000	4337	4467	4057	3710	3554	3412	3152	3035	2866	2865	2822	2631	2544	2383	2308	2237	2104	2041	1982	1870	1817	1717	1669	1624	15.36	1495	1454	1376	1339	1266	1199	1166	1135	1073	1044	2101 986	957	929	874	845	817	787	723	683	NOTE:

SPECIFICATION REFERENCE

TRANSITION CURVES - RURAL 45 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 1/07 802.39

-	RAMPS	FT	Lr	90	66 66	69	75	78	2 48	87	93	96	102	105	=	114	1	117	120	126	129	135	138	144	150	156	162	168	174	180	186	189	195	198	201	207	210	216	219	225	228	231	[
		ω	Lt	99	09	09	09	09	09	09	09	909	09	60	09	09	09	90	90	09	60	99	09	909	09	09	09	09	09	09	09	09	09	09	909	60	90	60	09	09	09	09	l
MAX.	CHANGE	FT		57	59	65	2 12	73	79	82	2 80	90	96	99	104	107	3 2	110	116	138	121	127	130	135	141	146	152	158	163	169	175	177	183	186	101	194	197	203	205	211	214	217	
⊠	INTERCHANGE	19	± 0	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	57	22	57	57	57	57	57	57	57	57	57	57	57	57	57	l
00	T H		> 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
B B		121	<u></u>		106	+	+	N CO C	135	140	149	154	164	168	178		0 88	$\vdash$	192		_	10	21	231	240	250	255	269		t 0 0 1	298	303	312	317	522	532	336	346	351	_	+	370	
USING	WIDTH=72	2	t c	++	96	++	96	96	96	96	96	96	96	96	96		96	96	96	+	96	++	+	96	96	96	96	++	96	96	96	96	96	96	96	96	96	96	-	96	96	96	
	<b>-</b>			0.0			+		0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0		0.0	+		0.0				0.0					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	
(RURAL	WIDTH=48 FT ANF WIDTH)	0 12	ر ـــ	++	9/	++	/06		101		112 (	919	+	126 (	+		141		144	+	_	+	166 (		180	+	++	+ + +	+++	+	24 0	27 (	34	38	42	49 (	52 0	+	263 (	+	74	78   0	
	WIDTH		Lt L	+	2 2	1 2 6	1 2	1 2 0	7 7	2 5	2 2	2 0	2 1.	2 1	12	2 5	7 7	2 1	2 2	7 2	2 2	2 1	2 2	2 2	120	7 2 2	2 2 2	120	120	7 2 9	2 2	2 2	2 2	2 2	2 0	2 2	2 2	2 2	2 2	7 2	2 2	2	1
MPH	-  -		» (	+	0.0	000	0 0	0.0	0		0.0		0.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	000	0.0	0.0	0.0	000	0.0	0.0	0	0.0	0 0	0.	0.0	0 7	7 0.	) 0	7	7   0 0	` ?
50	1=24 FT	12'		++		+	+	+++	) (O	0 0	0 0	0 0	0 0	4 7	0		+			+		+	3 0	0 0	0 0	200		1 2 1		4 1	0.0	2 6	+ 0	6	 	+ 9	ω <u>-</u>	3 0.	0 9	)       	3 0	7	
90	빌	5 -	c	+	5 53		+		+	1	0 8			φ α	-		3 94		96	+	<u> </u>	++	2 2	3 3	21 2	0 8 2	8 8 8	2 2 2	5 4 5	4 4	8 8 4 4	8 0	8 5 5	51 5	2 4	3 16	3 16	3 17	3 17	2 8	180	7	5
	FT W		Lt		0 48		-	4 4				84 8			+		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		48	+		+	$\perp$		4 4 8	+	4 4 4	-	++	1 4.	4 4	4 4	4 4	4	4 4	48	4 4	48		2 4 4 8 4 8	4 8		f _
SPEE		1 - 1	> C	+			0.0	+++	+	0.0	0.0	0.0	0.0	0.0	+	0.0	+			++	_	+	0.0			0.0	+	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	_	-
	WIDTH=22 FOLIVALENTS	10	7 0	++	47	5 2 2	25.0	28	62	64	69	71	75	77	82	8	8 8	86	88	93	95	6	102	106	110	135	119	124	128	132	135	139	14.3	146	148	152	154	159	161	165	168	176	-
ESIGN	IM NITIO		L	$\dashv$	4 4 4	4 4	4 † 4 †	4 4	1 4 4 4	44	4 4 4 4	4 4	4 4	44	44	44	4 4 4 4	44	4 4 4	4	4 4 4 4	4 4	4 4 4 4	44	4 4	4 4	4 4 4	4 4	4 4	4 4 3	44	44	1 4 4 4	4 4	4 4	44	4 4 4 4	44	44	4 † † † † † † † † † † † † † † † † † † †	44	7	+
	띮		> 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	2.0	2.1	2.1	000	7.7
OR A	WIDTH=20 F	1@ 10	٦	9 9	44	94 4	5 5	52	56	200	62	64	89	70	747	76	0 %	78	80 80	84	88	8 8	92	96	100	104	108	112	116	120	122	126	130	132	134	138	140	159	161	166	168	171	-
	<u></u> Z		† c	9 9	04 04	04 4	4 04	04	4 04	04	04 4	4 6	4 0	40	40	40	04	40	04	4	0 4 0 4	9 4	404	40	4 6	4 4	04 6	4 6	4 4	04 6	04	40	04	04	0 4	40	404	45	45	45	45	45	)
ORS	18 FT DES	2	> 0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.2	2.2	2.2	2.2	2.2	2.3	2.3	2.4	4.6	2.4	2.5	2.5	2.6	2.6	2.6	2.7	2.8	2.8	2, c 00, 00	2.9	2.9	3.0	3.0	3.7 7.7	3.1	4.2	1
ACT	IDTH= 1	1@ 9-	ב כ	36	38	24	4 4 5	74	51	53	56	288	62	63	67	69	147	147	147	147	147	147	147	147	147	147	14/	147	147	147	14 /	147	147	147	147	147	147	152	154	159	161	16.4	_
ഥ	MID		†	36	36	36	36	36	36	36	36	36	36	36	36	36	76	76	74	70	69	99	64	62	59	20	55	53	51	64	84	47	46	45	44	43	42	43	43	54	43	43	2
DESIGN			E(;;)	2.0	2.2	2.3	2.5	2.6	2.8	2.9	3.1	3.2	3.4	3.5	3.7	3.8	3.9	3.9	4.0	4.2	4.4	4.5	4.6	4.8	5.0	5.2	5.4 7.4	5.6	5.8	6.0	6.2	6.3	6.5	9.9	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	6.9	7.0	7.2	7.3	7.5	7.6	77	
DE	DESIGN	-20	î												T												1838								T								

TRANSITION CURVES - RURAL 50 MPH DESIGN SPEED

SPECIFICATION REFERENCE

NOTE: Lt, Lr & w VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w VALUES.

REV. 1/07 802.40

	RAMPS	FT	۲	0 64	67	73	76	79	98	68	76	CD 86	102	105	11	114	117	120	127	130	136	139	143	143	146	149	152	158	162	165	171	174	177	184	187	190	196	199	203	209	212	218	222	225	228 241	234	237	240	247	250	253	TC-5.01
		∞	Lt	0 49	64	64	64	64	64	64	40	64	64	64	40	64	64	40	64	64	40	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	64	40	64	64	64	64	64	64	64	64	64	64	64	64	ι
	INTERCHANGE	FT	۲	0 8	63	69	72	75	80	83	g 6	92	92	86	104	107	13	115	119	122	120	131	134	134	137	140	143	149	152	155	160	163	169	172	175	181	184	187	197	196	199	202	208	211	214	220	223	226	232	235	238	VALUE
MAX.	NTE	16	Lt	0 8	09	09	09	09 09	09	09	200	09	09	09	200	09	09	200	309	09	8 8	09	09	09	09	09	09	09	09	09	09	09	9	09	09	09	09	09	20 00	09	09	09	09	09	09	9	09	09	09	09	09	>
.;   	F	_	*	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Lt, Lr, AND
=	WIDTH=72	0 12	۲	103	108	118	123	128	138	143	94.	159	164	169	179	184	189	35	205	210	220	225	230	230	235	240	246	256	261	266	276	281	286	297	302	307	317	322	327	338	343	353	358	363	368	378	383	389	399	404	409	E, Lt,
9	MIDI	2	Ļ	103	103	103	103	103	103	103	10.5	103	103	103	10.3	103	103	10.5	103	103	10.3	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	103	10.5	103	103	103	103	103	103	DING
USING	L F	<u> </u>	3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	) C	0.0	0.0	0.0	0.0	0.0	0.0	CORRESPONDING
AL)	WIDTH=48 F	@ 12	۲	0 /	18	68	92	96	104	108	711.7	119	123	127	135	138	142	14p	154	158	16.5	169	173	17.3	177	180	184	192	196	200	207	211	215	223	226	230	238	242	246	253	257	265	269	272	2/6	284	288	292	299	303	307	CORRE
(RUR	WIDTH	2	Lt	0 /	77	//	77	11	77	77	1	//	77	77	//	77	7	1	77	77	//	77	77	11	//	77	77	//	77	77	//	77	77	77	77	77	77	77	//	77	77	//	77	77	//	77	77	77	//	77	77	丑
	FT	- 1	>	0.0	0.0	0.0	0.0	0 0	0.0			0.0	0.0		0.0		0.0	0 0	0.0	0.0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	FOR
MPH	WIDTH=24 F	@ 12.	7	0	54	59	62	64	69	72	1,5	//	82	85	6	92	95	200	103	105	100	113	115	115	2 2	120	123	128	131	133	138	141	143	149	151	15.4	159	161	16.6	169	172	177	179	182	184	189	192	195	200	202	205	RADIUS
	WIDTH	5 -	Lt	0	52	52	52	52	52	52	22	52	52	52	2 22	52	52	22.2	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	22	52	52	52	52	52	52 72 72	52	52	52	52	52	52	
	FT W		> (	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	ALLOWABLE
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SIGN			>	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0					0.0	0.0	0.0		0.0			0.0	0.0	0.0	0.0	0.0		0.0			0 0		0.0		0.0	0.0	0.0	0:0	2.0	2.0	2.1	2.2	2.3	IS THE
	MDTH=20 F	@ 10.		0 43	45	4 6 4	52	5.4	58	09	7.9	66	69	77	75	77	<u>,</u>	- C	9	88 8	00	94	96	96	080	001	103	201	109	11 11	115	118	120	124	126	128	132	135	130	141	143	0 4	149	152	40 40 40 40 40 40 40 40 40 40 40 40 40 4	158	9/1	178	0 8	187	190	RADIUS I
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$\bigcirc$	V PT V		>	0.0		0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.5	5.3	2.3	2.3	5.3	4.2	4.7	4.7	2.5	2.5	2.5	2.5	9.0	2.6	2.6	5.6	2.7	2.7	/ 8.	8.	80.0	σ. σ. σ	2.9	3.0	3.0	3.1	3.2	3.3	LISTED
2 /	# 19	-6		39 (	H	45 (		48	+	54	200	209	62 (	$\pm$	0 00	+	<u>                                    </u>	7,5	2/2	79 (	ν 2 α	85 (	87	[5]	101	161	161	101	161	161	161	161	161	161	161	161	161	161	10 12	161	161	101	161	161	161	165	891	0/1	. 6/1	. 6/1	182	FE T.
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				2 NC	$\perp$	_		_	_		_	_	Н	_	+		_	_	+		_	_		+	_	$\vdash$	_	_	$\vdash$	_	_	$\vdash$	_			_	_	_	_	$\perp$		_	$\vdash$	_	_	_	$\vdash$	_	_	Н	_	VALUES
DESIGN	DESIGN VFI OCITY	. 22	1 1	+	H	+		+	+		+	+	Н	+	+	$\vdash$			+		+	+	$\vdash$		+	H	+	+	Н	+	+		+	+	$\dashv$	+		$\vdash$	+	$\top$		+	Н	$\dashv$		+	$\vdash$	+	+	H	$\dashv$	≥ ⊗
DE	DES VFI (	. "	RADIUS(FT)	7190	6821	6179	5897	5638	5177	4972	3//4	4432	4274	4125	385	3728	3610	3498	3285	3192	3000	2927	2866	2865	2768	2692	262	2486	242	2356	2295	2185	2130	2026	1976	1927	1833	1788	1/4	1657	1615	1532	1491	1450	1405	1327	1285	1241	1145	1085	964	NOTE: Lt, Lr

SPECIFICATION REFERENCE

# TRANSITION CURVES - RURAL 55 MPH DESIGN SPEED

	AMPS	FT	٦	0	70	74	80	84	60	94	100	104	107	114	117	120	127	130	134	140	144	147	154	157	164	167	174	174	177	180	187	194	200	204	210	214	217	224	227	234	237	240	247	250	254	
	INTERCHANGE RAMPS WIDTH	2	Lt	67	<u> </u>	67	67	67	67	29	/9	67	67	67	29	67	67	67	67	67	29	67	67	67	67	67	/9	67	/9	67	67	67	/9	67	67	29	67	67	67	/9	29	67	/9	29	67	1
MAX.	SCHAN WIF	F	الر	63	99	73	76	79	85	88	9.	86	101	107	110	113	120	123	126	132	135	139	145	148	154	157	164	164	167	170	176	182	189	192	198	201	204	211	214	220	223	226	233	236	239	
% N	NTE	9	Lt	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	63	4 1
III	FT	_	> (	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	=
	WIDTH=72	@ 12'	١.	107	112	118	128	134	144	150	155	166	171	182	187	192	203	208	214	224	230	235	246	251	262	267	278	278 278	283	288	299	310	320	326	336	342	347	358	363	374	379	384	395	400	406	4,
USING	MIDI	2	t]	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107	107
	L F	<u> </u>	≥ (	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	_ C
(RURAL)	WIDTH=48 FT	0 12	١	08	84	92	96	100		112	+		128		140	_	+	-	164		172	176	+	188			208	_	+		+	232	240	244	252	256	_	268	Q   (	-	284	_	296	300	304	ας
1 1	WIDTH	2	t,	0 8	80	8 8	+	80	8 8	80	200	08	80		80	+	+	08	08 08	+	H	08 08	+	08 6	+		8 8	08 8	+	08 80		8 8 8	000	08 8		+	08 80	Н	08	80	_	08 6	000	80	80	0
MPH				+	$\vdash$		$\vdash$	+	+	$\vdash$	+	_	0.0	_	$\vdash$	0.0	+	_	0.0	$\perp$	$\sqcup$	+	++	_	$\perp$	$\vdash$	0.0	0.0	0.0		$\perp$	0.0	+	_	$\perp$	$\rightarrow$	0.0	$\perp$	0.0	0.0	0.0	_	0.0	0.0	0.0	00
		@ 12.		+	) 99	_	64 (	_	+	$\vdash$	+		98		$\vdash$	+	+	+	1107	+	Н	118	+	126 (	+	134 (	+	+	_	144	+	+	0 0	163 (	+	7	74 (	6	182	+	190	+	198	$\vdash$	203 (	208
90	WIDTH=24			54	54	4 4	45	40.0	t 40	54	4 4	4	45	4 4	54	4 4	1 1	1	1 4 5	54 1	54	40	40	40	54	40	54	40	54 1	54 1	40	40	40 4	40	54		40 40	1 1	40	1 4	54	40.0	40.04	54 2	54   2	C V =
	FT W				0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0.0	0.0	0 0	0.	0.0	0.	0.0	9 0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0. 0	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0	 0.	c
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ISI-	- =			0.0		0.0	$\vdash$	0.0	_	$\vdash$		-	0 0	0 0	0	0 0	+	_	0.0	$\perp$	$\vdash$	$\perp$	++	0.0	$\perp$	$\vdash$	0.0	0 0		0 0	$\perp$	++	0.0	0.0	$\perp$	0.0	0.0	0		0 0	0	0 0	0 0	0.	0.	_ _
<	WIDTH=20 FT	10.		45 0	$\vdash$		+	+	0 09	$\vdash$	+	+	2 0	+ 9	80	0 6	+	$\dashv$	+	+	Н	+	+	2 2	, 6	7	4 9	9 9	8 0.0	3 0	191	, 6	7 4	0 α	140 0	W 1	2 2	o	2 2	1 9	+	160	υ ιδ Ο Ο	0 /	0	- 5
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DESIGN	× Z ::			2.0	2.1	2.2	2.4	2.5	2.7	2.8	3.0	3.1	3.2	3.4	3.5	3.6	3.8	3.9	4.0	4.2	4.3	4 4 4 6	4.6	7.4	4.9	5.0	5.2	5.2	5.3	5.4	5.6	5.00	0.0	6.1	6.3	6.4	6.6	6.7	8.0	7.0	7.1	7.2	\ \ 4.	7.5	7.6	777
	DESIGN VELOCITY	09=	ADIUS(FT)	12000	8048	7654	6965	6661	6121	5879	5444	5247	5063	4725	4571	4424 4286	4155	4030	3911	3690	3587	3488	3303	3216	3053	2975	2866	2865	2759	2692	2565	2445	2332	2277	2173	2122	2072	1974	1925	1830	1782	1735	1638	1588	1537	1100

TRANSITION CURVES - RURAL 60 MPH DESIGN SPEED

SPECIFICATION REFERENCE

NOTE: Lt,Lr& w VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E,Lt,Lr,AND w VALUES.

REV. 1/07 802.42

	MPS	L		0 6	73	77	84	00	94	97	104	108	115	118	122	129	132	130	142	146	149	156	160	163	170	174	777	184	187	191	198	201	201	205	208	215	219	225	229	232	239	243	246	253	257	260	264	270	274	TC-5.0′	1
	E RAI	_   œ		0 8	9 9	2 2	2 2 3	9 9	2,0	2/2	2 2	2 5	2 2	70	2/2	2 2	2	2 5	2 2	70	2 5	2 2	70	9 8	70	70	2 5	2 2	70	2 2	202	2/2	2 2	20	2 2	70	2 5	2 2	70	2 5	2 2	20	2 5	70,	70	2 6	5 6	5 6	2 5	?	
	INTERCHANGE RAMPS	MDT FT		08	9 69	72	6/2	82	68	92	088	102	108	112	115	121	125	171	134	138	141	147	151	154	160	164	167	174	17.7	180	187	190	190	193	196	203	206	213	216	219	226	229	232	239	242	245	249	255	258	262   VALUES	į
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X	F		*	0.0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.0.	0.0	0.0	0.0	0.0	0.0	Lt, Lr, AND	:
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JSING			*	0.0	o: 0:	0 0	0.0	) c	0.	0 0	0 0	0.0	0.0	0.	0 0	0	0.0	)     	0 0	0.	0 0	0	0.0	) c	0.	0.	0 0	0.0	0.	0 0	0.	0 0	0 0	0.	0 0	0.	0.0	5 0	0.	0 0	0.	0.	o c	5 0.	0.	0. (	5 C	0	0.0	- I o.	;
AL) U	48 FT	WIDTH)	<u> </u>	0 0	88	0 0	- 5	သ စ	4	0 0	7 9	0 5	1 6	5	0 0	55 0	0	4 α Ο C	2 2	Н	180	+	H	70/19/	$\vdash$	210 0	4 ¤	22.0	27 0	31 0	29 0	5 2	12 0	0 21	52 0	0 00	264 0	3 5	0 //	281	0 68	294 0	298 0	306 0	0 01	4 ;	19 23 0	27 0	31	CORRESPONDING	; 5
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ED	ابما		>	0.0	0.0	0.0	0.0	5 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	١.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	00	0.0	0 0	0.0	0.0	0.0	0.0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5 O	0.0	0.0	0.0	5 0	0.0	0.0	1	- 1
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	M	<b>√</b>   00  ∧	Lt	0 (	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	52	THE MI	
ESIGN	[ ] ,	- 1	>	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0 0	0.0	0.0	<u>.</u> S	2
A	WIDTH=20	SOFTWARE	,   _	10	4 4	52	56	59	63	99	00/	73	77	8	82	8 0	89	20 0	96	86	100	105	107	130	114	117	119	124	126	128	133	135	135	138	140	145	147	152	154	156	161	163	166	170	173	175	180	182	184	L ZUB	; į
OR			Ļ	0 !	4 4	4 4	74	4 4	47	7 4 7	4 4	4 7	ţ	47	7 4 7	4 4	4 7	4 4	4 4	47	4 7	t 4	47	4 4	47	47	47	t 4	47	7 4	47	7 4 7	4 4	47	7 4	47	47	4 4	47	4 7	47	47	4 4	47	47	4	4 4	47	47	S.1 52	
S F(	18 FT	DESIGN	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	) ) )	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.4	2.5	2.5	2.5	2.5	2.5	2.6	2.6	2.6	2.7	2.7	2.7	2.8	2.8	2.0	2.9	2.9		
ORS	"DTH= 1	© 0	_	0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	74	2 2	53	57	59	63	65	200	72	74	0 82	80	82	98	88	90	95	97	90	103	105	107	= =	114	116	120	122	191	191	191	191	191	<u> </u>	191	191	191	191	191	191	191	191	191	191	192	IB/	
ACT	MIC		Lt	0 ;	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	42	99	65	64	62	61	0 65	28	58	56	55	45	53	52	51	51	49	49	SO I	- 1
L Z	,	— · ≻	E(%)	S S	2.0	2.2	2.4	2.5	2.7	2.8	3.0	3.1	3.3	3.4	3.5	3.7	3.0	υ. 4 υ. σ	7	4.2	5.4	4.5	9.4	4 4 √. α	6.4	5.0	7.7	5.3	5.4	5.5	5.7	0.0	0.00	5.9	6.0	6.2	6.3	6.5	9.9	6.7	0.9	7.0	7.1	7.3	7.4	7.5	7.6	7.8	7.9	VALUES	
DESIGN	DESIGN	VELUCII Y =65			9566 9083		$\top$							Ħ	1	1			$\top$	П			П		Ħ						П					Ħ	1	$\top$	П						Ħ			$\top$	$\top$	_ ≥	,

SPECIFICATION REFERENCE

TRANSITION CURVES - RURAL 65 MPH DESIGN SPEED

VIRGINIA DEPARTMENT OF TRANSPORTATION

REV. 1/07

	RAMPS	H	دً .	0 1	79	83	87	90	98	102	105	113	120	124	128	132	139	143	150	154	158	162	169	173	180	184	188	195	199	207	210	218	222	229	237	240	244	244	252	255	263	267	274	278	285	289	293
	3E RA	α	±	0 1	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	75	7
MAX.	INTERCHANGE	WIDTH FT T	د .	0 8	75	0/	82	98 8	93	96	100	107	= = =	# 12	121	125	132	136	139	146	150	153	160	164	168	175	200	185	189	196	200	207	210	217	224	228	232	232	239	242	249	253	260	264	271	274	010
	INTER	Ä		0 8	72	72/	72	72	72	72	72 / 2	72	72	72	72	72	72	72	72 /2	72	72	72	72	72	72/	72	72	72	72	72	72	72	72	12 2	72	72	72/2	72	72	72	72	72	72	72	72	72	72
8 %	14		>	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	-
E E		10,		$\vdash$	126	+	38	4 C	156	162	168	180	19.5	198	$\vdash$	210	222	228	234	+	252	258	270	276	782	594	2002	312	318	330	336	348	354	366	378	384	062	390	102	117	±14 170	126	2, 28, 28	444	456	462	-
USING	WIDTH=72	۲	Lt	Н,	07 02	Ŧ,	20 1	20 7	20 1	20 ,	20 20	+	20 %	+	-	20 %	20 2	20 2	07 02	20 2	20 2	200	20 2	20 20	20 20	20 2	200	20	20 20	20	200	20	20 02	202	20 20	20 3	20 20	20	20 2	20 20	20 4	20 4	20 4	20 20	+	20 4	
			*	<u> </u>		5 0	0.	0 0	0.	0.0	0.0	0	0.0	0.0	0.	0.0	0.	0.0	0.0	0.	0.	0 0	0.	0 0	5	0.	0.0	0.0	0 0	0.	0 0	0.	0 0	0.0	5 0	0 0	) ) )	0 0	0.0	0.0	5 0	0 0	0 0	0.0	0.	0 0	
(RURAL)	WIDTH=48 FT	LANE WIDTH)	1		90	+	$\Box$	08 0.	7	22	6. 12 0 0	55 0.	0 0	149	0.0	0 0		7 :	9/1			94	+	0 0	7 8	21 0.	50.0	34 0	39 0.	8	52 0.	51.0	0 0.	75 0.0	2 42	38	33 0.	93 0.	200	90 1	5 0.0	0 0	.00	0 0	72 0	0 0	
	/IDTH:	ANE «	1	H	+	+		+	11	21 2	2 0	2 5	2 2	+	0	0 (	16	1)	) (	0 18	38	0 0	20	20	2 2	0	0 0	0 2	2 2	0 24	2 2	2 2	26	200	287	28	200	250	3 30 6	2 6	3 0	32	32	2 3	0 34	34	
MPH		AT L	Lt	$\vdash$	200	+	+	8 8	0	0	0 0	1	8 8	8 8	6	ة اة 0 د	0	σ o	5 6 5 C	6	O. 0	δ   δ Ο   C	6	δ (c	5 0 5 0	δ 0	δ   δ Ο   C	) Ö	δ σ 0 c	0	δ   δ Ο   C	0	5 6 0 C	0	50	0	5 5 5 0	0	500	δ   δ	6 6 0	δ σ 0 c	0	δ   δ Ο   C	6	0 0	
70 /			*	0.0	_	+	+	0 0	+	$\vdash$	5 0	+	0.0	+	H	0.0	+	+	0.0	10	0 (	o c	0	o c	j 0	H	0.0	+	0.0	+	0.0	4	0 0	++	0 0	0.0	0 C	000	+	0.0	+	3 0.0	+	0.0	-	0 0	
0F ,	WIDTH=24	DESIGN SOFTWARE EQUIVALENTS (NUMBER OF LANES 10 10 10 11 10 11 10 12	<u> </u>		+	+	69	+	78	20 2	20 00	6	93	000	102	105	+	-	170	+	`	129	135	138	14,4	14.	15.7	156	162	165	168	17	177	1 00 6	<u> </u>	19.	0 0	195	201	204	210	213	219	222	228	23	
	>	ABER	Lt		9 9		+	9 9	09	09	9 9	9	9 9	8 8	9	9 9	9		9 9		09	9	9	9	9 9	09	09 09	09	9 9	9	09 09	9	99	188	09	09	9 9	09	8 6 8	09 09	8 8	9 6	99	09 09	09	9 8	
SPEED	2 FT	S (NU)	. ≥	0.0	0 0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0 0	0.0	0.0	0 0	0.0	0.0	+	0.0	+	0.0	0.0	0.0	0.0	0.0	0.0	+	0.0	+	0.0	+	0 0	$\perp$	0.0	
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DESIGN	MIC	ZUIVAI	ij	0 5	55	22	55	55	55	55	22	55	55	22	22	55	22	55	ζ. 7.7.	55	55	55	55	22	22	55	55	22	55	55	55	22	55	55	22	55	22	55	55	55	22	55	55	55	55	55	
	ᇤ	- RE	*	0.0	0.0			0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0		0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0:0	0.0	0.0	0.0	
A A	WIDTH=20	DFTWAI		0 8	53	55	28	09	65	9	7.3	75	78	83	85	88	93	95	98	103	105	108	113	115	120	123	125	130	133	138	140	145	148	153	158	160	163	163	168	170	175	178	183	185	190	193	
FOR	MID	SN SC	Ľ	0 5	202	20	50	20	50	50	202	50	20	20	50	20	50	50	202	50	50	20	50	20	20	50	20	50	50	50	200	20	50	202	20	50	202	50	20	20	20	20	20	20	50	20	
ORS	S FT	DESI	>	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	2.5	2.6	2.6	2.6	2.6	2.7	2.7	2.7	2.8	
FACTORS	WIDTH= 18	ō 0	,   <u>`</u>	0 ;	4 4 5 A	50	52	54	59	61	65	68	70	75	77	79	8	98	88 6	93	95	97	102	104	106	Ħ	113	117	120	124	126	131	133	138	142	144	14 / 205	205	205	205	205	205	205	205	205	205	
	.OIM	-	Lt	0 ;	4 4 7	45	45	45	45	45	45	45	7 7	45	45	45	45	45	4 4 5 م	45	45	45	45	45	4 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4	45	45	45	45	45	45	45	45	45	45	45	45	64	62	61	29	58	57	5 5	54	54	
DESIGN	Η.		E(%)		2.0	2.2	2.3	4.7	2.6	2.7	χ. 2 6.2 6.2	3.0	3.1	3.3		3.5	3.7	3.8	v. v.	4.1	4.2	4 4 ک 4	4.5	9.4	. 4 %.	6.4	5.0	5.2	5.3	5.5	9.6	. 8.	5.9	6.1	5.3	4.6	5.5	5.5	6.7	ω σ ω σ	7.0	7.1	5.7	4. 7.	7.6	7.7	
DES	DESIGN	VELOCITY =70	RADIUS(FT) E		10/51 2		П	8851 2	8127	7805	7227	6967	6724		6079	5888	5537	5376	5222	4937	4805 4	4679 4	4443 4	4332	4226 4	4027	3933 (	3756	3673	3514 E	3439	3296	3228	3099 (	2977 6	2919 6	2865	2862 6	2753 (	2699 (	2590 7	2535	2423	2365 /	2242	2175 7	

TRANSITION CURVES - RURAL 70 MPH DESIGN SPEED

SPECIFICATION REFERENCE

NOTE: Lt, Lr & w VALUES IN FEET. LISTED RADIUS IS THE MINIMUM ALLOWABLE RADIUS FOR THE CORRESPONDING E, Lt, Lr, AND w VALUES.

REV. 1/07 802.44